

YAYASAN BRATA BHAKTI DAERAH JAWA TIMUR UNIVERSITAS BHAYANGKARA SURABAYA LEMBAGA PENELITIAN DAN PENGABDIAN PADA MASYARAKAT (LPPM)

Kampus : Jl. A. Yani 114 Surabaya Telp. 031 - 8285602, 8291055, Fax. 031 - 8285601

SURAT KETERANGAN Nomor: Sket/ 13 /I/2023/LPPM/UBHARA

Kepala Lembaga Penelitian dan Pengabdian kepada Masyarakat (LPPM) Universitas Bhayangkara Surabaya menerangkan bahwa:

Nama	: Dr. Amirullah, ST, MT.
NIP	: 197705202005011001
NIDN	: 0020057701
TT 1. TT 1	77 I I DI I

Unit Kerja : Universitas Bhayangkara Surabaya

Benar telah melakukan kegiatan:

- Menulis jurnal berjudul Matlab/simulink simulation of unified power quality conditioner-battery energy storage system supplied by PV-wind hybrid using fuzzy logic controller (Amirullah, Ontoseno Penangsang, Adi Soeprijanto) di International Journal of Electrical and Computer Engineering (IJECE), Vol. 9, No. 3, June 2019, pp. 1479~1495, ISSN: 2088-8708, Publisher: Institute of Advanced Engineering and Science (IAES). Terindeks Scopus. Terindeks Scopus Q2.
- Telah melakukan korespondensi melalui email dalam proses penerbitan jurnal tersebut. Bukti korespondensi email dan bukti pendukung adalah benar sudah dilakukan oleh yang bersangkutan serta sudah dilampirkan bersama surat ini.

Demikian surat keterangan ini dibuat untuk kepentingan kelengkapan pengusulan Guru Besar.

Surabaya, 20 Januari 2023 Kepala LPPM

Drs. Heru Irianto, M.Si. NIP. 9000028

Lampiran 1 Bukti Korespondensi Email dengan Editor/Pengelola Jurnal

[IJECE] Submission Acknowledgement

From: Tole Sutikno (ijece@iaesjournal.com)

To: am9520012003@yahoo.com

Date: Wednesday, 2 May 2018 at 05:15 pm GMT+7

The following message is being delivered on behalf of International Journal of Electrical and Computer Engineering (IJECE).

Amirullah Amirullah:

Thank you for submitting the manuscript, "Comparative Performance of Unified Power Quality Conditioner-Battery Energy Storage System Supplied by PV/Wind/PV-Wind Hybrid using Fuzzy Logic Controller" to International Journal of Electrical and Computer Engineering (IJECE). With the online journal management system that we are using, you will be able to track its progress through the editorial process by logging in to the journal web site:

Manuscript URL:

http://iaescore.com/journals/index.php/IJECE/author/submission/13075 Username: amirullah_2017

If you have any questions, please contact me. Thank you for considering this journal as a venue for your work.

Tole Sutikno

International Journal of Electrical and Computer Engineering (IJECE)

International Journal of Electrical and Computer Engineering (IJECE) <u>http://www.iaescore.com/journals/index.php/IJECE</u>

Review Progress Paper ID 13075_Amirullah

From: amir rullah (am9520012003@yahoo.com)

- To: ijece@iaesjournal.com
- Cc: ijece@iaesjournal.com
- Date: Tuesday, 28 August 2018 at 07:58 am GMT+7

Dear Assoc Prof. Tole Sutikno, Ph.D.

Managing Editor IJECE

On Wednesday 2 May 2018 I had send paper ID 13075 title "Comparative Performance of Unified Power Quality Conditioner-Battery Energy Storage System Supplied by PV/Wind/PV-Wind Hybrid using Fuzzy Logic Controller" to International Journal of Electrical and Computer Engineering (IJECE) via online submission system (in review).

I would like know, how is the result of review progress of this paper now?

This is my email and I would be happy if you respond it.

Best Regards,

Amirullah PhD Candidate in EE ITS Surabaya Indonesia

Amirullah Paper ID 13075 Review Progress

From: amir rullah (am9520012003@yahoo.com)
To: ijece@iaesjournal.com
Cc: raditaapriana@gmail.com
Date: Friday, 14 September 2018 at 09:31 am GMT+7

Dear Assoc Prof. Tole Sutikno, Ph.D or Dr. Radita Apriana (IJECE Commitee)

I would like to get information by you for the paper ID 13075 entitle "Comparative Performance of Unified Power Quality Conditioner-Battery Energy Storage System Supplied by PV/Wind/PV-Wind Hybrid using Fuzzy Logic Controller (Amirullah, Ontoseno Penangsang, Adi Soeprijanto)" to International Journal of Electrical and Computer Engineering (IJECE)-in review, submitted on 2 May 2018.

How is the progress now? Has my paper already obtained a reviewer who will correct it?

I am sorry because I always asks you because my PhD Supervisors (Prof Ontoseno P and Prof Adi S) always asked to me about it.

I will be happy if you respond my email.

This is the email and thanks a lot for your cooperation.

Best Regards

Amirullah PhD Candidate in EE ITS Surabaya Indonesia

http://iaescore.com/journals/index.php/IJECE/author/submissionReview/13075

From: amir rullah (am9520012003@yahoo.com)

To: raditaapriana@gmail.com

- Cc: ijece@iaesjournal.com
- Date: Monday, 5 November 2018 at 06:30 am GMT+7

Dear Dr. Radita Apriana/Dr. Tole Sutikno IJECE Commitee

On 4 October 2018 I have revised my paper entitled Matlab/Simulink Simulation of Unified Power Quality Conditioner-Battery Energy Storage System Supplied by PV-Wind Hybrid using Fuzzy Logic Controller. The link is below:

http://iaescore.com/journals/index.php/IJECE/author/submissionReview/13075.

I would like information from you when the final result (acceptance information) release. I apologize asking you again because both of my PhD supervisors always asking me about the result of this paper.

The paper status now is **IN REVIEW: REVISIONS REQUIRED**.

This is my question and thanks a lot for responding.

Amirullah PhD Candidate in EE ITS Surabaya

Re: [IJECE] Revised Version Uploaded #13075

From: IJECE Journal (ijece@iaesjournal.com)

- To: am9520012003@yahoo.com
- Cc: adisup@ee.its.ac.id

Date: Friday, 9 November 2018 at 09:19 pm GMT+7

Dear Mr. Amirullah

It is my great pleasure to inform you that your paper is accepted and will be published on forthcoming issue of the International Journal of Electrical and Computer Engineering (IJECE), a Scopus indexed journal, SJR 2017 & CiteScore 2017 Q2 on both of the (Electrical & Electronics Engineering) and (Computer Science). Congratulations!

This journal is an OPEN ACCESS. Why publish open access? IAES open access authors benefit from: Quality, established and reputable journal, reaching key audiences' with 5 million users per month, high citations, etc. Benefits of the OPEN ACCESS policy:

- Researchers as authors: immediate visibility for research output and thus increased visibility and usage of their results. Open Access may even lead to an increase of impact.

- Researchers looking for information: access to literature everywhere, not only from a campus but also from any site with wifi access.

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So, Open access fee is paid by the authors, or on their behalf to support the cost of wide open access dissemination of research results, to pay deposit to CrossRef in order to each published articles has a Digital Object Identifier (DOI), to manage the various costs associated with handling and editing of the submitted manuscripts, and the Journal management and publication in general.

Each accepted paper will be charged (based on first author and first institution): USD 265 (~IDR 3500K for Indonesian Authors). This charge is for the first 8 pages, and if any published manuscript over 8 pages will incur extra charges USD45 (~IDR 600K for Indonesian Authors) per page (http://www.iaescore.com/journals/index.php/IJECE/about/submissions#authorFees)

The payment should be made by bank transfer (T/T): Bank Account name (please be exact)/Beneficiary: TOLE SUTIKNO Bank Name: Bank Mandiri Branch Office: Yogyakarta Kusumanegara City: Yogyakarta Country :Indonesia Bank Account # : 1370003247703 (main account) or, Bank Account # : 1370012625477 (secondary account) SWIFT Code: BMRIIDJAXXX

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Checklist for preparing your FINAL paper for publication: <u>http://www.iaescore.com/journals/index.php/IJECE/about/editorialPolicies#custom-3</u>

We really appreciate your total commitment to supporting this journal.

Thank you

Best Regards, T. Sutikno Editor IJECE@iaesjournal.com http://www.iaescore.com/journals/index.php/IJECE

On Thu, Oct 4, 2018 at 1:17 PM, Tole Sutikno <<u>ijece@iaesjournal.com</u>> wrote: The following message is being delivered on behalf of International Journal of Electrical and Computer Engineering (IJECE).

Tole Sutikno:

A revised version of "Matlab/Simulink Simulation of Unified Power Quality Conditioner-Battery Energy Storage System Supplied by PV-Wind Hybrid using Fuzzy Logic Controller" has been uploaded by the author Amirullah Amirullah.

Submission URL:

http://iaescore.com/journals/ index.php/IJECE/editor/ submissionReview/13075

Re: [IJECE] Revised Version Uploaded #13075

From: amir rullah (am9520012003@yahoo.com)

- To: ijece@iaesjournal.com
- Cc: raditaapriana@gmail.com
- Date: Friday, 9 November 2018 at 10:10 pm GMT+7

Dear IJECE Commitee,

Thanks a lot for your information and I would proccess the payment for the paper (ID: 13075) soon.

Amirullah PhD Candidate EE ITS Surabaya Lecturer Ubhara Surabaya

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Checklist for preparing your FINAL paper for publication: <u>http://www.iaescore.com/journals/index.php/IJECE/about/editorialPolicies#custom-3</u>

We really appreciate your total commitment to supporting this journal.

Thank you

Best Regards, T. Sutikno Editor IJECE@iaesjournal.com http://www.iaescore.com/journals/index.php/IJECE

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Tole Sutikno:

A revised version of "Matlab/Simulink Simulation of Unified Power Quality Conditioner-Battery Energy Storage System Supplied by PV-Wind Hybrid using Fuzzy Logic Controller" has been uploaded by the author Amirullah Amirullah.

Submission URL: http://iaescore.com/journals/ index.php/IJECE/editor/http://iaescore.com/journals/ index.php/IJECE/editor/ submissionReview/13075

Re: [IJECE] Revised Version Uploaded #13075

From: IJECE Journal (ijece@iaesjournal.com)

To: am9520012003@yahoo.com

Date: Saturday, 10 November 2018 at 12:45 pm GMT+7

Please adhere our guide. Maintain space and margin

On Sat, Nov 10, 2018 at 6:22 AM, amir rullah <<u>am9520012003@yahoo.com</u>> wrote:

Dear Dr. Tole Sutikno IJECE Commitee

I am apologize I would like to ask you why my paper ID 13075 back to revision again after accepted.

If I have any mistake please forgive me.

Amirullah PhD Candidate ITS Surabaya Lecturer Ubhara Surabaya

On Friday, 9 November 2018, 11:41:23 PM GMT+7, IJECE Journal <<u>ijece@iaesjournal.com</u>> wrote:

Please contact/reply to this email ONLY, or we will remove your paper Thank

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Re: [IJECE] Revised Version Uploaded #13075

From: amir rullah (am9520012003@yahoo.com)

To: ijece@iaesjournal.com

Cc: ijece@ieasjournal.com

Date: Sunday, 11 November 2018 at 01:47 pm GMT+7

Dear IJECE Admin,

Here I send you revised paper-3rd (ID: 13075) base on your file (doc) and last request.

I also have submit this paper to online submission system.

This is my email and your cooperation is apreciated. Thanks a lot.

Regards,

Amirullah

On Sunday, 11 November 2018, 9:27:11 AM GMT+7, IJECE Journal <ijece@iaesjournal.com> wrote:

Please make sure that your all tables and figures do not OUT the margin

On Sun, Nov 11, 2018 at 9:25 AM, IJECE Journal <ijece@iaesjournal.com > wrote:

Please use our file and do revise your paper carefully, and do not change any space (only to reduce your page length), or we will reject your paper. Submit your camera ready paper and complete your publication fee as soon. your cooperation is very appreciated.

On Sun, Nov 11, 2018 at 8:18 AM, amir rullah <<u>am9520012003@yahoo.com</u>> wrote:

Dear IJECE Admin,

Here I send you the revised paper-ID 13075 (2nd revision) entitled Matlab/Simulink Simulation of Unified Power Quality Conditioner-Battery Energy Storage System Supplied by PV-Wind Hybrid using Fuzzy Logic Controller (Amirullah Amirullah, Ontoseno Penangsang, Adi Soeprijanto).

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Thanks a lot for your request and I will revise it soon.

If the paper have been revised, I have to send it by this email or submit via online submissio (author version) or both of them?

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Cc: ijece@iaesjournal.com
Date: Monday, 12 November 2018 at 06:41 am GMT+7

Dear Dr. Tole Sutikno Ijece Commitee

Today I would send publication fee for our paper ID 13075 (15 pages) to your account in Mandiri Kusumanegara Jogja. The nominal fee is Rp. 7.700.000.

Rp. 3.500.000 (8 pages) + Rp. 4.200.000 (7 pages x Rp 600.000) = Rp. 7.700.000

Is the nominal fee correct?

This is my question and thanks a lot for your answer.

Best Regards,

Amirullah

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Lampiran 2 Bukti Pendukung

Lampiran 2.1 Naskah Makalah Submitted

Comparative Performance of Unified Power Quality Conditioner-Battery Energy Storage System Supplied by PV/Wind/PV-Wind Hybrid using Fuzzy Logic Controller

Amirullah^{1,2}, Ontoseno Penangsang¹, Adi Soeprijanto¹

¹Department of Electrical Engineering, Faculty of Electrical Technology, ITS Surabaya, ²Study Program of Electrical Engineering, Faculty of Engineering, University of Bhayangkara Surabaya

Article Info

ABSTRACT (10 PT)

Article history:

Received Jun 12th, 201x Revised Aug 20th, 201x Accepted Aug 26th, 201x

Keyword:

Power Quality UPQC Battery Energi Storage Photovoltaic Wind Turbine Total Harmonic Distortion Disturbance Scenario

This paper presents comparative performance of Unified Power Quality Conditioner-Battery Energy Storage (UPQC-BES) system supplied by Photovoltaic (PV)/Wind/PV-Wind Hybrid connected to three phase three wire (3P3W) of 380 volt (L-L) and 50 hertz distribution system. Fuzzy Logic Controller (FLC) is implemented to maintain DC voltage across the capacitor under disturbance scenarios of source and load as well as compare the results with Proportional Intergral (PI) controller. There are six scenarios of disturbance i.e. (1) non-linear load (NL), (2) unbalance and nonlinear load (Unba-NL), (3) distortion supply and non-linear load (Dis-NL), (4) sag and non-linear load (Sag-NL), (5) swell and non-linear load (Swell-NL), and (6) interruption and non-linear load (Inter-NL). In disturbance scenario 1 to 5, implementation of FLC on UPQC-BES system supplied by PV/Wind/PV-Wind Hybrid is able to result average THD of source voltage slightly better than PI and both methods have already met the limit in IEEE 519. Under scenario 6, FLC applied on UPQC-BES system supplied by PV/Wind/PV-Wind Hybrid gives better significantly result of average THD of source voltage than PI. In interference scenario 1 to 5, FLC method applied on UPOC-BES system supplied by PV/Wind/PV-Wind Hybrid with BES is able to result average THD of source current slightly better than PI. Furthermore under scenario 6, FLC applied on UPQC-BES system supplied by PV/Wind/PV-Wind Hybrid gives significantly better result average THD of source current than PI. In six scenarios of disturbance, both PI and FLC applied on UPQC-BES system supplied by PV/Wind/PV-Wind Hybrid, PV is able to result the highest average THD of load voltage/source current.

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1. INTRODUCTION

Photovoltaic (PV) and wind are the most renewable energy (RE) distributed generations (DGs) because able to convert sunlight and wind into power. PV/solar is one of potential DGs sources since it only need sunlight to generate electricity, where the resources are available in abundance, free and relatively clean. Indonesia has enormous energy potential from the sun because it lies on the equator. Almost all areas of Indonesia get sunlight about 10 to 12 hours per day, with an average intensity of irradiation of 4.5 kWh/m² or equivalent to 112.000 GW. The potential of wind energy in Indonesia generally has a speed between 4 to 5 m/s and classified as medium scale with potential capacity of 10 to 100 kW. The weakness of PV/wind turbine besides able to generate power, they also produces a number voltage and current harmonics resulted by presence of several types of PV/wind turbine devices and power converters as well as to increase a number of non-linear loads connected to the grid, so finally resulting in the decrease in power quality.

To overcome and improve power quality due to presence of non-linear loads and integration of PV and wind turbine to grid, furthermore it is a proposed UPQC. It serves to compensate for source voltage quality problems i.e. sag, swell unbalance, flicker, harmonics, and load current quality problems i.e. harmonics, unbalance, reactive currents, and neutral current. B. Han et. al and Vinod Khadkikar have investigated UPOC as one part of active power filter consisting of shunt and series active filters connected in parallel and serves as superior controller to overcome a number of power quality problems simultaneously. Series component was responsible for reducing a number of interference on source side i.e. voltage sag/swell, flicker, unbalanced voltage, and harmonics. This equipment served to inject a number of voltages to keep load voltage fixed at desired level in a balanced and distortion free. Shunt component was responsible for addressing a current quality problems i.e. low power factor, load current harmonics, and unbalanced load. It served to inject current on AC system so that source current became sinosioda balanced and in phase with source voltage [1,2]. UPQC based on RE has been investigated by some researchers. There are two methods used to overcome this problem i.e. using conventional and artificial intelligence. Shafiuzzaman K.K., et.al have proposed system includes a series inverter, shunt inverter, and a DG connected to a DC link through a rectifier using PI. The system was capable of increase source voltage quality (sag and interruption) and load current quality, as well as transfer of active power on/off grid mode [3]. The influence of DG on UPOC performance in reducing sag under conditions of some phase to ground faults to using DSTATCOM has been implemented by Norshafinash S., et.al. The DG was effective enough to help UPQC to improve sag [4]. It was connected in series with load resulting better sag migitation compared to system without DG. Implementation of UPQC using UVTG method with PI to reduce sag, swell, voltage/current harmonics has been done by S. N. Gohil, et.al. Simulation of voltage distortion was made by adding 5th and 7th harmonics at fundamental source voltage, resulting in a reduction of THD source current and THD load voltage [5].

UPQC supplied by PV panels using boost converter, PI, MPPT P and O, and p-q theory has been proposed by Yahia Bouzelata at.al [6]. The system was capable of compensate reactive power and reduce source current/load voltage harmonics, but did not discuss migitation of sag and interuption caused by PV penetration. Power quality enhancement of sag and source voltage harmonics on grid using UPQC supplied by PV array connected to DC link using PI compared with FLC has been done by Ramalengswara Rao, et.al. Combination of UPQC and PV using FLC can improve source voltage THD better than PI [7]. Amirullah et.al have researched a method for balancing current and line voltage, as a result of DGs of a single phase PV generator unit in randomly installed at homes through on a three phase four wire 220 kV and 50 Hz distribution line using BES and three of single phase bidirectional inverter. Both devices was capable of reduce unbalanced line current/voltage, but both of them were also capable of increase current/voltage harmonics on PCC bus [8]. Power quality migitation of UPQC on microgrid supplied by PV and wind turbine has been implemented by K S Srikanth et. al. It resulted that PI and FLC was able to improve power quality and reduce distortion in output power [9]. The UPQC-wind turbine to provide active power to overcome low sag and interruption voltage to grid has been investigated by H.Toodeji, et.al. The model was used VSC as a rectifier on generator output and controlled so that maximum power desired can be generated by different speed wind turbines using PI [10]. The UPQC-wind turbine connected to UPQC DC link was implemented by M. Hosseinpour, et al. The proposed combination using PI was capable of compensate swell, interruption voltage, and reactive power both on on/off grid [11]. R.Bhavani, et, al have researched on UPQC controlled by FLC to improve power quality in a DFIG wind turbine connected grid. FLC can improve power quality i.e. sag voltage and load current harmonics better than PI [12]. Power quality enhancement on wind turbine and BES with PI connected grid on PCC bus using UPQC has been implemented by S.Rajesh Rajan, et al. BES was installed to maintain and stabilize active power supply under different wind speed [13].

This research will compare UPQC-BES performance supplied by PV/wind/PV-wind hybrid connected to 3P3W of 380 volt (L-L) and 50 hertz distribution system. BES serves to store excess energy produced by PV/wind/PV-wind hybrid and distribute it to load if necessary, to prevent interruption voltage, and to adjust charging and discharging of energy in battery. BES is also expected to store excess power produced by three RE combinations and use it as backup power. FLC is proposed and compared with PI to control variable of DC voltage and DC reference voltage input to generate reference current source in current hysteresis controller on shunt active filter. DC voltage controller in shunt active filter and series active filter is used to migitate power quality of load voltage and source current. Performance of two controllers are used to determine load voltage, source current, load voltage THD, and source current THD based on IEEE 519.

This paper is presented as follow. Section 2 describes proposed method, model of UPQC-BES system supplied by PV/wind/PV-wind hybrid, simulation parameters, PV and PMSG wind turbine model, series and shunt active filter, as well as application of PI and FLC method for proposed model. Section 3 shows results and discussion about performance of THD analysis on the proposed model of PV/wind/PV-wind hybrid connected to DC link of UPQC-BES system using PI and FLC. In this section, six disturbance scenarios are presented and the results are verified with Matlab/Simulink. Finally, this paper in concluded in Section 4.

2. RESEARCH METHOD

2.1. Proposed Method

Figure 1 presents proposed model in this research. The RE based DG used is PV/Wind Turbine/PV-Wind Turbine Hybrid connected to 3P3W distribution system with 380 volt (L-L) and 50 Hz frequency, through UPQC-BES system. PV array produce power under fixed temperature and radiation as well as connect to UPQC-DC link through a DC/DC boost converter. The maximum power point tracking (MPPT) method with Pertub and Observer (P and O) algorithms helps PV produce maximum power and generate output voltage, as the input voltage for DC/DC boost converter. The converter serves to adjust duty-cycle value and output voltage of PV as its input voltage to produce an output voltage corresponding to UPQC DC link voltage. Wind turbine type used is a permanent magnetic synchronous generator (PMSG) with variable speed and fixed voltage which generating power and is connected to UPQC DC link circuit through AC/DC bridge rectifier. The rectifier helps to change AC PSMG stator output voltage to DC voltage through LC circuit that serves to filter and smooth it before connected to UPQC-DC link. BES connected to the UPQC-DC link circuit serves as energy storage and is expected to overcome interruption voltage and overall help UPQC performance to improve voltage and current quality on source and load bus. Simulation parameters proposed in this study is shown in Appendix Section. Power quality analysis is performed on PV/Wind/PV-Wind Hybrid conditions connected to 3P3W system through UPQC DC-link (on-grid) using BES circuit. Single phase circuit breakers (CBs) are used to connect and disconnect PV/Wind/Hybrid PV-Wind with UPQC DC-link. Each condition consists of six disturbance scenarios namely (1) NL, (2) Unba-NL, (3) Dis-NL, (4) Sag-NL, (5) Swell-NL, and (6) Inter-NL. FLC is used as a DC voltage control in a shunt active filter to improve the power quality of the load voltage and current source and compare it with PI controller. Each disturbance scenario uses a PI controller and FLC so that the total of 12 disturbances. The result analysis of research was carried out i.e. (1) voltage and current on source or poin common coupling (PCC) bus, (2) voltage and current on load bus, (3) harmonic voltage and harmonic current on source bus and (4) harmonic voltage and harmonic current on load bus. The final phase is to compare performance of UPQC-BES system on-grid supplied by PV/Wind/PV-Wind Hybrid using two controllers to improve power quality of load voltage and source current under six disturbance conditions.



Figure 1. Proposed model of UPQC-BES system supplied by PV/Wind/PV-Wind Hybrid

2.2. Photovoltaic Model

Figure 2 shows the equivalent circuit and V-I characteristic of a solar panel. A solar panel is composed of several PV cells that have series, parallel, or series-parallel external connections [14].


Figure 2. Equivalent circuit and V-I characteristic of solar panel The V-I characteristic of a solar panel is showed in (1):

$$I = I_{PV} - I_o \left[\exp\left(\frac{V + R_s I}{aV_t}\right) - 1 \right] - \frac{V + R_s I}{R_p}$$
(1)

where I_{PV} is the photovoltaic current, I_o is saturated reverse current, 'a' is the ideal diode constant, $V_t = N_S K T q^{-1}$ is the thermal voltage, N_S is the number of series cells, q is the electron charge, K is the Boltzmann constant, T is the temperature of p–n junction, R_S and R_P are series and parallel equivalent resistance of the solar panels. I_{PV} has a linear relation with light intensity and also varies with temperature variations. I_o is dependent on temperature variations. The values of I_{PV} and I_o are calculated as following (2) and (3) below:

$$I_{PV} = (I_{PV,n} + K_1 \Delta T) \frac{G}{G_n} I$$
(2)
$$I_o = \frac{I_{SC,n} + K_1 \Delta T}{\exp(V_{OC,n} + K_V \Delta T) / aV_t - 1}$$
(3)

In which $I_{PV,n}$, $I_{SC,n}$ and $V_{OC,n}$ are photovoltaic current, short circuit current and open circuit voltage in standard conditions ($T_n = 25$ C and $G_n = 1000$ Wm⁻²) respectively. K_I is the coefficient of short circuit current to temperature, $\Delta T = T - T_n$ is the temperature deviation from standard temperature, G is the light intensity and K_V is the ratio coefficient of open circuit voltage to temperature. Open circuit voltage, short circuit current and voltage-current corresponding to the maximum power are three important points of I-V characteristic of solar panel. These points are changed by variations of atmospheric conditions. By using (4) and (5) which are derived from PV model equations, short circuit current and open circuit voltage can be calculated in different atmospheric conditions.

$$I_{SC} = (I_{SC} + K_1 \Delta T) \frac{G}{G_n} \qquad (4) \qquad V_{OC} = V_{OC} + K_V \Delta T \qquad (5)$$

2.3. PMSG Wind Turbine

Wind turbine is onother part of an integrated system, which can be divided into two types i.e. fixed and variable speed wind turbines. In fixed speed type, rotating speed of turbine is fixed and hence, frequency of generated voltage remains constant, so it can be directly connected to the network. In this case, maximum power can not always be extracted by wind. On the other hand, on variable speed, turbine can rotate at different speeds, so maximum power can be generated in each wind speed by MPPT method [10]. The advantage of using a PMSG over a synchronous generator and DFIG machine because it has high efficiency and reliability. Due to the elimination of rotor external excitation, machine size, and cost also decreases, making PMSG to be more controlled easily with feedback control system. PMSG has become an attractive solution on wind generation systems with variable speed wind turbine applications [15]. Figure 3 and 4 shows model of PMSG wind turbine and wind turbin power characteristic curve.



Figure 3. Model of PMSG wind turbine

Figure 4. Wind turbin power characteristic curve

The output power of wind turbine can be expressed using (6), (7), and (8) [11].

$$\lambda = \frac{\omega_r R}{V_{wind}} \qquad (6) \qquad P_M = \frac{1}{2} \rho \pi R^2 C_p V_{wind}^3 \qquad (7) \qquad T_M = \frac{P_M}{\omega_r} = \frac{1}{2} \rho \pi R^5 C_p \frac{\omega_M^3}{\lambda^3} \qquad (8)$$

Where λ is the speed-tip ratio, V_{wind} is wind speed, R is blade radius, ω_r is rotor speed (rad/sec), ρ is the air density, C_P is the power coefficient, P_M is the output mechanical power, and T_M is output torque of wind turbine. The C_P coefficient is dependent on the pitch angle value, at which rotor blade can rotate along axis and tip-speed ratio λ expressed in (9).

$$C_{P} = (0.44 - 0.167\beta)\sin\frac{\pi(\lambda - 2)}{(13 - 0.3\beta)}$$
(9)

Where β is a pitch angle blade. In a fixed pitch type, the value of β is set to a fixed value.

2.4. Control of Series Active Filter

The main function of series active filter is as a sensitive load protection against a number of voltage interference at PCC bus. The control strategy algorithm of the source and load voltage in series active filter circuit is shown in Figure 5. It extracts the unit vector templates from the distorted input supply. Furthermore, the templates are expected to be ideal sinusoidal signal with unity amplitude. The distorted supply voltages are measured and divided by peak amplitude of fundamental input voltage V_m given in (10) [6].

$$V_m = \sqrt{\frac{2}{3}} \left(V_{sa}^2 + V_{sb}^2 + V_{sc}^2 \right) \tag{10}$$

A three phase locked loop (PLL) is used in order to generate a sinusoidal unit vector templates with a phase lagging by the use of sinus function. The reference load voltage signal is determined by multiplying the unit vector templates with the peak amplitude of the fundamental input voltage V_m . The load reference voltage (V_{La}^* , V_{Lb}^* , V_c^*) is then compared against to sensed load voltage (V_{La} , V_{Lb} , V_{Lc}) by a pulse width modulation (PWM) controller used to generate the desired trigger signal on series active filter.



Figure 5. Control strategy of series active filter

2.5. Control of Shunt Active Filter

The main function of shunt active filter is migitation of power quality problems on the load side. The control methodology in shunt active filter is that the absorbed current from the PCC bus is a balanced positive sequence current including unbalanced sag voltage conditions in the PCC bus or unbalanced conditions or non-linear loads. In order to obtain satisfactory compensation caesed by disturbance due to non-linear load, many algorithms have been used in the literature. This research used instantaneous reactive power theory method "p-q theory". The voltages and currents in Cartesian *abc* coordinates can be transformed to Cartesian $\alpha\beta$ coordinates as expressed in (11) and (12) [6].

$$\begin{bmatrix} v_{\alpha} \\ v_{\beta} \end{bmatrix} = \begin{bmatrix} 1 & -1/2 & -1/2 \\ 1 & \sqrt{3}/2 & -\sqrt{3}/2 \end{bmatrix} \begin{bmatrix} V_{a} \\ V_{b} \\ V_{c} \end{bmatrix}$$
(11)
$$\begin{bmatrix} i_{\alpha} \\ i_{\beta} \end{bmatrix} = \begin{bmatrix} 1 & -1/2 & -1/2 \\ 1 & \sqrt{3}/2 & -\sqrt{3}/2 \end{bmatrix} \begin{bmatrix} i_{La} \\ i_{Lb} \\ i_{Lc} \end{bmatrix}$$
(12)

The computation of the real power (p) and imaginary power (q) is showed in (13). The real power and imaginary are measured instantaneously power and in matrix it is form is given as. The presence of oscillating and average components in instantaneous power is presented in (14) [17].

$$\begin{bmatrix} p \\ q \end{bmatrix} = \begin{bmatrix} v_{\alpha} & v_{\beta} \\ -v_{\beta} & v_{\alpha} \end{bmatrix} \begin{bmatrix} i_{\alpha} \\ i_{\beta} \end{bmatrix}$$

$$p = \overline{p} + \widetilde{p} \quad ; \quad q = \overline{q} + \widetilde{q} \tag{13}$$

Where \overline{p} = direct component of real power, \widetilde{p} = fluctuating component of real power, \overline{q} = direct component of imaginary power, \widetilde{q} = fluctuating component of imaginary power. The total imaginary power (q) and the fluctuating component of real power are selected as power references and current references and are utilized through the use of (15) for compensating harmonic and reactive power [18].

$$\begin{bmatrix} i_{c\alpha}^{*} \\ i_{c\beta}^{*} \end{bmatrix} = \frac{1}{v_{\alpha}^{2} + v_{\beta}^{2}} \begin{bmatrix} v_{\alpha} & v_{\beta} \\ v_{\beta} & -v_{\alpha} \end{bmatrix} \begin{bmatrix} -\widetilde{p} + \overline{p}_{loss} \\ -q \end{bmatrix}$$
(15)

The signal \bar{p}_{loss} , is obtained from voltage regulator and is utilized as average real power. It can also be specified as the instantaneous active power which corresponds to the resistive loss and switching loss of the UPQC. The error obtained on comparing the actual DC-link capacitor voltage with the reference value is processed in FLC, engaged by voltage control loop as it minimizes the steady state error of the voltage across the DC link to zero. The compensating currents $(i_{ca}^*, i_{c\beta}^*)$ as required to meet the power demand of load are shown in (15). These currents are represented in α - β coordinates. The phase current required to acquire using (16) for compensation. These source phase currents $(i_{sa}^*, i_{sb}^*, i_{sc}^*)$ are represented in a-b-c axis obtained from the compensating current in the α - β coordinates presented in (16) [18].

$$\begin{bmatrix} \dot{i}_{sa} \\ \dot{i}_{sb}^{*} \\ \dot{i}_{sc}^{*} \end{bmatrix} = \sqrt{\frac{2}{3}} \begin{bmatrix} 1 & 0 \\ -1/2 & \sqrt{3}/2 \\ -1/2 & -\sqrt{3}/2 \end{bmatrix} \begin{bmatrix} \dot{i}_{ca}^{*} \\ \dot{i}_{c\beta}^{*} \end{bmatrix}$$
(16)

Figure 6 shows a control of shunt active filter.



Figure 6. Control strategy of shunt active filter

The proposed model of UPQC-BES system supplied by PV/wind/PV-wind hybrid is shown in Figure 1. From the figure, we can see that PV is connected to the DC link through a DC-DC boost converter circuit. The PV partially distributes power to the load and the remains is transfered to three phase grid. The load consists of non linear and unbalanced load. The non-linear load is a diode rectifier circuit with the RL load type, while the unbalanced load is a three phase RC load with different R value on each phase. To be economically efficient, PV must always work in MPP condition. In this research, MPPT method used is P and O algorithm. The model is also applied for UPQC-BES system which is supplied by wind/PV-wind hybrid. In order to operate properly, UPQC-BES system device must have a minimum DC link voltage (V_{dc}). The value of common DC link voltage depends on the nstantaneous energy avialable to UPQC is defined by in (17) [16]:

$$V_{dc} = \frac{2\sqrt{2} V_{LL}}{\sqrt{3}m} \tag{17}$$

where m is modulation index and V_{LL} is the AC grid line voltage of UPQC. Considering that modulation index as 1 and for line to line grid voltage ($V_{LL} = 380$ volt), the V_{dc} is obtained 620,54 volt and selected as 650 volt.

The input of shunt active filter showed in Figure 5 is DC voltage (V_{dc}) and reference DC voltage (V_{dc}^*), while the output is \overline{p}_{loss} by using PI controller. Then, the \overline{p}_{loss} is as one of input variable to generate the reference source current (I_{sa}^* , I_{sb}^* , and I_{sc}^*). The reference source current output is then compared to source current (I_{sa} , I_{sb} , and I_{sc}) by the current hysteresis control to generate trigger signal in IGBT circuit of shunt active filter. In this research, FLC as DC voltage control algorithm on shunt active filter is proposed and compared with PI controller. The FLC is capable of reduce oscilation and generate quick convergence calculation during disturbances. This method is also used to overcome the weakness of PI controller in determining proportional gain (K_p) and integral gain constant (K_i) which still use trial and error method.

2.6. Fuzzy Logic Controller

The research is started by determine \overline{p}_{loss} as the input variable to result the reference source current on current hysteresis controller to generate trigger signal on the IGBT shunt active filter of UPQC using PI controller (K_p = 0.2 and K_i = 1.5). By using the same procedure, \overline{p}_{loss} is also determined by using FLC. The FLC has been widely used in recent industrial processes because it has heuristic, simpler, more effective and has multi rule based variables in both linear and non-linear system variations. The main components of FLC are fuzzification, decision making (rulebase, database, reason mechanism) and defuzzification in Figure 7.



The fuzzy rule algorithm collects a number of fuzzy control rules in a particular order. This rule is used to control the system to meet the desired performance requirements and they are designed from a number of intelligent system control knowledge. The fuzzy inference of FLC using Mamdani method related to max-min composition. The fuzzy inference system in FLC consists of three parts: rule base, database, and reasoning mechanism [19]. The FLC method is performed by determining input variables V_{dc} (V_{dc-error}) and delta Vdc ($\Delta V_{dc-error}$), seven linguistic fuzzy sets, operation fuzzy block system (fuzzyfication, fuzzy rule base and defuzzification), $V_{dc-error}$ and $\Delta V_{dc-error}$ during fuzzification process, fuzzy rule base table, crisp value to determine \overline{p}_{loss} in defuzzification phase. The \overline{p}_{loss} is one of input variable to obtain compensating currents $(i_{c\alpha}^*, i_{c\beta}^*)$ in (16). During fuzzification process, a number of input variables are calculated and converted into linguistic variables based on a subset called membership function. The error Vdc (V_{dc-error}) and delta error Vdc ($\Delta V_{dc-error}$) are proposed input variable system and output variable is \bar{p}_{loss} . To translate these variables, each input and output variable is designed using seven membership functions: Negative Big (NB), Negative Medium (NM), Negative Small (NS), Zero (Z), Positive Small (PS), Positive Medium (PM) and Positive Big (PB). The membership functions of crisp input and output are presented with triangle and trapezoid membership functions. The value of V_{dc-error} range from -650 to 650, $\Delta V_{dc-error}$ from -650 to 650, and \overline{p}_{loss} from -100 to 100. The input and output MFs are shown in Figure 8.



Figure 8. Membership functions (a) $V_{dc-error}$, (b) $\Delta V_{dc-error}$, and (c) \overline{p}_{loss}

After the V_{dc-error} and $\Delta V_{dc-error}$ are obtained, then two input membership functions are converted to linguistic variables and uses them as input functions for FLC. The output membership function is generated using inference blocks and the basic rules of FLC as shown in Table 1. Finally the defuzzification block operates to convert generated \bar{p}_{loss} output from linguistic to numerical variable again. Then it becomes input variable for current hysteresis controller to produce trigger signal on the IGBT circuit of UPQC shunt active filter to reduce source current and load voltage harmonics. While simultaneously, it also improve power quality of 3P3W system under six scenarios due to the integration of PV/wind/PV-wind hybrid to UPQC-BES system.

3. RESULTS AND ANALYSIS

The analysis of proposed model is investigated through determination of six disturbance scenarios i.e. (1) NL, (2) Unba-NL, (3) Dis-NL, (4) Sag-NL, (5) Swell-NL, and (6) Inter-NL. Scenario 1, the model is connected a non-linear load with R_L and L_L of 60 Ohm and 0.15 mH respectively. Scenario 2, the model is connected to non-linear load and during 0.3 s since t = 0.2 s to t = 0.5 s connected to unbalance three phase load with R_1 , R_2 , R_3 as 6 Ohm, 12 Ohm, 24 Ohm respectively, and value of C_1 , C_2 , C_3 as 2200 μ F. Scenario 3, the model is connected to non-linear load and source voltage generating 5th and 7th harmonic components with individual harmonic distortion values of 5% and 2% respectively. Scenario 4, the model is connected to non-linear load and source experiences a sag voltage disturbance of 50% for 0.3 s between t = 0.2 s to t = 0.5 s to t =

s. Scenario 5, the model is connected to a non-linear load and source experiences a swell voltage disturbance of 50% for 0.3 s between t = 0.2 s to t = 0.5 s. Scenario 6, the model is connected to non-linear load and source experiences an interruption voltage interference of 100% for 0.3 s between t = 0.2 s to t = 0.5 S. Each scenario of UPQC uses PI controller and FLC so total number of disturbance are 12 scenarios. By using Matlab/Simulink, the model is then executed according to the desired scenario to obtain curve of source voltage (V_s), load voltage (V_L), compensation voltage (V_c), source current (V_s), load current (I_L), and DC voltage DC link (V_{dc}). Then, THD value of source voltage, source current, load voltage, and load current in each phase as well as average THD value (Avg THD) are obtained base on the curves. THD in each phase is determined in one cycle started at t = 0.35 s. The results of average of source voltage, source current, load voltage, and load current of 3P3W system using UPQC-BES system supplied by PV/wind/PV-wind hybrid are presented in Table 2, 3, and 4. Next THD in each phase and average THD are showed in Table 5, 6 and 7. Table 2. Voltage and Current of 3P3W System Using UPQC-BES System Supplied by PV/

		1 a0	IC 2. VOI	lage and	Current	101512	Ju Sys	CIII USI	ng OI (ZC-DL	system	Supplie	ubyiv			
Scenarios	:	Source Volta	ige Vs (Volt)		I	load Volta	ge V _L (Vol	t)	S	ource Curr	ent Is (Ampe	ere)	L	oad Current	I _L (Ampere)	
Secharios	Ph A	Ph B	Ph C	Avg	Ph A	Ph B	Ph C	Avg	Ph A	Ph B	Ph C	Avg	Ph A	Ph B	Ph C	Avg
							PI C	Controller								
1. NL	309.6	309.6	309.6	309.6	307.6	307.8	307.7	307.7	7.766	7.793	7.759	7.773	8.528	8.529	8.533	8.530
Unba-NL	307.4	308.0	308.0	307.8	308.3	308.7	308.3	308.4	31.00	24.84	28.73	28.15	22.50	34.12	34.52	30.38
Dist-NL	309.6	309.6	309.6	309.6	313,8	314.3	317.4	317.4	7.897	7.919	7.867	7.895	8.748	8.704	8.785	8.746
Sag-NL	154.5	154.5	154.5	154.5	307.1	307.3	307.3	307.2	7.235	7.276	7.226	7.246	8.509	8.514	8.510	8.511
5. Swell-NL	464.7	464.7	464.7	464.7	308.6	308.7	308.6	308.6	7.979	7.980	7.964	7.975	8.550	8.553	8.554	8.553
6. Inter-NL	0.5359	1.385	0.8501	0.9238	310.2	259.8	290.2	286.7	7.392	12.67	6.045	8.703	8.707	7.747	7.637	8.031
							Fuzzy Lo	gic Contro	oller							
1. NL	309.5	309.5	309.5	309.5	307.7	307.9	307.7	307.8	8.420	8.426	8.416	8.421	8.527	8.532	8.531	8.530
Unba-NL	307.4	307.9	308.0	307.8	308.5	308.7	308.4	308.5	31.66	25.50	29.36	28.84	22.52	34.11	35.52	30.72
3. Dist-NL	309.6	309.5	309.5	309.5	313.4	312.9	315.9	314.1	8.516	8.565	8.496	8.526	8.741	8.677	8.736	8.718
Sag-NL	154.4	154.4	154.4	154.4	307.3	307.3	307.2	307.3	8.563	8.560	8.561	8.561	8.514	8.517	8.512	8.515
5. Swell-NL	464.6	464.6	464.6	464.6	308.6	308.8	308.6	308.7	8.396	8.389	8.389	8.392	8.552	8.556	8.554	8.554
6. Inter-NL	0.4467	0.3918	0.3801	0.4062	314.0	293.4	304.9	304.1	4.024	3.778	3.608	3.804	8.874	8.195	8.193	8.421

Table 3. Voltage and Current of 3P3W System Using UPQC-BES System supplied by Wind

Samerica	:	Source Volta	ge Vs (Volt)		L	oad Volta	ge V _L (Vol	t)	S	ource Curre	ent Is (Ampe	ere)	L	oad Current	IL (Ampere)	
Scenarios	Ph A	Ph B	Ph C	Avg	Ph A	Ph B	Ph C	Avg	Ph A	Ph B	Ph C	Avg	Ph A	Ph B	Ph C	Avg
							PI C	Controller								
1. NL	309.5	309.6	309.6	309.6	308.6	308.6	308.2	308.5	7.863	7.875	7.840	7.869	8.554	8.553	8.546	8.551
Unba-NL	307.4	308.0	308.0	308.0	308.9	309.2	308.7	308.9	31.07	24.97	28.81	28.28	2255	34.17	34.57	30.43
3. Dist-NL	309.6	309.5	309.6	309.6	312.9	312.9	315.4	313.8	7.993	8.015	7.947	7.985	8.817	8.682	8.741	8.747
Sag-NL	154.5	154.5	154.5	154.5	308.0	308.1	307.8	307.9	7.428	7.455	7.368	7.417	8.527	8.535	8.532	8.531
5. Swell-NL	464.7	464.7	464.7	464.7	309.3	309.3	309.0	309.2	8.015	8.020	8.002	8.012	8.564	8.573	8.568	8.568
6. Inter-NL	1.256	1.022	0.592	0.957	234.0	316.4	274.0	274.8	11.27	9.866	7.028	9.388	5.958	8.697	8.204	7.619
							Fuzzy Lo	gic Contro	oller							
1. NL	309.5	309.5	309.5	309.5	308.5	308.6	308.3	308.5	8.418	8.410	8.414	8.414	8.545	8.552	8.549	8.549
2. Unba-NL	307.4	307.9	308.0	307.8	309.0	309.3	308.9	309.1	31.64	25.47	29.34	28.82	22.56	34.18	34.59	30.44
3. Dist-NL	309.5	309.5	309.5	309.5	313.2	313.7	314.1	313.7	8.519	8.531	8.531	8.527	8.713	8.714	8.718	8.715
Sag-NL	154.4	154.4	154.4	154.4	308.0	308.1	307.7	307.9	8.557	8.539	8.561	8.552	8.528	8.541	8.525	8.531
5. Swell-NL	464.6	464.7	464.7	464.7	309.2	309.3	309.2	309.2	8.391	8.385	8.388	8.388	8.565	8.570	8.567	8.567
6. Inter-NL	0.3563	0.3957	0.3963	0.3828	303.7	300.0	315.3	306.4	3.358	3.464	3.542	3.420	8.557	8.418	8.731	8.569

Table 4. Voltage and Current of 3P3W System Using UPQC-BES System Supplied PV-Wind Hybrid

Commiss		Source Volta	ge V _S (Volt)		I	.oad Voltag	ge V _L (Vol	t)	S	ource Curr	ent Is (Ampe	ere)	L	oad Current	IL (Ampere)	
Scenarios	Ph A	Ph B	Ph C	Avg	Ph A	Ph B	Ph C	Avg	Ph A	Ph B	Ph C	Avg	Ph A	Ph B	Ph C	Avg
							PI C	Controller								
1. NL	309.6	309.6	309.6	309.6	307.8	308.0	307.7	307.8	7.790	7.802	7.770	7.787	8.527	8.537	8.533	8.533
Unba-NL	307.4	308.0	308.0	307.8	308.4	308.8	308.4	308.6	31.02	24.87	28.74	28.21	22.52	34.13	34.53	31.40
3. Dist-NL	309.6	309.5	309.6	309.6	314.0	315.5	316.9	315.5	7.942	7.939	7.918	7.933	8.739	8.750	8.783	8.757
Sag-NL	154.5	154.5	154.5	154.5	307.3	307.4	307.2	307.3	7.289	7.309	7.251	7.283	8.513	8.516	8.515	8.515
5. Swell-NL	464.7	464.7	464.7	464.7	308.7	308.9	308.7	308.8	7.985	7.985	7.975	7.982	8.552	8.558	8.558	8.556
6. Inter-NL	1.048	0.825	0.8447	0.9059	247.5	300.7	303.7	283.9	5.119	5.927	9.271	6.773	7.016	7.893	8.793	7.867
							Fuzzy Lo	gic Contro	oller							
1. NL	309.5	309.5	309.5	309.5	307.8	308.0	307.7	307.8	8.419	8.418	8.409	8.413	8.529	8.539	8.533	8.534
Unba-NL	307.4	307.9	308.0	307.8	308.7	308.7	308.9	308.8	31.66	25.47	29.32	28.82	22.54	34.13	34.56	30.41
Dist-NL	309.5	309.5	309.5	309.5	314.4	315.5	316.6	315.5	8.581	8.593	8.568	8.581	8.761	8.722	8.761	8.748
Sag-NL	154.4	154.4	154.4	154.4	307.3	307.5	307.3	307.4	8.566	8.572	8.563	8.567	8.511	8.520	8.519	8.517
5. Swell-NL	464.6	464.6	464.6	464.6	308.8	308.8	308.7	308.8	8.391	8.394	8.396	8.394	22.33	22.35	22.36	22.35
6. Inter-NL	0.4178	0.4027	0.4020	0.4175	311.6	295.7	310.4	305.9	3.774	3.544	3.593	3.640	8.855	8.321	8.288	8.488

Table 2 shows UPQC-BES system supplied PV connected 3P3W system using PI and FLC, disturbance scenarios 1 to 5 produce an average load voltage above 307 V. While in scenario 6, FLC produces a higher average load voltage of 304.1 V than if using a PI of 286.7 V. If reviewed from average source current with PI, the highest and lowest average source currents are generated by disturbance scenarios 2 and 4 of 28.15 A and 7,246 A. Whereas if using FLC the highest and lowest average source currents are achieved in scenario 2 and 6 of 28.84 A and 3,804 A. Table 3 presents UPQC-BES supplied by wind connected to 3P3W with PI and FLC, scenarios 1 to 5 is capable of result a stable load voltage above 308 V. The difference is that in scenario 6, PI generates a load voltage of 274.8 V, otherwise if using FLC, load voltage increases to 306.4 V.

If reviewed from source current using PI, the highest and lowest average source currents are resulted by scenarios 2 and 4 of 28.28 A and 7.417 A. Rather, if using FLC, the highest and lowest average source currents are achieved in scenario 2 and 6 of 28.82 A and 3,420 A. Table 4 shows UPQC-BES supplied PV-wind hybrid connected 3P3W using PI and FLC, scenarios 1 to 5 produce an average load voltage above 307 V. While in scenario 6, FLC generates an average load voltage 305.9 V higher than if using PI control of 283.9 V. If reviewed from average source current with PI, the highest and lowest average source currents are resulted by scenarios 2 and 4 of 28.21 A and 6,773 A. Otherwise if using FLC the highest and lowest average source currents are achieved in scenario 2 and 6 of 28.82 A and 3,640 A respectively.

Table 5.	Harmonics	of 3P3W	System	Using	UPOO	C-BES S	vstem Su	applied	by PV
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Scenarios		Source Volta	ge THD (%)		L	oad Voltag	ge THD (%	5)		Source Curre	ent THD (%)		Load Cur	rent (%)	
Scenarios	Ph A	Ph B	Ph C	Avg	Ph A	Ph B	Ph C	Avg	Ph A	Ph B	Ph C	Avg	Ph A	Ph B	Ph C	Avg
							PI Co	ontroller								
1. NL	2.35	2.36	2.32	2.34	2.48	2.50	2.46	2.48	12.89	12.72	12.92	12.84	22.32	22.34	22.32	22.33
Unba-NL	2.29	2.20	2.24	2.24	2.43	2.23	2.37	2.34	2.660	2.330	2.240	2.410	5.230	2.070	2.660	3.320
3. Dist-NL	5.84	5.86	5.94	5.88	6.36	5.90	6.58	6.28	12.75	12.64	13.06	12.82	21.92	22.16	22.33	22.14
Sag-NL	4.69	4.75	4.81	4.75	2.46	2.48	2.53	2.49	14.26	13.96	14.16	14.13	22.28	22.31	22.28	22.29
5. Swell-NL	1.56	1.53	1.55	1.55	2.47	2.43	2.45	2.45	12.51	12.36	12.44	12.44	22.34	22.32	22.32	22.33
6. Inter-NL	NA	NA	NA	NA	32.11	15.09	28.54	25.25	270.90	145.89	275.67	230.82	47.70	34.58	36.29	39.53
						F	uzzy Log	ic Contr	oller							
1. NL	2.35	2.33	2.35	2.34	2.48	2.46	2.49	2.47	11.83	11.82	11.84	11.83	22.33	22.32	22.33	22.33
Unba-NL	2.25	2.27	2.20	2.24	2.39	2.41	2.34	2.38	2.620	2.400	2.220	2.413	5.230	2.100	2.640	3.323
3. Dist-NL	5.83	5.88	5.93	5.88	6.23	5.93	6.69	6.28	11.83	11.90	12.14	11.96	21.84	22.34	22.53	22.24
Sag-NL	4.71	4.76	4.79	4.75	2.46	2.48	2.50	2.48	11.91	11.88	11.86	11.89	22.27	22.32	22.32	22.31
5. Swell-NL	1.55	1.54	1.54	1.54	2.45	2.44	2.46	2.45	11.90	11.84	11.85	11.86	22.36	22.33	22.35	22.35
6. Inter-NL	NA	NA	NA	NA	13.05	6.60	11.15	10.27	30.61	34.72	31.57	32.30	24.25	24.25	24.71	24.40

Table 6. Harmonics of 3P3W System Using UPQC-BES System Supplied by Wind

Companies		Source Volta	ge THD (%)		L	oad Voltag	ge THD (%	5)		Source Curr	ent THD (%)		Load Cur	rent (%)	
Scenarios	Ph A	Ph B	Ph C	Avg	Ph A	Ph B	Ph C	Avg	Ph A	Ph B	Ph C	Avg	Ph A	Ph B	Ph C	Avg
							PI Co	ontroller								
1. NL	1.88	1.87	1.94	1.89	1.99	1.97	2.05	2.00	12.63	12.37	12.70	12.57	12.30	12.30	12.34	12.31
Unba-NL	1.83	1.76	1.82	1.80	1.92	1.85	1.93	1.90	2.46	2.07	2.20	2.24	5.26	2.07	2.69	3.34
3. Dist-NL	5.67	5.71	5.77	5.72	6.00	6.83	6.02	6.28	12.48	12.26	12.66	12.47	22.01	22.12	22.08	22.07
Sag-NL	3.76	3.86	3.86	1.83	1.97	2.02	2.03	2.01	13.59	13.17	13.51	13.42	22.29	22.31	22.30	22.30
5. Swell-NL	1.26	1.24	1.29	1.26	1.99	1.97	2.05	2.00	12.31	12.20	12.31	12.27	22.36	22.33	22.37	22.35
6. Inter-NL	NA	NA	NA	NA	14.09	35.59	34.73	28.14	157.76	139.01	266.07	186.95	37.6	34.39	46.97	39.65
						F	uzzy Log	ic Contr	oller							
1. NL	1.89	1.88	1.93	1.90	1.99	1.98	2.04	2.00	11.71	11.72	11.77	11.73	22.34	22.31	22.32	22.32
Unba-NL	1.85	1.79	1.78	1.81	1.95	1.87	1.88	1.90	2.43	2.11	2.12	2.22	5.24	2.07	2.70	3.24
3. Dist-NL	5.67	5.71	5.78	5.72	5.99	6.39	6.13	6.17	11.72	11.62	11.90	11.75	22.08	21.94	22.47	22.16
Sag-NL	3.79	3.81	3.86	3.82	1.97	1.99	2.03	1.99	11.72	11.69	11.74	11.72	22.28	22.30	22.35	22.31
5. Swell-NL	1.27	1.24	1.28	1.26	2.00	1.96	2.04	2.00	11.66	11.76	11.76	11.73	22.31	22.33	22.35	22.33
6. Inter-NL	NA	NA	NA	NA	7.59	6.44	10.95	8.33	27.33	28.27	26.39	27.33	25.39	23.65	24.31	24.45

Table 7. Harmonics of 3P3W System Using UPQC-BES System Supplied by PV-Wind Hybrid

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Commiss		Source Volta	ge THD (%)		L	oad Voltag	ge THD (%)		Source Curre	ent THD (%)		Load Cur	rent (%)	
Scenarios	Ph A	Ph B	Ph C	Avg	Ph A	Ph B	Ph C	Avg	Ph A	Ph B	Ph C	Avg	Ph A	Ph B	Ph C	Avg
							PI Co	ontroller								
1. NL	2.25	2.19	2.29	2.24	2.37	2.31	2.42	3.37	12.85	12.62	12.74	12.74	22.33	22.31	22.34	22.33
Unba-NL	2.18	2.08	2.15	2.13	2.30	2.19	2.18	2.22	2.63	2.30	2.29	2.407	5.23	2.07	2.67	3.323
3. Dist-NL	5.81	5.82	5.89	5.84	6.12	5.88	6.75	6.25	12.71	12.63	12.98	12.77	22.05	22.13	22.54	22.24
Sag-NL	4.53	4.48	4.51	4.51	2.37	2.35	2.37	2.36	14.16	13.50	13.99	13.88	22.27	22.30	22.28	22.28
5. Swell-NL	1.49	1.46	1.51	1.49	2.37	2.31	2.40	2.36	12.43	12.29	12.41	12.38	22.34	22.32	22.33	22.33
6. Inter-NL	NA	NA	NA	NA	18.61	36.38	28.42	27.8	387.71	330.34	189.29	302.45	36.73	38.51	36.83	37.36
						F	uzzy Log	ic Contr	oller							
1. NL	2.25	2.23	2.25	2.24	2.37	2.35	2.39	2.37	11.85	11.74	11.84	11.81	22.32	22.31	22.33	22.32
Unba-NL	2.23	2.15	2.05	2.14	2.37	2.26	2.17	2.26	2.52	2.41	2.14	2.446	5.23	2.07	2.69	3.330
3. Dist-NL	5.80	5.83	5.90	5.84	6.57	5.26	7.06	6.29	11.83	11.78	12.24	11.95	22.15	22.23	22.95	22.44
Sag-NL	4.53	4.52	4.54	4.86	2.36	2.35	2.35	2.35	11.79	11.74	11.84	11.79	22.29	22.30	22.29	22.29
5. Swell-NL	1.48	1.46	1.51	1.48	2.35	2.32	2.40	2.35	11.78	11.81	11.81	11.80	22.33	22.35	22.36	22.35
6. Inter-NL	NA	NA	NA	NA	10.30	4.90	10.25	8.48	27.44	29.52	28.63	28.53	23.20	23.97	24.65	23.94

Table 5 shows that average THD of load voltage (V_L) of UPQC-BES system supplied by PV in 3P3W system for scenarios 1 to 5 using PI control is within limits in IEEE 519. The highest and lowest average THD load voltages are achieved under scenario 6 and 2 as 25.25% and 2.34% respectively. PI controller is also able to migitate average THD source voltage in scenario 6 from not accessible (NA) to 25.25% on the load side. The highest and lowest average THD of source current are achieved in scenario 6 and 2 as 230.82% and 2.41%. Table 5 also indicates that average THD of load voltage of UPQC system supplied by PV with BES using FLC in scenarios 1 to 5, has fulfilled limits in IEEE 519. The highest and lowest average THD of load voltage are achieved under scenario 6 and 2 of 10.27% and 2.38%. The use of FLC method is also able to reduce average THD on source voltage in scenario 6 from NA to 10.27% on load side. The highest and lowest average THD of source current are achieved in scenario 6 and 2.413%.

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Table 6 presents that average THD of load voltage of UPQC-BES system supplied by wind in 3P3W system for interference scenarios 1 to 5 using PI is within limits prescribed in IEEE 519. The highest and lowest average THD load voltages is achieved under scenario 6 and scenario 2 as 28.14% and 1.90% respectively. PI controller is also able to reduce average THD source voltage in scenario 6 from NA to 28.14% on the load side. The highest and lowest average THD of source current are achieved in scenario 6 and 2 as 186.95% and 2.24% respectively. Table 6 also shows that average THD of load voltage of UPQC-BES supplied by wind using FLC in scenarios 1 to 5, has fulfilled limits prescribed in IEEE 519. The highest and lowest average THD of load voltage are achieved under scenario 6 and 4 of 8.33% and 1.90%. FLC method is also able to reduce average THD on source voltage in scenario 6 from NA to 7.33% on load side. The highest and lowest average THD source current are achieved in scenario 6 and 2 of 27.33% and 2.22%. Table 7 represents that average THD of load voltage (VL) of UPQC-BES system supplied by PV-wind hybrid in 3P3W system for scenarios 1 to 5 using PI is within limits in IEEE 519. The highest and lowest average THD load voltages are achieved under scenario 6 and 2 as 27.8% and 2.22% respectively. PI is also able to migitate average THD source voltage in scenario 6 from NA to 27.8% on load side. The highest and lowest average THD of source current are achieved in scenario 6 and 2 as 302.45% and 2.407% respectively. Table 7 also indicates that average THD of load voltage of UPQC-BES system supplied by PV-wind hybrid using FLC for scenarios 1 to 5, has fulfilled limits in IEEE 519. The highest and lowest average THD of load voltage are achieved under scenario 6 and 2 of 8.48% and 2.26%. FLC method is also able to reduce average THD on source voltage in scenario 6 from NA to 8.48% on load side. The highest and lowest average THD of source current are achieved in scenario 6 and 2 of 28.53% and 2.446%. Overall for UPQC-BES system system supplied by PV/wind/PV-wind hybrid in scenarios 1 to 5 using PI and FLC is able to improve average THD of source current better on average THD of load current. Figure 9 presents UPQC-BES system performance supplied by PV/wind/PV-wind hybrid using FLC in scenario 6.



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Figure 9.a.(i) shows that in scenario 6, UPQC-BES system supplied by PV at t = 0.2 s to t = 0.5 s, average source voltage (V_S) falls as 100% to 0.4062 V. During the disturbance, PV is able to generate power to UPOC DC link and injecting full average compensation voltage (V_{C}) in Figure 9.a.(iii) through injection transformer on series active filter so that average load voltage (V_L) in Figure 9.a.(ii) remains stable at 304.1 V. As long as fault period, although nominal of average source current (I_s) in Figure 9.a.(iv) drops to 3.804 A, combination of PV and BES is able to generate power, store excess energy of PV, and inject current into load through shunt active filter so that average load current (I_L) in Figure 9.a.(v) remains as 8.421 A. Figure 9.b.(i) presents on UPQC-BES supplied by wind at t = 0.2 s to t = 0.5 s average source voltage (V_s) drops 100% to 0.3828 V. During the disturbance, wind is able to generate power to UPQC DC link and injecting full average compensation voltage (V_C) in Figure 9.b.(iii) through injection transformer on series active filter so that average load voltage (V_L) in Figure 9.b.(ii) remains stable at 306.4 V. During fault period, although nominal of average source current (I_s) falls to 3.420 A, combination of wind and BES is able to generate power, store excess energy of wind, and inject current into load through shunt active filter so that average load current (I_L) in Figure 9.b.(v) remains as 8.569 A. Figure 9.c.(i) indicates on UPQC-BES supplied by PV-Wind Hybrid at t = 0.2 s to t = 0.5 s average source voltage (V_s) drops 100% to 0.4175 V. During the disturbance, PV-wind hybrid is able to generate power to UPQC DC link and injecting full average compensation voltage (V_C) in Figure 9.c.(iii) through injection transformer on series active filter so that average load voltage (VL) in Figure 9.b.(ii) remains stable at 305.9 V. As long as disturbance period, although nominal of average source current (I_s) falls to 3.640 A, combination of PV-wind hybrid and BES is able to generate power, store excess energy of wind, and inject current into load through shunt active filter so that average load current (I_L) in Figure 9.c.(v) remains as 8.488 A. Figure 10 shows spectra of load voltage harmonics on phase A of UPQC-BES system supplied by PV/wind/PV-wind hybrid using FLC in scenario 6. Figure 11 shows performance of average THD of load voltage and source current on UPQC-BES system supplied by PV/wind/PV-wind hybrid.



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Figure 11(a) shows that in scenario 1 to 5, the implementation of FLC on UPQC-BES system supplied by PV/Wind/PV-Wind is able to result average THD of source voltage slightly better than PI controller and both method have already met the limit in IEEE 519. Further under scenario 6, FLC applied on UPQC-BES system supplied by PV/wind/PV-wind hybrid gives better significantly result of average THD of source voltage than PI controller. In six disturbance scenarios, both PI controller and FLC applied on UPQC-BES system supplied by PV/Wind/PV-Wind, PV is able to result the highest average THD of source voltages. Figure 11(b) presents that in disturbance scenario 1 to 5, implementation of FLC on UPQC-BES system supplied by PV/wind/PV-wind hybrid is able to result average THD of source current slightly better than PI controller. Furthermore under scenario 6, FLC applied on UPQC-BES system supplied by PV/wind/PV-wind hybrid is able to result average THD of source current slightly better than PI controller. Furthermore under scenario 6, FLC applied on UPQC-BES system supplied by PV/wind/PV-wind hybrid is able to result average THD of source current slightly better than PI controller. Furthermore under scenario 6, FLC applied on UPQC-BES system supplied by PV/wind/PV-wind hybrid gives better significantly result average THD of source voltage than PI controller. Both PI controller and FLC on UPQC-BES system supplied by PV/wind/PV-wind hybrid gives better significantly result average THD of source voltage than PI controller. Both PI controller and FLC on UPQC-BES system supplied by PV/wind/PV-wind hybrid gives better significantly result average THD of source voltage than PI controller. Both PI controller and FLC on UPQC-BES system supplied by PV/wind/PV-wind hybrid in six disturbance scenarios, PV is able to result the highest average THD of source current.

4. CONCLUSION

Comparative performance of UPQC-BES system supplied by PV/wind/PV-wind hybrid using PI controller and FLC have been discussed. In disturbance scenario 1 to 5, implementation of FLC on UPQC-BES system supplied by PV/wind/PV-wind hybrid with BES is able to result average THD of source voltage slightly better than PI and both methods have already met the limit in IEEE 519. Under scenario 6, FLC applied on UPQC-BES system supplied by PV/wind/PV-wind hybrid with BES give significantly better result average THD of source voltage than PI. In six disturbance scenarios, both PI and FLC applied on UPQC-BES system supplied by PV/wind/PV-wind hybrid is able to result the highest average THD of source voltage. In interference scenario 1 to 5, FLC method on UPQC-BES system supplied by PV/wind/and PV-wind hybrid is capable of result average THD of source current slightly better than PI. Furthermore under scenario 6, FLC applied on UPQC-BES system supplied by PV/wind/PV-wind hybrid gives significantly better result of average THD of source voltage than PI. Both PI and FLC on UPQC-BES system supplied by PV/wind/PV-wind hybrid gives significantly better result of average THD of source voltage than PI. Both PI and FLC on UPQC-BES system supplied by PV/wind/PV-wind hybrid gives significantly better result of average THD of source voltage than PI. Both PI and FLC on UPQC-BES system supplied by PV/wind/PV-wind hybrid in six scenarios, PV is able to result the highest average THD of source current.

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APPENDIX

Three phase grid: RMS voltage 380 volt (L-L), 50 Hz, line impedance: $R_s = 0.1$ Ohm $L_s = 15$ mH; series and shunt active filter: series inductance $L_{se} = 0.015$ mH; shunt inductance $L_{sh} = 15$ mH; injection transformers: rating 10 kVA, 50 Hz, turn ratio $(N_1/N_2) = 1:1$; non linear load: resistance $R_L = 60$ ohm, inductance $L_L = 0.15$ mH, load impedance $R_c = 0.4$ ohm and $L_c = 15$ mH; unbalance load: resistance $R_1 = 24$ ohm, $R_2 = 12$ ohm, and $R_3 = 6$ ohm, capacitance $C_1, C_2, C_3 = 2200 \ \mu\text{F}$; DC-link: voltage $V_{DC} = 650$ volt and capacitance $C_{DC} = 3000 \ \mu\text{F}$; battery energe storage: type = nickel metal hybrid, DC voltage = 650 volt, rated capacity = 200 Ah, initial SOC = 100%, inductance $L_1 = 6$ mH, capacitance $C_1 = 200 \ \mu\text{F}$; photovoltaic: active power = 0.6 kW temperature = 25^o C, irradiance = 1000 W/m²; PMSG wind turbine active power = 0.6 kW, voltage = 380 volt, 50 Hz, wind speed = 5 m/s, picth angle = 2; PI controller: $K_p = 0.2$, $K_i = 1.5$; fuzzy model: method = mamdani, composition = max-min; input membership function: error (V_{dc}) = trapmf, trimf; output membership function: \bar{p}_{loss} = trapmf,trimf.

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Lampiran 2.2 Review makalah dari editor

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Matlab/Simulink Simulation of Unified Power Quality Conditioner-Battery Energy Storage System Supplied by PV-Wind Hybrid usingFuzzy Logic Controller

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Article Info	ABSTRACT
Article history: Received Jun 12 th , 201x Revised Aug 20 th , 201x Accepted Aug 26 th , 201x	This paper presents performance analysis of Unified Power Quality Conditioner-Battery Energy Storage (UPQC-BES) system supplied by Photovoltaic (PV)-Wind Hybrid connected to three phase three wire (3P3W) of 380 volt (L-L) and 50 hertz distribution system. The performance of supply system is compared with two renewable energy (RE) sources i.e. PV and Wind, respectively. Fuzzy Logic Controller (FLC) is implemented to
Keyword: Power Quality UPQC Battery Energi Storage Photovoltaic Wind Turbine PV-Wind Hybrid Total Harmonic Distortion	maintain DC voltage across the capacitor under disturbance scenarios of source and load as well as to compare the results with Proportional Intergral (PI) controller. There are six scenarios of disturbance i.e. (1) non-linear load (NL), (2) unbalance and nonlinear load (Unba-NL), (3) distortion supply and non-linear load (Dis-NL), (4) sag and non-linear load (Sag-NL), (5) swell and non-linear load (Swell-NL), and (6) interruption and non-linear load (Inter-NL). In disturbance scenario 1 to 5, implementation of FLC on UPQC-BES system supplied by three RE sources is able to obtain average THD of load voltage/source current slightly better than PI. Furthermore under scenario 6, FLC applied on UPQC-BES system supplied by three RE sources gives significantly better result of average THD of load voltage/source current than PI. This research is simulated using Matlab/Simulink.
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1. INTRODUCTION

PV and windare the most REdistributed generations (DGs) because they are able to convertsunlight and wind into power. PV and solararethepotential DGs sources since it only need sunlight to generate electricity, where the resources are available in abundance, free and relatively clean. Indonesia has enormous energy potential from the sunbecause it lies on the equator. Almost all areas of Indonesia get sunlight about 10 to 12 hours per day, with an average intensity of irradiation of 4.5 kWh/m² or equivalent to 112.000 GW. The potential of wind energy in Indonesia generally has a speed between 4 to 5 m/s and classified as medium scale with potential capacity of 10 to 100 kW. The weakness of PV and wind turbine besidesable to generate power, they also produces a number voltage and current harmonics resulted bypresence of several types of PV and wind turbine devices and power converters as well as to increase a number of non-linear loads connected to the grid, so finally resulting inthe decrease in power quality.

In order to overcome and improve power quality due to presence of non-linear loads and integration of PV and wind turbine to grid, UPQC is a proposed. UPQCserves to compensate for source voltage quality

problemsi.e. sag, swell unbalance, flicker, harmonics, and load current quality problems i.e. harmonics, unbalance, reactive currents, and neutral current, B. Han et, al and Vinod Khadkikar have investigated UPOC as one part of active power filter consisting of shunt and series active filters connected in parallel and serves as superior controller to overcome a number of power quality problems simultaneously. Series component has been responsible for reducing a number of interference on source side i.e. voltage sag/swell, flicker, unbalanced voltage, and harmonics. Shunt component has been responsible for addressing a current quality problems i.e. low power factor, load current harmonics, and unbalanced load. [1,2].UPQC based on RE has been investigated by some researchers. There are two methods used to overcome this problem i.e. using conventional and artificial intelligence.Shafiuzzaman K.K., et.al have proposed system includes a series inverter, shunt inverter, and a DG connected to a DC link through a rectifier using PI. The system was capable of increase source voltage quality i.e. sag and interruption and load current quality, as well as transfer of active power on/off grid mode [3]. The influence of DG on UPQC performance in reducing sag under conditions of some phase to ground faults to using DSTATCOM has been implemented byNorshafinash S., et.al.The DG was effective enough to help UPQC to improve sag [4]. It was connected in series with load resulting better sagmigitationcompared to system without DG. Implementation of UPQC using UVTG method with PI to reduce sag, swell, voltage/current harmonics has been doneby S. N. Gohil, et.al. Simulation of voltage distortion was made by adding 5^{th} and 7^{th} harmonics at fundamental source voltage, resulting in a reduction of THD source current and THD load voltage [5].

UPQC supplied byPV panels using boost converter, PI, MPPT P and O, and p-q theoryhas been proposed byYahiaBouzelata at.al[6]. The system was capable of compensate reactive power and reduce source current/load voltage harmonics, butdid not discuss migitation of sag and interuption caused by PV penetration. Power quality enhancement of sag and source voltage harmonics on grid using UPQC supplied by PV array connected to DC link using PI compared with FLC has been done by Ramalengswara Rao, et.al. Combination of UPOC and PV using FLC can improve source voltage THD better than PI [7]. Amirullah et.al haveresearched a method for balancing current and line voltage, as a result of DGs of a single phase PV generator unit in randomly installed at homes through on a three phase four wire 220 kV and 50 Hz distribution line using BES and three of single phase bidirectional inverter. Both devices was capable of reduce unbalanced line current/voltage, but both of them were also capable of increase current/voltage harmonics on PCC bus [8]. Power quality migitation of UPQC on microgrid supplied by PV and wind turbine has been implemented by K S Srikanth et. al. It resulted that PI and FLC was able to improve power quality and reduce distortion in output power [9]. The UPQC-wind turbine to provide active power to overcome low sag and interruption voltage to grid has been investigated by H.Toodeji, et.al. The model was used VSC as a rectifier on generator output and controlled so that maximum power desired can be generated by different speed wind turbines using PI[10]. The UPQC-wind turbine connected to UPQC DC link was implemented by M. Hosseinpour, et al. The proposed combination using PI was capable of compensate swell, interruption voltage, and reactive power both on on/off grid [11]. R.Bhavani, et, al have researched on UPQC controlled by FLC to improve power quality in a DFIG wind turbine connected grid. FLC can improve power quality i.e. sag voltage and load current harmonics better than PI[12]. Power quality enhancement on wind turbine and BES with PI connected grid on PCC bus using UPQC has been implemented by S.RajeshRajan, et al. BES was installed to maintain and stabilize active power supply under different windspeed [13].

This researchwill analyze UPQC-BES performance supplied by PV-wind hybrid connected to 3P3W of 380 volt (L-L) and 50 hertz distribution system. The performance of supply system is compared with two RE sources i.e. PV and Wind, respectively. BES serves to store excess energy produced by three RE sources and distribute it to load if necessary, to prevent interruption voltage, and to adjust charging and discharging of energy in battery. BES is also expected to store excess power produced by three RE combinations and use it as backup power. FLC is proposed and compared with PI to control variable of DC voltage and DC reference voltage input to generate reference current source in current hysteresis controller on shunt active filter. DC voltage controller in shunt active filter and series active filter is used to migitate power quality of load voltage and source current. Performance of two controllers are used to determine load voltage, source current, load voltage THD, and source current THD based on IEEE 519. This paper is presented as follow. Section 2 describes proposed method, model of UPQC-BES system supplied by three RE sources i.e. PV, wind, and PV-wind hybrid, simulation parameters, PV and PMSG wind turbine model, series and shunt active filter, as well as application of PI and FLC method for proposed model. Section 3 shows results and analysis about performance of THD analysis on the proposed model of three RE sources connected to DC link of UPQC-BES system using PI and FLC. In this section, six disturbance scenarios are presented and the results are verified with Matlab/Simulink. Finally, this paper in concluded in Section 4.

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2. RESEARCH METHOD

2.1. Proposed Method

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Figure 1 shows proposed model in this research. The RE sources based DGs used i.e. PV, Wind Turbine, and PV-Wind Turbine Hybrid connected to 3P3W distribution system with 380 volt (L-L) and 50 Hz frequency, through UPQC-BES system. PV array produce power under fixed temperature and radiation as well as connect to UPQC-DC link through a DC/DC boost converter. The maximum power point tracking (MPPT) method with Pertub and Observer (P and O) algorithms helps PV produce maximum power and generate output voltage, as the input voltage for DC/DC boost converter. The converter serves to adjust dutycycle value and output voltage of PV as its input voltage to produce an output voltage corresponding to UPQC DC link voltage. Wind turbine type used is a permanent magnetic synchronous generator (PMSG) with variable speed and fixed voltage which generating power and is connected to UPQC DC link circuit through AC/DC bridge rectifier. The rectifier helps to change AC PSMG stator output voltage to DC voltage through LC circuit that serves to filter and smooth it before connected to UPQC-DC link.BES connected to the UPQC-DC link circuit serves as energy storage and is expected to overcome interruption voltage and overall help UPQC performance to improve voltage and current quality on source and load bus. Simulation parameters proposed in this study is shown in Appendix Section. Power quality analysis is performed on PV, Wind, PV-Wind Hybrid respectively, connected to 3P3W system through UPQC DC-link (on-grid) using BES circuit. Single phase circuit breakers (CBs) are used to connect and disconnect PV, Wind, and Hybrid PV-Wind respectively with UPOC DC-link.

There are six disturbance scenarios i.e.(1) NL, (2) Unba-NL, (3) Dis-NL, (4) Sag-NL, (5) Swell-NL, and (6) Inter-NL. In scenario 1, the model is connected a non-linear load with R_L and $L_L\,$ of 60 Ohm and 0.15 mH respectively. In scenario 2, the model is connected to non-linear load and during 0.3 s since t = 0.2 s to t = 0.5 s connected to unbalance three phase load with R_1 , R_2 , R_3 as 6 Ohm, 12 Ohm, 24 Ohm respectively, and value of C1, C2, C3 as 2200 µF. In scenario 3, the model is connected to non-linear load and source voltage generating 5th and 7th harmonic components with individual harmonic distortion values of 5% and 2% respectively. In scenario 4, the model is connected to non-linear load and source experiences a sag voltage disturbance of 50% for 0.3 s between t = 0.2 s to t = 0.5 s. In scenario 5, the model is connected to a nonlinear load and source experiences a swell voltage disturbance of 50% for 0.3 s between t = 0.2 s to t = 0.5 s. In scenario 6, the model is connected to non-linear load and source experiences an interruption voltage interference of 100% for 0.3 s between t = 0.2 s to t = 0.5 s.FLC is used as a DC voltage control in a shunt active filter to improve the power quality of the load voltage and current source and compare it with PI controller. Each disturbance scenario uses a PI controller and FLC so that the total of 12 disturbances. The result analysis of research was carried out i.e. (1) voltage and current on source or poin common coupling (PCC) bus, (2) voltage and current on load bus, (3) harmonic voltage and harmonic current on source bus and (4) harmonic voltage and harmonic current on load bus. The final phase is to compare performance of UPQC-BES system on-grid supplied by PV, Wind, PV-Wind Hybrid respectively using two controllers to improve power quality of load voltage and source current under six disturbance conditions.



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2.2. Photovoltaic Model

Figure 2 shows the equivalent circuit and V-I characteristic of a solar panel. A solar panel is composed of several PV cells that have series, parallel, or series-parallel external connections [14].



Figure 2. Equivalent circuit and V-I characteristic of solar panel

The V-I characteristic of a solar panel is showed in (1):

$$I = I_{PV} - I_o \left[\exp\left(\frac{V + R_s I}{a V_r}\right) - 1 \right] - \frac{V + R_s I}{R_p}$$
(1)

where I_{PV} is the photovoltaic current, I_o is saturated reverse current, 'a' is the ideal diode constant, $V_t = N_S K T q^{-1}$ is the thermal voltage, N_S is the number of series cells, q is the electron charge, K is the Boltzmann constant, T is the temperature of p–n junction, R_S and R_P are series and parallel equivalent resistance of the solar panels. I_{PV} has a linear relation with light intensity and also varies with temperature variations. I_o is dependent on temperature variations. The values of I_{PV} and I_o are calculated as following (2) and (3):

$$I_{PV} = (I_{PV,n} + K_1 \Delta T) \frac{G}{G} I$$
⁽²⁾

$$I_o = \frac{I_{SC,n} + K_I \Delta T}{\exp(V_{oC,n} + K_V \Delta T)/aV_v - 1}$$
(3)

In which $I_{PV,n}$, $I_{SC,n}$ and $V_{OC,n}$ are photovoltaic current, short circuit current and open circuit voltage in standard conditions ($T_n = 25$ C and $G_n = 1000$ Wm⁻²) respectively. K_I is the coefficient of short circuit current to temperature, $\Delta T = T - T_n$ is the temperature deviation from standard temperature, G is the light intensity and K_V is the ratio coefficient of open circuit voltage to temperature. Open circuit voltage, short circuit current and voltage-current corresponding to the maximum power are three important points of I-V characteristic of solar panel. These points are changed by variations of atmospheric conditions. By using (4) and (5) which are derived from PV model equations, short circuit current and open circuit voltage can be calculated in different atmospheric conditions.

$$I_{SC} = (I_{SC} + K_1 \Delta T) \frac{G}{G_n}$$
⁽⁴⁾

$$V_{OC} = V_{OC} + K_V \Delta T \tag{5}$$

2.3. PMSG Wind Turbine

Wind turbine is onother part of an integrated system, which can be divided into two types i.e. fixed and variable speed wind turbines. In fixed speed type, rotating speedof turbine is fixed and hence, frequency of generated voltage remains constant, so it can be directly connected to the network. In this case, maximum power can not always be extracted by wind. On the other hand, on variable speed, turbine can rotate at different speeds, so maximum power can be generated in each wind speed by MPPT method [10].The

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advantage of using a PMSG over a synchronous generator and DFIG machine because it has high efficiency and reliability. Due to the elimination of rotor external excitation, machine size,and cost also decreases, making PMSGto be more controlled easily with feedback control system. PMSG has become an attractive solution on wind generation systems with variable speed wind turbine applications [15]. Figure 3 and 4 shows model of PMSG wind turbine and wind turbinpower characteristiccurve.

3.4 m/s 3 m/s

1.4

1.2

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The output power of wind turbine can be expressed using (6), (7), and (8) [11].

ō

0.2

$$\lambda = \frac{\omega_r R}{V_{wind}}$$

$$P_{yx} = \frac{1}{\rho} \rho \pi R^2 C_z V_{wind}^3$$
(6)
(7)

0.4 0.6 0.8 1 Turbine speed (pu of nominal generator speed)

Figure 4. Wind turbin power characteristic curve

$$P_{M} = \frac{1}{2} \rho \pi R^{2} C_{p} V_{wind}^{3}$$
(7)
$$T_{m} = \frac{P_{M}}{2} \frac{1}{2} e^{\frac{1}{2} C_{p}} \frac{\omega_{M}^{3}}{\omega_{M}^{3}}$$
(8)

$$T_{M} = \frac{F_{M}}{\omega_{r}} = \frac{1}{2} \rho \pi R^{5} C_{p} \frac{\omega_{M}}{\lambda^{3}}$$
(8)

Where λ is the speed-tip ratio, V_{wind} is wind speed, R is blade radius, ω_r is rotor speed (rad/sec), ρ is the air density, C_P is the power coefficient, P_M is the output mechanical power, and T_M is output torque of wind turbine. The CP coefficient is dependent on the pitch angle value, at which rotor blade can rotate along axis and tip-speed ratio λ expressed in (9).

$$C_{p} = (0.44 - 0.167\beta)\sin\frac{\pi(\lambda - 2)}{(13 - 0.3\beta)}$$
(9)

Where β is a pitch angle blade. In a fixed pitch type, the value of β is set to a fixed value.

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2.4. Control of Series Active Filter

The main function of series active filter is as a sensitive load protection against a number of voltage interference at PCC bus. The control strategy algorithm of the source and load voltage in series active filter circuit is shown in Figure 5. It extracts the unit vector templates from the distorted input supply. Furthermore, the templates are expected to be ideal sinusoidal signal with unity amplitude. The distorted supply voltages are measured and divided by peak amplitude of fundamental input voltage V_m givenin (10) [6].

$$V_m = \sqrt{\frac{2}{3} \left(V_{sa}^2 + V_{sb}^2 + V_{sc}^2 \right)}$$
(10)

A three phase locked loop (PLL) is used in order to generate a sinusoidal unit vector templates with a phase lagging by the use of sinus function. The reference load voltage signal is determined by multiplying the unit vector templates with the peak amplitude of the fundamental input voltage V_m . The load reference voltage $(V_{La}^*, V_{Lb}^*, V_c^*)$ is then compared against to sensed load voltage (V_{La}, V_{Lb}, V_{Lc}) by a pulse width modulation (PWM) controller used to generate the desired trigger signal on series active filter.



Figure 5. Control strategy of series active filter

2.5. Control of Shunt Active Filter

The main function of shunt active filter is migitation of power quality problems on the load side. The control methodology in shunt active filter is that the absorbed current from the PCC bus is a balanced positive sequence current including unbalanced sag voltage conditions in the PCC bus or unbalanced conditions or non-linear loads. In order to obtain satisfactory compensation caesed by disturbance due to non-linear load, many algorithms have been used in the literature. This research used instantaneous reactive power theory method "p-q theory". The voltages and currents in Cartesian *abc*coordinates can be transformed to Cartesian $\alpha\beta$ coordinates as expressed in (11) and (12) [6].

$$\begin{bmatrix} v_{\alpha} \\ v_{\beta} \end{bmatrix} = \begin{bmatrix} 1 & -1/2 & -1/2 \\ 1 & \sqrt{3}/2 & -\sqrt{3}/2 \end{bmatrix} \begin{bmatrix} V_{a} \\ V_{b} \\ V_{c} \end{bmatrix}$$
(11)

$$\begin{bmatrix} i_{a} \\ i_{\beta} \end{bmatrix} = \begin{bmatrix} 1 & -1/2 & -1/2 \\ 1 & \sqrt{3}/2 & -\sqrt{3}/2 \end{bmatrix} \begin{bmatrix} i_{La} \\ i_{Lb} \\ i_{Lc} \end{bmatrix}$$
(12)

The computation of the real power (p) and imaginary power (q) is showed in (13). The real power and imaginary are measured instantaneously power and in matrix it is form is given as. The presence of oscillating and average components in instantaneous power is presented in (14) [17].

$$\begin{bmatrix} p \\ q \end{bmatrix} = \begin{vmatrix} v_{\alpha} & v_{\beta} \\ -v_{\beta} & v_{\alpha} \end{vmatrix} \begin{bmatrix} i_{\alpha} \\ i_{\beta} \end{bmatrix}$$
(13)

$$p = \overline{p} + \widetilde{p} \quad ; q = \overline{q} + \widetilde{q} \tag{14}$$

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Where \bar{p} = direct component of real power, \tilde{p} = fluctuating component of real power, \bar{q} = direct component of imaginary power, \tilde{q} = fluctuating component of imaginary power. The total imaginary power (q) and the fluctuating component of real power are selected as power references and current references and are utilized through the use of (15) for compensating harmonic and reactive power [18].

$$\begin{bmatrix} i_{c\alpha}^{*} \\ i_{c\beta}^{*} \end{bmatrix} = \frac{1}{v_{\alpha}^{2} + v_{\beta}^{2}} \begin{bmatrix} v_{\alpha} & v_{\beta} \\ v_{\beta} & -v_{\alpha} \end{bmatrix} \begin{bmatrix} -\widetilde{p} + \overline{p}_{loss} \\ -q \end{bmatrix}$$
(15)

The signal \bar{p}_{iss} , is obtained from voltage regulator and is utilized as average real power. It can also be specified as the instantaneous active power which corresponds to the resistive loss and switching loss of the UPQC. The error obtained on comparing the actual DC-link capacitor voltage with the reference value is processed in FLC, engaged by voltage control loop as it minimizes the steady state error of the voltage across the DC link to zero. The compensating currents $(i_{\alpha\alpha}^*, i_{c\beta}^*)$ as required to meet the power demand of load are shown in (15). These currents are represented in α - β coordinates. The phase current required to acquire using (16) for compensation. These source phase currents $(i_{x\alpha}^*, i_{x\beta}^*, i_{xc}^*)$ are represented in a-b-c axis obtained from the compensating current in the α - β coordinates presented in (16) [18].

$$\begin{bmatrix} \dot{i}_{sa} \\ \dot{i}_{sb}^* \\ \dot{i}_{sc}^* \end{bmatrix} = \sqrt{\frac{2}{3}} \begin{bmatrix} 1 & 0 \\ -1/2 & \sqrt{3}/2 \\ -1/2 & -\sqrt{3}/2 \end{bmatrix} \begin{bmatrix} \dot{i}_{c\alpha} \\ \dot{i}_{c\beta}^* \end{bmatrix}$$
(16)

Figure 6 shows a control of shunt active filter.



Figure 6.Control strategy of shunt active filter

The proposed model of UPQC-BES system supplied by three RE sources is shown in Figure 1. From the figure, we can see that PV is connected to the DC link through a DC-DC boost converter circuit. The PV partially distributes power to the load and the remains istransfered to three phase grid. The load consists of non linear and unbalanced load. The non-linear load is a diode rectifier circuit with the RL load type, while the unbalanced load is a three phase RC load with different R value on each phase. To be economically efficient, PV must always work in MPP condition. In this research, MPPT method used is P and O algorithm. The model is also applied for UPQC-BES system which is supplied by wind and PV-wind hybrid respectively. In order to operate properly, UPQC-BES system device must have a minimum DC link voltage (V_{dc}). The value of common DC link voltage depends on the nstantaneous energy avialable to UPQC is defined by in (17) [16]:

$$V_{dc} = \frac{2\sqrt{2} V_{LL}}{\sqrt{3}m} \tag{17}$$

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where m is modulation index and V_{LL} is the AC grid line voltage of UPQC. Considering that modulation index as 1 and forline to line grid voltage ($V_{LL} = 380$ volt), the V_{dc} is obtained 620,54 volt and selected as 650 volt.

The input of shunt active filter showed in Figure 5 is DC voltage (V_{dc}) and reference DC voltage (V_{dc}^*), while the output is \bar{p}_{loss} by using PI controller. Then, the \bar{p}_{loss} is as one of input variable to generate the reference source current (I_{sa}^* , I_{sb}^* , and I_{sc}^*). The reference source current output is then compared to source current (I_{sa} , I_{sb}^* , and I_{sc}^*). The reference source current output is then compared to source current (I_{sa} , I_{sb}^* , and I_{sc}^*). The reference source current output is then compared to source current (I_{sa} , I_{sb}^* , and I_{sc}^*). The reference source current output is then compared to source current (I_{sa} , I_{sb}^* , and I_{sc}^*). The reference source current output is then compared to source current (I_{sa} , I_{sb}^* , and I_{sc}^*). The reference source current output is then compared to source current (I_{sa} , I_{sb}^* , and I_{sc}^*). The reference source current output is then compared to source current (I_{sa} , I_{sb}^* , and I_{sc}^*). The reference source current output is then compared to source current (I_{sa} , I_{sb}^* , and I_{sc}^*). The reference source current output is then compared to source current (I_{sa}^* , I_{sb}^* , and I_{sc}^*). The reference source current output is the compared to source current (I_{sa}^* , I_{sb}^* , and I_{sc}^*). The reference source current output is the compared to source current (I_{sa}^* , I_{sb}^* , and I_{sc}^*) by the current hysteresis control algorithm on shunt active filter is proposed and compared with PI controller. The FLC is capable of reduce oscilation and generate quick convergence calculation during disturbances. This method is also used to overcome the weakness of PI controller in determining proportional gain (K_p) and integral gain constant (K_i) which still use trial and error method.

2.6. Fuzzy Logic Controller

The research is started by determine \bar{p}_{loss} as the input variable to result the reference source current on current hysteresis controller to generate trigger signal on the IGBT shunt active filter of UPQC using PI controller ($K_p = 0.2$ and $K_i = 1.5$). By using the same procedure, \bar{p}_{loss} is also determined by using FLC. The FLC has been widely used in recent industrial processes because it has heuristic, simpler, more effective and has multi rule based variables in both linear and non-linear system variations. The main components of FLC are fuzzification, decision making (rulebase, database, reason mechanism) and defuzzification in Figure 7.



The fuzzy rule algorithm collects a number of fuzzy control rules in a particular order. This rule is used to control the system to meet the desired performance requirements and they are designed from a number of intelligent system control knowledge. The fuzzy inference of FLC using Mamdani method related to max-min composition. The fuzzy inference system in FLC consists of three parts: rule base, database, and reasoning mechanism [19]. The FLC method is performed by determining input variables V_{dc} ($V_{dc-error}$) and delta Vdc ($\Delta V_{dc-error}$), seven linguistic fuzzy sets, operation fuzzy block system (fuzzyfication, fuzzy rule base and defuzzification), $V_{dc-error}$ and $\Delta V_{dc-error}$ during fuzzification process, fuzzy rule base table, crisp value to determine \bar{p}_{loss} in defuzzification phase. The \bar{p}_{loss} is one of input variable to obtain compensating currents $(i_{c\alpha}^*, i_{c\beta}^*)$ in (16). During fuzzification process, a number of input variables are calculated and converted into linguistic variables based on a subset called membership function. The error Vdc (V_{dc-error}) and delta error Vdc ($\Delta V_{dc-error}$) are proposed input variable system and output variable is \bar{p}_{loss} . To translate these variables, each input and output variable is designed using seven membership functions: Negative Big (NB), Negative Medium (NM), Negative Small (NS), Zero (Z), Positive Small (PS), Positive Medium (PM) and Positive Big (PB). The membership functions of crisp input and output are presented with triangle and trapezoid membership functions. The value of V_{dc-error} range from -650 to 650, Δ V_{dc-error} from -650 to 650, and \bar{p}_{loss} from -100 to 100. The input and output MFs are shown in Figure 8.



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Figure 8. Membership functions (a) $V_{dc-error}$, (b) $\Delta V_{dc-error}$, and (c) \overline{p}_{loss}

After the V_{dc-error} and $\Delta V_{dc-error}$ are obtained, then two input membership functions are converted to linguistic variables and uses them as input functions for FLC. The output membership function is generated using inference blocks and the basic rules of FLC as shown in Table 1. Finally the defuzzification block operates to convert generated \bar{p}_{loss} output from linguistic to numerical variable again. Then it becomes input variable for current hysteresis controller to produce trigger signal on the IGBT circuit of UPQC shunt active filter to reduce source current and load voltage harmonics. While simultaneously, it also improve power quality of 3P3W system under six scenarios due to the integration of three RE sourcesto UPQC-BES system.

3. RESULTS AND ANALYSIS

The analysis of proposed model is investigated through determination of six disturbance scenarios i.e. (1) NL, (2) Unba-NL, (3) Dis-NL, (4) Sag-NL, (5) Swell-NL, and (6) Inter-NL. Each scenario of UPQC uses PI controller and FLC so total number of disturbance are 12 scenarios.By using Matlab/Simulink, the model is then executed according to the desired scenario to obtain curve of source voltage (V_s), load voltage (V_L), compensation voltage (V_c), source current (V_s), load current (IL), and DC voltage DC link (V_{dc}). Then, THD value of source voltage, source current, load voltage, and load current in each phase as well as average THD value (Avg THD) are obtained base on the curves. THD in each phase is determined in one cycle started at t = 0.35 s. The results of average of source voltage, source current, load voltage, and load current of 3P3Wsystem using UPQC-BES system supplied by three RE sources i.e. PV, wind, and PV-wind hybrid are presented in Table 2, 3, and 4. Next THD in each phase and average THD are showed in Table 5, 6 and 7.

		Table	e 2. Volta	age an	d Curre	ent of 3	P3W Sy	stem	Using 1	UPQC-	BES S	ystem S	Supplie	d by P	V	
C		Source Vo	ltage V _S (V)			Load Volt	age $V_L(V)$			Source Cu	irrent Is (A)			Load Cur	rent IL (A)	
Sch	Ph A	Ph B	Ph C	Avg	Ph A	Ph B	Ph C	Avg	Ph A	Ph B	Ph C	Avg	Ph A	Ph B	Ph C	Avg
								PI Controll	ler							
1	309.6	309.6	309.6	309.6	307.6	307.8	307.7	307.7	7.766	7.793	7.759	7.773	8.528	8.529	8.533	8.530
2	307.4	308.0	308.0	307.8	308.3	308.7	308.3	308.4	31.00	24.84	28.73	28.15	22.50	34.12	34.52	30.38
3	309.6	309.6	309.6	309.6	313,8	314.3	317.4	317.4	7.897	7.919	7.867	7.895	8.748	8.704	8.785	8.746
4	154.5	154.5	154.5	154.5	307.1	307.3	307.3	307.2	7.235	7.276	7.226	7.246	8.509	8.514	8.510	8.511
5	464.7	464.7	464.7	464.7	308.6	308.7	308.6	308.6	7.979	7.980	7.964	7.975	8.550	8.553	8.554	8.553
6	0.536	1.385	0.850	0.924	310.2	259.8	290.2	286.7	7.392	12.67	6.045	8.703	8.707	7.747	7.637	8.031
							Fuzz	y Logic Co	ntroller							
1	309.5	309.5	309.5	309.5	307.7	307.9	307.7	307.8	8.420	8.426	8.416	8.421	8.527	8.532	8.531	8.530
2	307.4	307.9	308.0	307.8	308.5	308.7	308.4	308.5	31.66	25.50	29.36	28.84	22.52	34.11	35.52	30.72
3	309.6	309.5	309.5	309.5	313.4	312.9	315.9	314.1	8.516	8.565	8.496	8.526	8.741	8.677	8.736	8.718
4	154.4	154.4	154.4	154.4	307.3	307.3	307.2	307.3	8.563	8.560	8.561	8.561	8.514	8.517	8.512	8.515
5	464.6	464.6	464.6	464.6	308.6	308.8	308.6	308.7	8.396	8.389	8.389	8.392	8.552	8.556	8.554	8.554
6	0.447	0.392	0.380	0.407	314.0	293.4	304.9	304.1	4.024	3.778	3.608	3.804	8.874	8.195	8.193	8.421

	Table 3. Voltage and Current of 3P3W System Using UPQC-BES System supplied by Wind															
C		Source Vol	ltage V _S (V)			Load Volt	age V _L (V)			Source Cu	rrent I _S (A)			Load Cur	rent IL (A)	
Sch	Ph A	Ph B	Ph C	Avg	Ph A	Ph B	Ph C	Avg	Ph A	Ph B	Ph C	Avg	Ph A	Ph B	Ph C	Avg
								PI Control	ller							
1	309.5	309.6	309.6	309.6	308.6	308.6	308.2	308.5	7.863	7.875	7.840	7.869	8.554	8.553	8.546	8.551
2	307.4	308.0	308.0	308.0	308.9	309.2	308.7	308.9	31.07	24.97	28.81	28.28	2255	34.17	34.57	30.43
3	309.6	309.5	309.6	309.6	312.9	312.9	315.4	313.8	7.993	8.015	7.947	7.985	8.817	8.682	8.741	8.747
4	154.5	154.5	154.5	154.5	308.0	308.1	307.8	307.9	7.428	7.455	7.368	7.417	8.527	8.535	8.532	8.531
5	464.7	464.7	464.7	464.7	309.3	309.3	309.0	309.2	8.015	8.020	8.002	8.012	8.564	8.573	8.568	8.568
6	1.256	1.022	0.592	0.957	234.0	316.4	274.0	274.8	11.27	9.866	7.028	9.388	5.958	8.697	8.204	7.619
							Fuz	zy Logic Co	ontroller							
1	309.5	309.5	309.5	309.5	308.5	308.6	308.3	308.5	8.418	8.410	8.414	8.414	8.545	8.552	8.549	8.549
2	307.4	307.9	308.0	307.8	309.0	309.3	308.9	309.1	31.64	25.47	29.34	28.82	22.56	34.18	34.59	30.44
3	309.5	309.5	309.5	309.5	313.2	313.7	314.1	313.7	8.519	8.531	8.531	8.527	8.713	8.714	8.718	8.715
4	154.4	154.4	154.4	154.4	308.0	308.1	307.7	307.9	8.557	8.539	8.561	8.552	8.528	8.541	8.525	8.531
5	464.6	464.7	464.7	464.7	309.2	309.3	309.2	309.2	8.391	8.385	8.388	8.388	8.565	8.570	8.567	8.567
6	0.257	0 204	0.207	0 292	202.7	200.0	215 2	206.4	2 259	2 464	2 5 4 2	2 420	0 557	0 410	9 721	9 560

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	Tał	ole 4. V	oltage ai	nd Cur	rent of	3P3W	System	Using	UPQC	C-BES	System	Supplie	ed PV-	Wind H	fybrid		
C	Source Voltage V _S (V)					Load Vo	tage V _L (V)			Source 0	Current I _S (A)			Load Current IL (A)			
Sch	Ph A	Ph B	Ph C	Avg	Ph A	Ph B	Ph C	Avg	Ph A	Ph B	Ph C	Avg	Ph A	Ph B	Ph C	Avg	
PI Controller																	
1	309.6	309.6	309.6	309.6	307.8	308.0	307.7	307.8	7.790	7.802	7.770	7.787	8.527	8.537	8.533	8.533	
2	307.4	308.0	308.0	307.8	308.4	308.8	308.4	308.6	31.02	24.87	28.74	28.21	22.52	34.13	34.53	31.40	
3	309.6	309.5	309.6	309.6	314.0	315.5	316.9	315.5	7.942	7.939	7.918	7.933	8.739	8.750	8.783	8.757	
4	154.5	154.5	154.5	154.5	307.3	307.4	307.2	307.3	7.289	7.309	7.251	7.283	8.513	8.516	8.515	8.515	
5	464.7	464.7	464.7	464.7	308.7	308.9	308.7	308.8	7.985	7.985	7.975	7.982	8.552	8.558	8.558	8.556	
6	1.048	0.825	0.845	0.906	247.5	300.7	303.7	283.9	5.119	5.927	9.271	6.773	7.016	7.893	8.793	7.867	
							Fuzz	y Logic Co	ntroller								
1	309.5	309.5	309.5	309.5	307.8	308.0	307.7	307.8	8.419	8.418	8.409	8.413	8.529	8.539	8.533	8.534	
2	307.4	307.9	308.0	307.8	308.7	308.7	308.9	308.8	31.66	25.47	29.32	28.82	22.54	34.13	34.56	30.41	
3	309.5	309.5	309.5	309.5	314.4	315.5	316.6	315.5	8.581	8.593	8.568	8.581	8.761	8.722	8.761	8.748	
4	154.4	154.4	154.4	154.4	307.3	307.5	307.3	307.4	8.566	8.572	8.563	8.567	8.511	8.520	8.519	8.517	
5	464.6	464.6	464.6	464.6	308.8	308.8	308.7	308.8	8.391	8.394	8.396	8.394	22.33	22.35	22.36	22.35	
6	0.412	0.403	0.402	0.418	311.6	295.7	310.4	305.9	3.774	3.544	3.593	3.640	8.855	8.321	8.288	8.488	

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Table 2 shows UPQC-BES system supplied PV connected 3P3W system using PI and FLC, disturbance scenarios 1 to 5 produce an average load voltage above 307 V. While in scenario 6, FLC produces a higher average load voltage of 304.1 V than if using a PIof 286.7 V. If reviewed from average source current with PI, the highest and lowest average source currents are generated by disturbance scenarios 2 and 4 of 28.15 A and 7,246 A. Whereas if using FLC the highest and lowest average source currents are achieved in scenario 2 and 6 of 28.84 A and 3.804 A.Table 3 shows UPQC-BES supplied by windconnected to 3P3W with PI and FLC, scenarios 1 to 5 is able to obtain a stable load voltage above 308 V. The difference is that in scenario 6, PI generates a load voltage of 274.8 V, otherwise if using FLC, load voltage increases to 306.4 V. If reviewed from source current using PI, the highest and lowest average source currents are resulted by scenarios 2 and 4of 28.28 A and 7.417 A. Rather, if using FLC, the highest and lowest average source currents are achieved in scenario 2 and 6 of 28.82 A and 3,420 A.Table 4 shows UPQC-BES supplied PV-wind hybrid connected 3P3W using PI and FLC, scenarios 1 to 5 produce an average load voltage above 307 V. While in scenario 6, FLC generates an average load voltage 305.9 V higher than if using PI control of 283.9 V. If reviewed from average source current with PI, the highest and lowest average source currents are resulted by scenarios 2 and 4 of 28.21 A and 6,773 A. Otherwise if using FLC the highest and lowest average source currents are achieved in scenario 2 and 6 of 28.82 A and 3.640 A respectively.

Table 5. Harmonics of 3P3W System Using UPQC-BESSystem Supplied by PV

C	S	ource Voltag	ge THD (%)		Load Volta	age THD (%)	S	ource Currer	nt THD (%)		Load Current (%)			
Sch	Ph A	Ph B	Ph C	Avg	Ph A	Ph B	Ph C	Avg	Ph A	Ph B	Ph C	Avg	Ph A	Ph B	Ph C	Avg
								PI Con	troller						-	
1	2.35	2.36	2.32	2.34	2.48	2.50	2.46	2.48	12.89	12.72	12.92	12.84	22.32	22.34	22.32	22.33
2	2.29	2.20	2.24	2.24	2.43	2.23	2.37	2.34	2.660	2.330	2.240	2.410	5.230	2.070	2.660	3.320
3	5.84	5.86	5.94	5.88	6.36	5.90	6.58	6.28	12.75	12.64	13.06	12.82	21.92	22.16	22.33	22.14
4	4.69	4.75	4.81	4.75	2.46	2.48	2.53	2.49	14.26	13.96	14.16	14.13	22.28	22.31	22.28	22.29
5	1.56	1.53	1.55	1.55	2.47	2.43	2.45	2.45	12.51	12.36	12.44	12.44	22.34	22.32	22.32	22.33
6	NA	NA	NA	NA	32.11	15.09	28.54	25.25	270.90	145.89	275.67	230.82	47.70	34.58	36.29	39.53
								Fuzzy Logic	Controller							
1	2.35	2.33	2.35	2.34	2.48	2.46	2.49	2.47	11.83	11.82	11.84	11.83	22.33	22.32	22.33	22.33
2	2.25	2.27	2.20	2.24	2.39	2.41	2.34	2.38	2.620	2.400	2.220	2.413	5.230	2.100	2.640	3.323
3	5.83	5.88	5.93	5.88	6.23	5.93	6.69	6.28	11.83	11.90	12.14	11.96	21.84	22.34	22.53	22.24
4	4.71	4.76	4.79	4.75	2.46	2.48	2.50	2.48	11.91	11.88	11.86	11.89	22.27	22.32	22.32	22.31
5	1.55	1.54	1.54	1.54	2.45	2.44	2.46	2.45	11.90	11.84	11.85	11.86	22.36	22.33	22.35	22.35
6	NA	NA	NA	NA	13.05	6.60	11.15	10.27	30.61	34.72	31.57	32.30	24.25	24.25	24.71	24.40

		Т	able 6.	Harmo	nics of	3P3W	System	n Using	UPQC	-BESS	ystem S	Supplie	d by W	ind		
C		Source Volta	age THD (%)	Load Voltage THD (%)				5	Source Curr	ent THD (%)	Load Current (%)			
Sch	Ph A	Ph B	Ph C	Avg	Ph A	Ph B	Ph C	Avg	Ph A	Ph B	Ph C	Avg	Ph A	Ph B	Ph C	Avg
PI Controller																
1	1.88	1.87	1.94	1.89	1.99	1.97	2.05	2.00	12.63	12.37	12.70	12.57	12.30	12.30	12.34	12.31
2	1.83	1.76	1.82	1.80	1.92	1.85	1.93	1.90	2.460	2.070	2.200	2.240	5.260	2.070	2.690	3.340
3	5.67	5.71	5.77	5.72	6.00	6.83	6.02	6.28	12.48	12.26	12.66	12.47	22.01	22.12	22.08	22.07
4	3.76	3.86	3.86	1.83	1.97	2.02	2.03	2.01	13.59	13.17	13.51	13.42	22.29	22.31	22.30	22.30
5	1.26	1.24	1.29	1.26	1.99	1.97	2.05	2.00	12.31	12.20	12.31	12.27	22.36	22.33	22.37	22.35
6	NA	NA	NA	NA	14.09	35.59	34.73	28.14	157.76	139.01	266.07	186.95	37.60	34.39	46.97	39.65
							Fuz	zy Logic Co	ntroller							
1	1.89	1.88	1.93	1.90	1.99	1.98	2.04	2.00	11.71	11.72	11.77	11.73	22.34	22.31	22.32	22.32
2	1.85	1.79	1.78	1.81	1.95	1.87	1.88	1.90	2.43	2.11	2.12	2.220	5.240	2.070	2.700	3.240
3	5.67	5.71	5.78	5.72	5.99	6.39	6.13	6.17	11.72	11.62	11.90	11.75	22.08	21.94	22.47	22.16
4	3.79	3.81	3.86	3.82	1.97	1.99	2.03	1.99	11.72	11.69	11.74	11.72	22.28	22.30	22.35	22.31
5	1.27	1.24	1.28	1.26	2.00	1.96	2.04	2.00	11.66	11.76	11.76	11.73	22.31	22.33	22.35	22.33
6	NA	NA	NA	NA	7.59	6.44	10.95	8.33	27.33	28.27	26.39	27.33	25.39	23.65	24.31	24.45

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	Table 7. Harmonics of 3P3W System Using UPQC-BES System Supplied by PV-Wind Hybrid																
C	S	ource Vol	tage THD (%)	Load Voltage THD (%)				S	Source Current THD (%)				Load Current (%)			
Sch	Ph A	Ph B	Ph C	Avg	Ph A	Ph B	Ph C	Avg	Ph A	Ph B	Ph C	Avg	Ph A	Ph B	Ph C	Avg	
PI Controller																	
1	2.25	2.19	2.29	2.24	2.37	2.31	2.42	3.37	12.85	12.62	12.74	12.74	22.33	22.31	22.34	22.33	
2	2.18	2.08	2.15	2.13	2.30	2.19	2.18	2.22	2.630	2.300	2.290	2.407	5.230	2.070	2.670	3.323	
3	5.81	5.82	5.89	5.84	6.12	5.88	6.75	6.25	12.71	12.63	12.98	12.77	22.05	22.13	22.54	22.24	
4	4.53	4.48	4.51	4.51	2.37	2.35	2.37	2.36	14.16	13.50	13.99	13.88	22.27	22.30	22.28	22.28	
5	1.49	1.46	1.51	1.49	2.37	2.31	2.40	2.36	12.43	12.29	12.41	12.38	22.34	22.32	22.33	22.33	
6	NA	NA	NA	NA	18.61	36.38	28.42	27.8	387.71	330.34	189.29	302.45	36.73	38.51	36.83	37.36	
							Fu	izzy Logic C	Controller								
1	2.25	2.23	2.25	2.24	2.37	2.35	2.39	2.37	11.85	11.74	11.84	11.81	22.32	22.31	22.33	22.32	
2	2.23	2.15	2.05	2.14	2.37	2.26	2.17	2.26	2.520	2.410	2.140	2.446	5.230	2.070	2.690	3.330	
3	5.80	5.83	5.90	5.84	6.57	5.26	7.06	6.29	11.83	11.78	12.24	11.95	22.15	22.23	22.95	22.44	
4	4.53	4.52	4.54	4.86	2.36	2.35	2.35	2.35	11.79	11.74	11.84	11.79	22.29	22.30	22.29	22.29	
5	1.48	1.46	1.51	1.48	2.35	2.32	2.40	2.35	11.78	11.81	11.81	11.80	22.33	22.35	22.36	22.35	
6	NA	NA	NA	NA	10.30	4.90	10.25	8.48	27.44	29.52	28.63	28.53	23.20	23.97	24.65	23.94	

Table 5 shows that average THD of load voltage (V_L) of UPQC-BES system supplied by PV in 3P3W system for scenarios 1 to 5 using PI control is within limits in IEEE 519. The highest and lowest average THD load voltages are achieved under scenario 6 and 2 as 25.25% and 2.34% respectively. PI controller is also able to migitate average THD source voltage in scenario 6 from not accessible (NA) to 25.25% on the load side. The highest and lowest average THD of source current are achieved in scenario 6 and 2 as 230.82% and 2.41%. Table 5 also indicates that average THD of load voltage of UPQC system supplied by PV with BES using FLC in scenarios 1 to 5, has fulfilled limits in IEEE 519. The highest and lowest average THD of load voltage are achieved under scenario 6 and 2 of 10.27% and 2.38%. The use of FLC method is also able to reduce average THD of source current are achieved in scenario 6 and 2 of 32.30% and 2.413%.

Table 6 shows that average THD of load voltage of UPQC-BES system supplied by wind in 3P3W system for interference scenarios 1 to 5 using PI is within limits prescribed in IEEE 519. The highest and lowest average THD load voltages is achieved under scenario 6 and scenario 2 as 28.14% and 1.90% respectively. PI controller is also able to reduce average THD source voltage in scenario 6 from NA to 28.14% on the load side. The highest and lowest average THD of source current areachieved in scenario 6 and 2 as 186.95% and 2.24% respectively. Table 6also shows that average THD of load voltage of UPQC-BES supplied by wind using FLC in scenarios 1 to 5, has fulfilled limits prescribed in IEEE 519. The highest and lowest average THD of load voltage are achieved under scenario 6 and 40 8.33% and 1.90%. FLC method is also able to reduce average THD on source voltage in scenario 6 from NA to 7.33% on load side. The highest and lowest average THD on source current are achieved in Scenario 6 and 2 of 27.33% and 2.22%.

Table 7shows that average THD of load voltage (V_L) of UPQC-BES system supplied by PV-wind hybrid in 3P3W system for scenarios 1 to 5 using PI is within limits in IEEE 519. The highest and lowest average THD load voltages are achieved under scenario 6 and 2 as 27.8% and 2.22% respectively. PI is also able to migitate average THD of source voltage in scenario 6 from NA to 27.8% on load side. The highest and lowest average THD of source current are achieved in scenario 6 and 2 as 302.45% and 2.407% respectively. Table 7 also indicates that average THD of load voltage of UPQC-BES system supplied by PV-wind hybrid using FLC for scenarios 1 to 5, has fulfilled limits in IEEE 519. The highest and lowest average THD of load voltage are achieved under scenario 6 and 2 of 8.48% and 2.26%. FLC method is also able to reduce average THD of source voltage in scenario 6 from NA to 8.48% on load side. The highest and lowest average THD of source current are achieved in scenario 6 and 2 of 28.53% and 2.446%. Overall for UPQC-BES system supplied by three RE sources in scenarios 1 to 5 using PI and FLC is able to improve average THD of source current better on average THD of load current. Figure 9 presents UPQC-BES system performance supplied by three RE sources using FLC in scenario 6.

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Figure 9.a.(i) shows that in scenario 6, UPQC-BES system supplied by PV at t = 0.2 s to t = 0.5 s, average source voltage (V_S) falls as 100% to 0.4062 V. During the disturbance, PV is able to generate power to UPQC DC link and injecting full average compensation voltage (V_C) in Figure 9.a.(ii) through injection transformer on series active filter so that average load voltage (V_L) in Figure 9.a.(ii) remains stable at 304.1 V. As long as fault period, although nominal of average source current (I_S) in Figure 9.a.(iv) drops to 3.804 A, combination of PV and BES is able to generate power, store excess energy of PV, and inject current into

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load through shunt active filter so that average load current (IL) in Figure 9.a.(v) remains as 8.421 A.Figure 9.b.(i) presents on UPQC-BES supplied by wind at t = 0.2 s to t = 0.5 s average source voltage (Vs) drops 100% to 0.3828 V. During the disturbance, wind is able to generate power to UPQC DC link and injecting full average compensation voltage (V_C) in Figure 9.b.(iii) through injection transformer on series active filter so that average load voltage (VL) in Figure 9.b.(ii) remains stable at 306.4 V. During fault period, although nominal of average source current (Is) fallsto 3.420 A, combination of wind and BES is able to generate power, store excess energy of wind, and inject current into load through shunt active filter so that average load current (IL) in Figure 9.b.(v) remains as 8.569 A.Figure 9.c.(i) indicates on UPQC-BES supplied by PV-Wind Hybrid at t = 0.2 s to t = 0.5 s average source voltage (V_s) drops 100% to 0.4175 V. During the disturbance, PV-wind hybrid is able to generate power to UPQC DC link and injecting full average compensation voltage (V_C) in Figure 9.c.(iii) through injection transformer on series active filter so that average load voltage (VL) in Figure 9.b.(ii) remains stable at 305.9V. As long as disturbance period, although nominal of average source current (Is) falls to 3.640 A, combination of PV-wind hybrid and BES is able to generate power, store excess energy of wind, and inject current into load through shunt active filter so that average load current (IL) in Figure 9.c.(v) remains as 8.488 A.Figure 10 shows spectra of load voltage harmonics on phase A of UPQC-BES system supplied by three RE sources using FLC in scenario 6. Figure 11 shows performance of average THD of load voltage and source current on UPQC-BES system supplied by three RE sources.





Figure 11. Performance of UPQC-BES supplied by threeRE sources using PI and FLC

Figure 11(a) shows that in scenario 1 to 5, the implementation of FLC on UPQC-BES system supplied by three RE sources is able to obtain average THD of load voltage slightly better than PI controller and both method have already met the limit in IEEE 519. Further under scenario 6, FLC applied on UPQC-BES system supplied by three RE sourcesgivessignificantly better result of average THD of load voltage than PI controller. In six disturbance scenarios, both PI controller and FLC applied on UPQC-BES system supplied by three RE sources, PV is ableto obtainthe highest average THD of load voltages.Figure 11(b) shows that in disturbance scenario 1 to 5, implementation of FLC on UPQC-BES system supplied by three RE sources able to obtain average THD of source current slightly better than PI controller. Furthermore under scenario 6, FLC applied on UPQC-BES system supplied by three RE sources gives significantly better result of average THD of source current than PI controller. Both PI controller and FLC on UPQC-BES system supplied by three RE sources is significantly better result of average THD of source current. Both PI controller and FLC on UPQC-BES system supplied by three RE sources is significantly better result of average THD of source current than PI controller. Both PI controller and FLC on UPQC-BES system supplied by three RE sources is significantly better current.

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4. CONCLUSION

Comparative performance analysis of UPQC-BES system supplied by three RE sources i.e. PV, wind, and PV-wind hybrid respectively using PI controller and FLC have been discussed. In disturbance scenario 1 to 5, implementation of FLC on UPQC-BES system supplied by three RE sources is able to obtain average THD of load voltage slightly better than PI and both methods have already met the limit in IEEE 519. Under scenario 6, FLC applied on UPQC-BES system supplied by three RE sources givessignificantly better result average THD of load voltage than PI. In six disturbance scenarios, both PI and FLC applied on UPQC-BES system supplied by three RE sources in the highest average THD of load voltage than PI. In six disturbance scenarios, both PI and FLC applied on UPQC-BES system supplied by three RE sources; able to obtain average THD of source current slightly better than PI. Furthermore under scenario 6, FLC applied on UPQC-BES system supplied by three RE sources ifficantly better to dotain average THD of source current slightly better than PI. Furthermore under scenario 6, FLC applied on UPQC-BES system supplied by three RE sources in six scenarios, PV is able to obtain the highest average THD of source current than PI. Both PI and FLC on UPQC-BES system supplied by three RE sources in six scenarios, PV is able to obtain the highest average THD of source current.

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APPENDIX

Three phase grid: RMS voltage 380 volt (L-L), 50 Hz, line impedance: $R_s = 0.1$ Ohm $L_s = 15$ mH; series and shunt active filter: series inductance $L_{se} = 0.015$ mH; shunt inductance $L_{sh} = 15$ mH; injection transformers: rating 10 kVA, 50 Hz, turn ratio (N_1/N_2) = 1:1; non linear load: resistance $R_L = 60$ ohm, inductance $L_L = 0.15$ mH, load impedance $R_e = 0.4$ ohm and $L_c = 15$ mH; unbalance load: resistance $R_1 = 24$ ohm, $R_2 = 12$ ohm, and $R_3 = 6$ ohm, capacitance $C_1, C_2, C_3 = 2200 \ \mu$ F; DC-link: voltage $V_{DC} = 650$ volt and capacitance $C_{DC} = 3000 \ \mu$ F; battery energe storage: type = nickel metal hybrid, DC voltage = 650 volt, rated capacity = 200 Ah, initial SOC = 100%, inductance $L_1 = 6$ mH, capacitance $C_1 = 200 \ \mu$ F; photovoltaic: active power = 0.6 kW temperature = 25⁰ C, irradiance = 1000 W/m²; PMSG wind turbine active power = 0.6 kW, voltage = 380 volt, 50 Hz, wind speed = 5 m/s, picth angle = 2; PI controller: $K_p = 0.2$, $K_i = 1.5$; fuzzy model: method = mandani, composition = max-min; input membership function: error (V_{dc}) = trapmf, trimf; output membership function: \overline{p}_{loss} = trapmf,trimf.

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BIOGRAPHIES OF AUTHORS



IJECE

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Lampiran 2.3 Revisi pertama makalah

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Matlab/simulink simulation of unified power quality conditioner-battery energy storage system supplied by PV-wind hybrid using fuzzy logic controller

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Article Info	ABSTRACT
Article history:	This paper presents performance analysis of Unified Power Quality
Received May 2, 2018 Revised Nov 11, 2018 Accepted Dec 2, 2018	Photovoltaic (PV)-Wind Hybrid connected to three phase three wire (3P3W) of 380 volt (L-L) and 50 hertz distribution system. The performance of supply system is compared with two renewable energy (RE) sources i.e. PV and Wind, respectively. Fuzzy Logic Controller (FLC) is implemented to
Keywords:	maintain DC voltage across the capacitor under disturbance scenarios of source and load as well as to compare the results with Proportional Intergral
Battery energi storage Photovoltaic Power quality PV-Wind Hybrid Total harmonic distortion UPQC Wind turbine	(PI) controller. There are six scenarios of disturbance i.e. (1) non-linear load (NL), (2) unbalance and nonlinear load (Unba-NL), (3) distortion supply and non-linear load (Dis-NL), (4) sag and non-linear load (Sag-NL), (5) swell and non-linear load (Swell-NL), and (6) interruption and non-linear load (Inter-NL). In disturbance scenario 1 to 5, implementation of FLC on UPQC- BES system supplied by three RE sources is able to obtain average THD of load voltage/source current slightly better than PI. Furthermore under scenario 6, FLC applied on UPQC-BES system supplied by three RE sources gives significantly better result of average THD of load voltage/source current than PI. This research is simulated using Matlab/Simulink.
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1. INTRODUCTION

PV and wind are the most RE distributed generations (DGs) because they are able to convert sunlight and wind into power. PV and solar are the potential DGs sources since it only need sunlight to generate electricity, where the resources are available in abundance, free and relatively clean. Indonesia has enormous energy potential from the sun because it lies on the equator. Almost all areas of Indonesia get sunlight about 10 to 12 hours per day, with an average intensity of irradiation of 4.5 kWh/m² or equivalent to 112.000 GW. The potential of wind energy in Indonesia generally has a speed between 4 to 5 m/s and classified as medium scale with potential capacity of 10 to 100 kW. The weakness of PV and wind turbine besides able to generate power, they also produces a number voltage and current harmonics resulted by presence of several types of PV and wind turbine devices and power converters as well as to increase a number of non-linear loads connected to the grid, so finally resulting in the decrease in power quality.

In order to overcome and improve power quality due to presence of non-linear loads and integration of PV and wind turbine to grid, UPQC is a proposed. UPQC serves to compensate for source voltage quality problems i.e. sag, swell unbalance, flicker, harmonics, and load current quality problems i.e. harmonics,

unbalance, reactive currents, and neutral current. B. Han et. al and Vinod Khadkikar have investigated UPQC as one part of active power filter consisting of shunt and series active filters connected in parallel and serves as superior controller to overcome a number of power quality problems simultaneously. Series component has been responsible for reducing a number of interference on source side i.e. voltage sag/swell, flicker, unbalanced voltage, and harmonics. Shunt component has been responsible for addressing a current quality problems i.e. low power factor, load current harmonics, and unbalanced load. [1,2]. UPQC based on RE has been investigated by some researchers. There are two methods used to overcome this problem i.e. using conventional and artificial intelligence.Shafiuzzaman K.K., et.al have proposed system includes a series inverter, shunt inverter, and a DG connected to a DC link through a rectifier using PI. The system was capable of increase source voltage quality i.e. sag and interruption and load current quality, as well as transfer of active power on/off grid mode [3]. The influence of DG on UPQC performance in reducing sag under conditions of some phase to ground faults to using DSTATCOM has been implemented by Norshafinash S., et.al. The DG was effective enough to help UPQC to improve sag [4]. It was connected in series with load resulting better sag migitation compared to system without DG. Implementation of UPQC using UVTG method with PI to reduce sag, swell, voltage/current harmonics has been doneby S. N. Gohil, et.al. Simulation of voltage distortion was made by adding 5th and 7th harmonics at fundamental source voltage, resulting in a reduction of THD source current and THD load voltage [5].

UPQC supplied by PV panels using boost converter, PI, MPPT P and O, and p-q theory has been proposed by Yahia Bouzelata at.al [6]. The system was capable of compensate reactive power and reduce source current/load voltage harmonics, but did not discuss migitation of sag and interuption caused by PV penetration. Power quality enhancement of sag and source voltage harmonics on grid using UPQC supplied by PV array connected to DC link using PI compared with FLC has been done by Ramalengswara Rao, et.al. Combination of UPQC and PV using FLC can improve source voltage THD better than PI [7]. Amirullah et.al have researched a method for balancing current and line voltage, as a result of DGs of a single phase PV generator unit in randomly installed at homes through on a three phase four wire 220 kV and 50 Hz distribution line using BES and three of single phase bidirectional inverter. Both devices was capable of reduce unbalanced line current/voltage, but both of them were also capable of increase current/voltage harmonics on PCC bus [8]. Power quality migitation of UPQC on microgrid supplied by PV and wind turbine has been implemented by K S Srikanth et. al. It resulted that PI and FLC was able to improve power quality and reduce distortion in output power [9]. The UPQC-wind turbine to provide active power to overcome low sag and interruption voltage to grid has been investigated by H.Toodeji, et.al. The model was used VSC as a rectifier on generator output and controlled so that maximum power desired can be generated by different speed wind turbines using PI [10]. The UPQC-wind turbine connected to UPQC DC link was implemented by M. Hosseinpour, et al. The proposed combination using PI was capable of compensate swell, interruption voltage, and reactive power both on on/off grid [11]. R.Bhavani, et, al have researched on UPQC controlled by FLC to improve power quality in a DFIG wind turbine connected grid. FLC can improve power quality i.e. sag voltage and load current harmonics better than PI [12]. Power quality enhancement on wind turbine and BES with PI connected grid on PCC bus using UPQC has been implemented by S.RajeshRajan, et al. BES was installed to maintain and stabilize active power supply under different wind speed [13].

This research will analyze UPQC-BES performance supplied by PV-wind hybrid connected to 3P3W of 380 volt (L-L) and 50 hertz distribution system. The performance of supply system is compared with two RE sources i.e. PV and Wind, respectively. BES serves to store excess energy produced by three RE sources and distribute it to load if necessary, to prevent interruption voltage, and to adjust charging and discharging of energy in battery. BES is also expected to store excess power produced by three RE combinations and use it as backup power. FLC is proposed and compared with PI to control variable of DC voltage and DC reference voltage input to generate reference current source in current hysteresis controller on shunt active filter. DC voltage controller in shunt active filter and series active filter is used to migitate power quality of load voltage and source current.Performance of two controllers are used to determine load voltage, source current, load voltage THD, and source current THD based on IEEE 519. This paper is presented as follow. Section 2 describes proposed method, model of UPQC-BES system supplied by three RE sources i.e. PV, wind, and PV-wind hybrid, simulation parameters, PV and PMSG wind turbine model, series and shunt active filter, as well as application of PI and FLC method for proposed model. Section 3 shows results and analysis about performance of THD analysis on the proposed model of three RE sources connected to DC link of UPQC-BES system using PI and FLC. In this section, six disturbance scenarios are presented and the results are verified with Matlab/Simulink. Finally, this paper in concluded in Section 4.

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Int J Elec & Comp Eng 2. RESEARCH METHOD

2.1. Proposed method

Figure 1 shows proposed model in this research. The RE sources based DGs used i.e. PV, Wind Turbine, and PV-Wind Turbine Hybrid connected to 3P3W distribution system with 380 volt (L-L) and 50 Hz frequency, through UPQC-BES system. PV array produce power under fixed temperature and radiation as well as connect to UPQC-DC link through a DC/DC boost converter. The maximum power point tracking (MPPT) method with Pertub and Observer (P and O) algorithms helps PV produce maximum power and generate output voltage, as the input voltage for DC/DC boost converter. The converter serves to adjust dutycycle value and output voltage of PV as its input voltage to produce an output voltage corresponding to UPQC DC link voltage. Wind turbine type used is a permanent magnetic synchronous generator (PMSG) with variable speed and fixed voltage which generating power and is connected to UPQC DC link circuit through AC/DC bridge rectifier. The rectifier helps to change AC PSMG stator output voltage to DC voltage through LC circuit that serves to filter and smooth it before connected to UPQC-DC link.BES connected to the UPQC-DC link circuit serves as energy storage and is expected to overcome interruption voltage and overall help UPQC performance to improve voltage and current quality on source and load bus. Simulation parameters proposed in this study is shown in Appendix Section. Power quality analysis is performed on PV, Wind, PV-Wind Hybrid respectively, connected to 3P3W system through UPQC DC-link (on-grid) using BES circuit. Single phase circuit breakers (CBs) are used to connect and disconnect PV, Wind, and Hybrid PV-Wind respectively with UPOC DC-link.

There are six disturbance scenarios i.e.(1) NL, (2) Unba-NL, (3) Dis-NL, (4) Sag-NL, (5) Swell-NL, and (6) Inter-NL. In scenario 1, the model is connected a non-linear load with R_L and L_L of 60 Ohm and 0.15 mH respectively. In scenario 2, the model is connected to non-linear load and during 0.3 s since t = 0.2 s to t = 0.5 s connected to unbalance three phase load with R1, R2, R3 as 6 Ohm, 12 Ohm, 24 Ohm respectively, and value of C1, C2, C3 as 2200 µF. In scenario 3, the model is connected to non-linear load and source voltage generating 5th and 7th harmonic components with individual harmonic distortion values of 5% and 2% respectively. In scenario 4, the model is connected to non-linear load and source experiences a sag voltage disturbance of 50% for 0.3 s between t = 0.2 s to t = 0.5 s. In scenario 5, the model is connected to a nonlinear load and source experiences a swell voltage disturbance of 50% for 0.3 s between t = 0.2 s to t = 0.5 s. In scenario 6, the model is connected to non-linear load and source experiences an interruption voltage interference of 100% for 0.3 s between t = 0.2 s to t = 0.5 s.FLC is used as a DC voltage control in a shunt active filter to improve the power quality of the load voltage and current source and compare it with PI controller. Each disturbance scenario uses a PI controller and FLC so that the total of 12 disturbances. The result analysis of research was carried out i.e. (1) voltage and current on source or poin common coupling (PCC) bus, (2) voltage and current on load bus, (3) harmonic voltage and harmonic current on source bus and (4) harmonic voltage and harmonic current on load bus. The final phase is to compare performance of UPQC-BES system on-grid supplied by PV, Wind, PV-Wind Hybrid respectively using two controllers to improve power quality of load voltage and source current under six disturbance conditions.



Figure 1. Proposed model of UPQC-BES system supplied by PV, wind, and PV-wind Hybrid

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2.2. Photovoltaic model

Figure 2 shows the equivalent circuit and V-I characteristic of a solar panel. A solar panel is composed of several PV cells that have series, parallel, or series-parallel external connections [14].



Figure 2. Equivalent circuit and V-I characteristic of solar panel

The V-I characteristic of a solar panel is showed in (1):

$$I = I_{PV} - I_o \left[\exp\left(\frac{V + R_s I}{aV_r}\right) - 1 \right] - \frac{V + R_s I}{R_p}$$
(1)

where I_{PV} is the photovoltaic current, I_o is saturated reverse current, 'a' is the ideal diode constant, $V_t = N_S K T q^{-1}$ is the thermal voltage, N_S is the number of series cells, q is the electron charge, K is the Boltzmann constant, T is the temperature of p-n junction, R_S and R_P are series and parallel equivalent resistance of the solar panels. I_{PV} has a linear relation with light intensity and also varies with temperature variations. I_o is dependent on temperature variations. The values of I_{PV} and I_o are calculated as following (2) and (3):

$$I_{PV} = (I_{PV,n} + K_1 \Delta T) \frac{G}{G_n} I$$
⁽²⁾

$$I_o = \frac{I_{SC,n} + K_I \Delta T}{\exp(V_{oC,n} + K_V \Delta T) / aV_t - 1}$$
(3)

In which $I_{PV,n}$, $I_{SC,n}$ and $V_{OC,n}$ are photovoltaic current, short circuit current and open circuit voltage in standard conditions ($T_n = 25$ C and $G_n = 1000$ Wm⁻²) respectively. K_I is the coefficient of short circuit current to temperature, $\Delta T = T - T_n$ is the temperature deviation from standard temperature, G is the light intensity and K_v is the ratio coefficient of open circuit voltage to temperature. Open circuit voltage, short circuit current and voltage-current corresponding to the maximum power are three important points of I-V characteristic of solar panel. These points are changed by variations of atmospheric conditions. By using (4) and (5) which are derived from PV model equations, short circuit current and open circuit voltage can be calculated in different atmospheric conditions.

$$I_{SC} = (I_{SC} + K_1 \Delta T) \frac{G}{G}$$
⁽⁴⁾

$$V_{oc} = V_{oc} + K_V \Delta T \tag{5}$$

2.3. PMSG wind turbine

Wind turbine is onother part of an integrated system, which can be divided into two types i.e. fixed and variable speed wind turbines. In fixed speed type, rotating speed of turbine is fixed and hence, frequency of generated voltage remains constant, so it can be directly connected to the network. In this case, maximum power can not always be extracted by wind. On the other hand, on variable speed, turbine can rotate at different speeds, so maximum power can be generated in each wind speed by MPPT method [10].The

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advantage of using a PMSG over a synchronous generator and DFIG machine because it has high efficiency and reliability. Due to the elimination of rotor external excitation, machine size, and cost also decreases, making PMSG to be more controlled easily with feedback control system. PMSG has become an attractive solution on wind generation systems with variable speed wind turbine applications [15]. Figure 3 and 4 shows model of PMSG wind turbine and wind turbin power characteristic curve.



Figure 3. Model of PMSG wind turbine



Figure 4. Wind turbin power characteristic curve

The output power of wind turbine can be expressed using (6), (7), and (8) [11].

$$\lambda = \frac{\omega_r R}{V_{wind}} \tag{6}$$

 $P_M = \frac{1}{2} \rho \pi R^2 C_p V_{wind}^3 \tag{7}$

$$T_{M} = \frac{P_{M}}{\omega_{r}} = \frac{1}{2} \rho \pi R^{5} C_{p} \frac{\omega_{M}^{3}}{\lambda^{3}}$$

$$\tag{8}$$

Where λ is the speed-tip ratio, V_{wind} is wind speed, R is blade radius, ω_r is rotor speed (rad/sec), ρ is the air density, C_P is the power coefficient, P_M is the output mechanical power, and T_M is output torque of wind turbine. The C_P coefficient is dependent on the pitch angle value, at which rotor blade can rotate along axis and tip-speed ratio λ expressed in (9).

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$$C_{p} = (0.44 - 0.167\beta)\sin\frac{\pi(\lambda - 2)}{(13 - 0.3\beta)}$$
(9)

Where β is a pitch angle blade. In a fixed pitch type, the value of β is set to a fixed value.

2.4. Control of series active filter

The main function of series active filter is as a sensitive load protection against a number of voltage interference at PCC bus. The control strategy algorithm of the source and load voltage in series active filter circuit is shown in Figure 5. It extracts the unit vector templates from the distorted input supply. Furthermore, the templates are expected to be ideal sinusoidal signal with unity amplitude. The distorted supply voltages are measured and divided by peak amplitude of fundamental input voltage V_m givenin (10) [6].

$$V_m = \sqrt{\frac{2}{3} \left(V_{sa}^2 + V_{sb}^2 + V_{sc}^2 \right)}$$
(10)

A three phase locked loop (PLL) is used in order to generate a sinusoidal unit vector templates with a phase lagging by the use of sinus function. The reference load voltage signal is determined by multiplying the unit vector templates with the peak amplitude of the fundamental input voltage V_m . The load reference voltage $(V_{La}^*, V_{Lb}^*, V_c^*)$ is then compared against to sensed load voltage (V_{La}, V_{Lb}, V_{Lc}) by a pulse width modulation (PWM) controller used to generate the desired trigger signal on series active filter.



Figure 5. Control strategy of series active filter

2.5. Control of shunt active filter

The main function of shunt active filter is migitation of power quality problems on the load side. The control methodology in shunt active filter is that the absorbed current from the PCC bus is a balanced positive sequence current including unbalanced sag voltage conditions in the PCC bus or unbalanced conditions or non-linear loads. In order to obtain satisfactory compensation caesed by disturbance due to non-linear load, many algorithms have been used in the literature. This research used instantaneous reactive power theory method "p-q theory". The voltages and currents in Cartesian *abc*coordinates can be transformed to Cartesian *aβ* coordinates as expressed in (11) and (12) [16].

$$\begin{bmatrix} v_{\alpha} \\ v_{\beta} \end{bmatrix} = \begin{bmatrix} 1 & -1/2 & -1/2 \\ 1 & \sqrt{3}/2 & -\sqrt{3}/2 \end{bmatrix} \begin{bmatrix} V_{a} \\ V_{b} \\ V_{c} \end{bmatrix}$$
(11)

$$\begin{bmatrix} i_{\alpha} \\ i_{\beta} \end{bmatrix} = \begin{bmatrix} 1 & -1/2 & -1/2 \\ 1 & \sqrt{3}/2 & -\sqrt{3}/2 \end{bmatrix} \begin{bmatrix} i_{La} \\ i_{Lb} \\ i_{Lc} \end{bmatrix}$$
(12)

The computation of the real power (p) and imaginary power (q) is showed in (13). The real power and imaginary are measured instantaneously power and in matrix it is form is given as. The presence of oscillating and average components in instantaneous power is presented in (14) [17].

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$\begin{bmatrix} p \\ q \end{bmatrix} = \begin{bmatrix} v_{\alpha} & v_{\beta} \\ -v_{\beta} & v_{\alpha} \end{bmatrix} \begin{bmatrix} i_{\alpha} \\ i_{\beta} \end{bmatrix}$		(13)
$p = \overline{p} + \widetilde{p}$; $q = \overline{q} + \widetilde{q}$		(14)

Where $\bar{p} =$ direct component of real power, $\tilde{p} =$ fluctuating component of real power, $\bar{q} =$ direct component of imaginary power, $\tilde{q} =$ fluctuating component of imaginary power. The total imaginary power (q)and the fluctuating component of real power are selected as power references and current references and are utilized through the use of (15) for compensating harmonic and reactive power [18].

$$\begin{bmatrix} i_{c\alpha}^* \\ i_{c\beta}^* \end{bmatrix} = \frac{1}{v_{\alpha}^2 + v_{\beta}^2} \begin{bmatrix} v_{\alpha} & v_{\beta} \\ v_{\beta} & -v_{\alpha} \end{bmatrix} \begin{bmatrix} -\widetilde{p} + \overline{p}_{loss} \\ -q \end{bmatrix}$$
(15)

The signal \bar{p}_{loss} , is obtained from voltage regulator and is utilized as average real power. It can also be specified as the instantaneous active power which corresponds to the resistive loss and switching loss of the UPQC. The error obtained on comparing the actual DC-link capacitor voltage with the reference value is processed in FLC, engaged by voltage control loop as it minimizes the steady state error of the voltage across the DC link to zero. The compensating currents $(i_{c\alpha}^*, i_{c\beta}^*)$ as required to meet the power demand of load are shown in (15). These currents are represented in α - β coordinates. The phase current required to acquire using (16) for compensation. These source phase currents $(i_{s\alpha}^*, i_{sb}^*, i_{sc}^*)$ are represented in a-b-c axis obtained from the compensating current in the α - β coordinates presented in (16) [18].Figure 6 shows a control of shunt active filter.

$$\begin{bmatrix} i_{sa}^{*} \\ i_{sb}^{*} \\ i_{sc}^{*} \end{bmatrix} = \sqrt{\frac{2}{3}} \begin{bmatrix} 1 & 0 \\ -1/2 & \sqrt{3}/2 \\ -1/2 & -\sqrt{3}/2 \end{bmatrix} \begin{bmatrix} i_{ca}^{*} \\ i_{c\beta}^{*} \end{bmatrix}$$
(16)



Figure 6.Control strategy of shunt active filter

The proposed model of UPQC-BES system supplied by three RE sources is shown in Figure 1. From the figure, we can see that PV is connected to the DC link through a DC-DC boost converter circuit. The PV partially distributes power to the load and the remains istransfered to three phase grid. The load consists of non linear and unbalanced load. The non-linear load is a diode rectifier circuit with the RL load type, while the unbalanced load is a three phase RC load with different R value on each phase. To be economically efficient, PV must always work in MPP condition. In this research, MPPT method used is P and O algorithm. The model is also applied for UPQC-BES system which is supplied by wind and PV-wind hybrid respectively. In order to operate properly, UPQC-BES system device must have a minimum DC link voltage (V_{dc}). The value of common DC link voltage depends on the nstantaneous energy avialable to UPQC is defined by in (17) [16]:

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$$V_{dc} = \frac{2\sqrt{2}V_{LL}}{\sqrt{3}m} \tag{17}$$

where m is modulation index and V_{LL} is the AC grid line voltage of UPQC. Considering that modulation index as 1 and forline to line grid voltage ($V_{LL} = 380$ volt), the V_{dc} is obtained 620,54 volt and selected as 650 volt.

The input of shunt active filter showed in Figure 5 is DC voltage (V_{dc}) and reference DC voltage (V_{dc}^*), while the output is \overline{p}_{loss} by using PI controller. Then, the \overline{p}_{loss} is as one of input variable to generate the reference source current (I_{sa}^* , I_{sb}^* , and I_{sc}^*). The reference source current output is then compared to source current (I_{sa} , I_{sb} , and I_{sc}) by the current hysteresis control to generate trigger signal in IGBT circuit of shunt active filter. In this research, FLC as DC voltage control algorithm on shunt active filter is proposed and compared with PI controller. The FLC is capable of reduce oscilation and generate quick convergence calculation during disturbances. This method is also used to overcome the weakness of PI controller in determining proportional gain (K_p) and integral gain constant (K_i) which still use trial and error method.

2.6. Fuzzy logic controller

The research is started by determine \bar{p}_{loss} as the input variable to result the reference source current on current hysteresis controller to generate trigger signal on the IGBT shunt active filter of UPQC using PI controller ($K_p = 0.2$ and $K_i = 1.5$). By using the same procedure, \bar{p}_{loss} is also determined by using FLC. The FLC has been widely used in recent industrial processes because it has heuristic, simpler, more effective and has multi rule based variables in both linear and non-linear system variations. The main components of FLC are fuzzification, decision making (rulebase, database, reason mechanism) and defuzzification in Figure 7.

	Fuzzy Logic Controller	Table 2. Fuzzy Rule Base								
V _{dc}	$\begin{array}{c} V_{de,srow} \\ \hline \\ Fuzzification \\ \hline \\ \Delta V_{de}, gray \\ \hline \\ \hline \\ \hline \\ Fuzzification \\ \hline \\ $	V _{dc-} error ΔV _{dc-} error	NB	NM	NS	Z	PS	РМ	PB	
Ţ.	Reason	PB	Z	PS	PS	PM	PM	PB	PB	
V _{dc} *	Wechanism	PM	NS	Z	PS	PS	PM	PM	PB	
		PS	NS	NS	Z	PS	PS	PM	PM	
		Z	NM	NS	NS	Z	PS	PS	PM	
	Figure 7 Diagram block of FLC	NS	NM	NM	NS	NS	Z	PS	PS	
	Figure 7. Diagram block of FLC	NM	NB	NM	NM	NS	NS	Z	PS	
		NB	NB	NB	NM	NM	NS	NS	Z	

The fuzzy rule algorithm collects a number of fuzzy control rules in a particular order. This rule is used to control the system to meet the desired performance requirements and they are designed from a number of intelligent system control knowledge. The fuzzy inference of FLC using Mamdani method related to max-min composition. The fuzzy inference system in FLC consists of three parts: rule base, database, and reasoning mechanism [19]. The FLC method is performed by determining input variables V_{dc} (V_{dc-error}) and delta Vdc ($\Delta V_{dc-error}$), seven linguistic fuzzy sets, operation fuzzy block system (fuzzyfication, fuzzy rule base and defuzzification), $V_{\text{dc-error}}$ and $\Delta V_{\text{dc-error}}$ during fuzzification process, fuzzy rule base table, crisp value to determine \bar{p}_{loss} in defuzzification phase. The \bar{p}_{loss} is one of input variable to obtain compensating currents $(i_{c\alpha}^*, i_{c\beta}^*)$ in (16). During fuzzification process, a number of input variables are calculated and converted into linguistic variables based on a subset called membership function. The error Vdc (V_{dc-error}) and delta error Vdc ($\Delta V_{dc-error}$) are proposed input variable system and output variable is \overline{p}_{loss} . To translate these variables, each input and output variable is designed using seven membership functions: Negative Big (NB), Negative Medium (NM), Negative Small (NS), Zero (Z), Positive Small (PS), Positive Medium (PM) and Positive Big (PB). The membership functions of crisp input and output are presented with triangular and trapezoidal membership functions. The value of V_{dc-error} range from -650 to 650, Δ V_{dc-error} from -650 to 650, and \overline{p}_{loss} from -100 to 100. The input and output MFs are shown in Figure 8.

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After the V_{dc-error} and $\Delta V_{dc-error}$ are obtained, then two input membership functions are converted to linguistic variables and uses them as input functions for FLC. The output membership function is generated using inference blocks and the basic rules of FLC as shown in Table 1. Finally the defuzzification block operates to convert generated \overline{p}_{loss} output from linguistic to numerical variable again. Then it becomes input

variable for current hysteresis controller to produce trigger signal on the IGBT circuit of UPQC shunt active filter to reduce source current and load voltage harmonics. While simultaneously, it also improve power quality of 3P3W system under six scenarios due to the integration of three RE sources to UPQC-BES system.

3. RESULTS AND ANALYSIS

The analysis of proposed model is investigated through determination of six disturbance scenarios i.e. (1) NL, (2) Unba-NL, (3) Dis-NL, (4) Sag-NL, (5) Swell-NL, and (6) Inter-NL. Each scenario of UPQC uses PI controller and FLC so total number of disturbance are 12 scenarios.By using Matlab/Simulink, the model is then executed according to the desired scenario to obtain curve of source voltage (V_s), load voltage (V_L), compensation voltage (V_c), source current (V_s), load current (I_L), and DC voltage DC link (V_{dc}). Then, THD value of source voltage, source current, load voltage, and load current in each phase as well as average THD value (Avg THD) are obtained base on the curves. THD in each phase is determined in one cycle started at t = 0.35 s. The results of average of source voltage, source current, load voltage, and voltage, and load current of 3P3W system using UPQC-BES system supplied by three RE sources i.e. PV, wind, and PV-wind hybrid are presented in Table 2, 3, and 4. Next THD in each phase and average THD are showed in Table 5, 6 and 7.

	Table 2. Voltage and Current of 3P3W System Using UPQC-BES System Supplied by PV																
C	So	urce Vo	ltage V _S	(V)		Load Voltage V _L (V)				Source Current I _S (A)				Load Current I _L (A)			
Sch	Ph A	Ph B	Ph C	Avg	Ph A	Ph B	Ph C	Avg	Ph A	Ph B	Ph C	Avg	Ph A	Ph B	Ph C	Avg	
PI Controller																	
1	309.6	309.6	309.6	309.6	307.6	307.8	307.7	307.7	7.766	7.793	7.759	7.773	8.528	8.529	8.533	8.530	
2	307.4	308.0	308.0	307.8	308.3	308.7	308.3	308.4	31.00	24.84	28.73	28.15	22.50	34.12	34.52	30.38	
3	309.6	309.6	309.6	309.6	313,8	314.3	317.4	317.4	7.897	7.919	7.867	7.895	8.748	8.704	8.785	8.746	
4	154.5	154.5	154.5	154.5	307.1	307.3	307.3	307.2	7.235	7.276	7.226	7.246	8.509	8.514	8.510	8.511	
5	464.7	464.7	464.7	464.7	308.6	308.7	308.6	308.6	7.979	7.980	7.964	7.975	8.550	8.553	8.554	8.553	
6	0.536	1.385	0.850	0.924	310.2	259.8	290.2	286.7	7.392	12.67	6.045	8.703	8.707	7.747	7.637	8.031	
							Fuzzy l	Logic Cor	troller								
1	309.5	309.5	309.5	309.5	307.7	307.9	307.7	307.8	8.420	8.426	8.416	8.421	8.527	8.532	8.531	8.530	
2	307.4	307.9	308.0	307.8	308.5	308.7	308.4	308.5	31.66	25.50	29.36	28.84	22.52	34.11	35.52	30.72	
3	309.6	309.5	309.5	309.5	313.4	312.9	315.9	314.1	8.516	8.565	8.496	8.526	8.741	8.677	8.736	8.718	
4	154.4	154.4	154.4	154.4	307.3	307.3	307.2	307.3	8.563	8.560	8.561	8.561	8.514	8.517	8.512	8.515	
5	464.6	464.6	464.6	464.6	308.6	308.8	308.6	308.7	8.396	8.389	8.389	8.392	8.552	8.556	8.554	8.554	
6	0.447	0.392	0.380	0.407	314.0	293.4	304.9	304.1	4.024	3.778	3.608	3.804	8.874	8.195	8.193	8.421	

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	Tal	ble 3. V	/oltage	e and C	urrent	of 3P3	W Sys	tem U	sing U	PQC-I	BES S	ystem	supplie	ed by V	Wind	
Can	Sc	ource Vol	tage V _S (V)	L	oad Volt	age V _L (V	0	S	ource Cu	rrent I _S (A	A)	I	.oad Cur	rent I _L (A)
Sch	Ph A	Ph B	Ph C	Avg	Ph A	Ph B	Ph C	Avg	Ph A	Ph B	Ph C	Avg	Ph A	Ph B	Ph C	Avg
							Pl	Control	ler							
1	309.5	309.6	309.6	309.6	308.6	308.6	308.2	308.5	7.863	7.875	7.840	7.869	8.554	8.553	8.546	8.551
2	307.4	308.0	308.0	308.0	308.9	309.2	308.7	308.9	31.07	24.97	28.81	28.28	225 5	34.17	34.57	30.43
3	309.6	309.5	309.6	309.6	312.9	312.9	315.4	313.8	7.993	8.015	7.947	7.985	8.817	8.682	8.741	8.747
4	154.5	154.5	154.5	154.5	308.0	308.1	307.8	307.9	7.428	7.455	7.368	7.417	8.527	8.535	8.532	8.531
5	464.7	464.7	464.7	464.7	309.3	309.3	309.0	309.2	8.015	8.020	8.002	8.012	8.564	8.573	8.568	8.568
6	1.256	1.022	0.592	0.957	234.0	316.4	274.0	274.8	11.27	9.866	7.028	9.388	5.958	8.697	8.204	7.619
							Fuzzy l	Logic Co	ntroller							
1	309.5	309.5	309.5	309.5	308.5	308.6	308.3	308.5	8.418	8.410	8.414	8.414	8.545	8.552	8.549	8.549
2	307.4	307.9	308.0	307.8	309.0	309.3	308.9	309.1	31.64	25.47	29.34	28.82	22.56	34.18	34.59	30.44
3	309.5	309.5	309.5	309.5	313.2	313.7	314.1	313.7	8.519	8.531	8.531	8.527	8.713	8.714	8.718	8.715
4	154.4	154.4	154.4	154.4	308.0	308.1	307.7	307.9	8.557	8.539	8.561	8.552	8.528	8.541	8.525	8.531
5	464.6	464.7	464.7	464.7	309.2	309.3	309.2	309.2	8.391	8.385	8.388	8.388	8.565	8.570	8.567	8.567
6	0.357	0.396	0.397	0.383	303.7	300.0	315.3	306.4	3.358	3.464	3.542	3.420	8.557	8.418	8.731	8.569

12	Sc	urce Vol	tage Ve (V)	L	oad Volta	ge Vr (V)	S	ource Cu	rrent Ie (A)	1	oad Cur	rent Ir (A	0
Scn	Ph A	Ph B	PhC	Avg	Ph A	Ph B	PhC	Avg	Ph A	Ph B	PhC	Avg	Ph A	Ph B	Ph C	Avg
							PI	Controll	er							
1	309.6	309.6	309.6	309.6	307.8	308.0	307.7	307.8	7.790	7.802	7.770	7.787	8.527	8.537	8.533	8.533
2	307.4	308.0	308.0	307.8	308.4	308.8	308.4	308.6	31.02	24.87	28.74	28.21	22.52	34.13	34.53	31.40
3	309.6	309.5	309.6	309.6	314.0	315.5	316.9	315.5	7.942	7.939	7.918	7.933	8.739	8.750	8.783	8.757
4	154.5	154.5	154.5	154.5	307.3	307.4	307.2	307.3	7.289	7.309	7.251	7.283	8.513	8.516	8.515	8.515
5	464.7	464.7	464.7	464.7	308.7	308.9	308.7	308.8	7.985	7.985	7.975	7.982	8.552	8.558	8.558	8.556
6	1.048	0.825	0.845	0.906	247.5	300.7	303.7	283.9	5.119	5.927	9.271	6.773	7.016	7.893	8.793	7.867
							Fuzzy I	logic Co	ntroller							
1	309.5	309.5	309.5	309.5	307.8	308.0	307.7	307.8	8.419	8.418	8.409	8.413	8.529	8.539	8.533	8.534
2	307.4	307.9	308.0	307.8	308.7	308.7	308.9	308.8	31.66	25.47	29.32	28.82	22.54	34.13	34.56	30.41
3	309.5	309.5	309.5	309.5	314.4	315.5	316.6	315.5	8.581	8.593	8.568	8.581	8.761	8.722	8.761	8.748
4	154.4	154.4	154.4	154.4	307.3	307.5	307.3	307.4	8.566	8.572	8.563	8.567	8.511	8.520	8.519	8.517
5	464.6	464.6	464.6	464.6	308.8	308.8	308.7	308.8	8.391	8.394	8.396	8.394	22.33	22.35	22.36	22.35
6	0.412	0.403	0.402	0.418	311.6	295.7	310.4	305.9	3.774	3.544	3.593	3.640	8.855	8.321	8.288	8.488

Table 2 shows UPQC-BES system supplied PV connected 3P3W system using PI and FLC, disturbance scenarios 1 to 5 produce an average load voltage above 307 V. While in scenario 6, FLC produces a higher average load voltage of 304.1 V than if using a PIof 286.7 V. If reviewed from average source current with PI, the highest and lowest average source currents are generated by disturbance scenarios 2 and 4 of 28.15 A and 7,246 A. Whereas if using FLC the highest and lowest average source currents are achieved in scenario 2 and 6 of 28.84 A and 3.804 A.Table 3 shows UPQC-BES supplied by windconnected to 3P3W with PI and FLC, scenarios 1 to 5 is able to obtain a stable load voltage above 308 V. The difference is that in scenario 6, PI generates a load voltage of 274.8 V, otherwise if using FLC, load voltage increases to 306.4 V. If reviewed from source current using PI, the highest and lowest average source currents are achieved in scenario 2 and 6 of 28.82 A and 7.417 A. Rather, if using FLC, the highest and lowest average source currents are achieved in scenario 2 and 6 of 28.82 A and 3,420 A. Table 4 shows UPQC-BES supplied PV-wind hybrid connected 3P3W using PI and FLC, scenarios 1 to 5 produce an average load voltage above 307 V. While in scenario 2 and 6 of 28.82 A and 3,420 A. Table 4 shows UPQC-BES supplied PV-wind hybrid connected 3P3W using PI and FLC, scenarios 1 to 5 produce an average load voltage above 307 V. While in scenario 2 and 4 of 28.21 A and 6,773 A. Otherwise if using FLC the highest and lowest average source currents are resulted by scenarios 2 and 4 of 28.21 A and 6,773 A. and 3,640 A respectively.

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		Та	ble 5.	Harm	onics	of 3P3	W Sys	stem U	sing UI	QC-BE	ES Syste	em Sup	plied b	y PV		
C	Sou	rce Volta	ge THD	(%)	Lo	ad Volta	ge THD ((%)	S	ource Curr	ent THD (%)		Load Cu	rrent (%)	
Sch	Ph A	Ph B	Ph C	Avg	Ph A	Ph B	Ph C	Avg	Ph A	Ph B	Ph C	Avg	Ph A	Ph B	Ph C	Avg
								PI Co	ontroller							
1	2.35	2.36	2.32	2.34	2.48	2.50	2.46	2.48	12.89	12.72	12.92	12.84	22.32	22.34	22.32	22.33
2	2.29	2.20	2.24	2.24	2.43	2.23	2.37	2.34	2.660	2.330	2.240	2.410	5.230	2.070	2.660	3.320
3	5.84	5.86	5.94	5.88	6.36	5.90	6.58	6.28	12.75	12.64	13.06	12.82	21.92	22.16	22.33	22.14
4	4.69	4.75	4.81	4.75	2.46	2.48	2.53	2.49	14.26	13.96	14.16	14.13	22.28	22.31	22.28	22.29
5	1.56	1.53	1.55	1.55	2.47	2.43	2.45	2.45	12.51	12.36	12.44	12.44	22.34	22.32	22.32	22.33
6	NA	NA	NA	NA	32.11	15.09	28.54	25.25	270.90	145.89	275.67	230.82	47.70	34.58	36.29	39.53
							F	uzzy Log	ic Control	ler						
1	2.35	2.33	2.35	2.34	2.48	2.46	2.49	2.47	11.83	11.82	11.84	11.83	22.33	22.32	22.33	22.33
2	2.25	2.27	2.20	2.24	2.39	2.41	2.34	2.38	2.620	2.400	2.220	2.413	5.230	2.100	2.640	3.323
3	5.83	5.88	5.93	5.88	6.23	5.93	6.69	6.28	11.83	11.90	12.14	11.96	21.84	22.34	22.53	22.24
4	4.71	4.76	4.79	4.75	2.46	2.48	2.50	2.48	11.91	11.88	11.86	11.89	22.27	22.32	22.32	22.31
5	1.55	1.54	1.54	1.54	2.45	2.44	2.46	2.45	11.90	11.84	11.85	11.86	22.36	22.33	22.35	22.35
6	NA	NA	NA	NA	13.05	6.60	11.15	10.27	30.61	34.72	31.57	32.30	24.25	24.25	24.71	24.40

Table 6. Harmonics of 3P3W System Using UPQC-BES System Supplied by Wind

Con	Sou	ce Volta	ge THD	(%)	Lo	ad Volta	ge THD ((%)	S	ource Curr	ent THD (9	%)		Load Cu	rrent (%)	
Sell	Ph A	Ph B	Ph C	Avg	Ph A	Ph B	Ph C	Avg	Ph A	Ph B	Ph C	Avg	Ph A	Ph B	Ph C	Avg
								PI Co	ntroller							
1	1.88	1.87	1.94	1.89	1.99	1.97	2.05	2.00	12.63	12.37	12.70	12.57	12.30	12.30	12.34	12.31
2	1.83	1.76	1.82	1.80	1.92	1.85	1.93	1.90	2.460	2.070	2.200	2.240	5.260	2.070	2.690	3.340
3	5.67	5.71	5.77	5.72	6.00	6.83	6.02	6.28	12.48	12.26	12.66	12.47	22.01	22.12	22.08	22.07
4	3.76	3.86	3.86	1.83	1.97	2.02	2.03	2.01	13.59	13.17	13.51	13.42	22.29	22.31	22.30	22.30
5	1.26	1.24	1.29	1.26	1.99	1.97	2.05	2.00	12.31	12.20	12.31	12.27	22.36	22.33	22.37	22.35
6	NA	NA	NA	NA	14.09	35.59	34.73	28.14	157.76	139.01	266.07	186.95	37.60	34.39	46.97	39.65
							Fu	izzy Log	ic Controll	er						
1	1.89	1.88	1.93	1.90	1.99	1.98	2.04	2.00	11.71	11.72	11.77	11.73	22.34	22.31	22.32	22.32
2	1.85	1.79	1.78	1.81	1.95	1.87	1.88	1.90	2.43	2.11	2.12	2.220	5.240	2.070	2.700	3.240
3	5.67	5.71	5.78	5.72	5.99	6.39	6.13	6.17	11.72	11.62	11.90	11.75	22.08	21.94	22.47	22.16
4	3.79	3.81	3.86	3.82	1.97	1.99	2.03	1.99	11.72	11.69	11.74	11.72	22.28	22.30	22.35	22.31
5	1.27	1.24	1.28	1.26	2.00	1.96	2.04	2.00	11.66	11.76	11.76	11.73	22.31	22.33	22.35	22.33
6	NA	NA	NA	NA	7.59	6.44	10.95	8.33	27.33	28.27	26.39	27.33	25.39	23.65	24.31	24.45

Table 7 Harmonics of 3P3W S	vetom Using UPOC-BES Sy	actom Supplied by	PV_Wind Hybrid
	vsicin Using UI OC-DES Sy	such supplied by	I v - vv mu IIvonu

Con	Sou	ce Volta	ge THD	(%)	Loa	d Voltag	e THD (%)	S	ource Curr	ent THD (%)		Load Cu	rrent (%))
Sch	Ph A	Ph B	Ph C	Avg	Ph A	Ph B	Ph C	Avg	Ph A	Ph B	Ph C	Avg	Ph A	Ph B	Ph C	Avg
								PI Co	ntroller							
1	2.25	2.19	2.29	2.24	2.37	2.31	2.42	3.37	12.85	12.62	12.74	12.74	22.33	22.31	22.34	22.33
2	2.18	2.08	2.15	2.13	2.30	2.19	2.18	2.22	2.630	2.300	2.290	2.407	5.230	2.070	2.670	3.323
3	5.81	5.82	5.89	5.84	6.12	5.88	6.75	6.25	12.71	12.63	12.98	12.77	22.05	22.13	22.54	22.24
4	4.53	4.48	4.51	4.51	2.37	2.35	2.37	2.36	14.16	13.50	13.99	13.88	22.27	22.30	22.28	22.28
5	1.49	1.46	1.51	1.49	2.37	2.31	2.40	2.36	12.43	12.29	12.41	12.38	22.34	22.32	22.33	22.33
6	NA	NA	NA	NA	18.61	36.38	28.42	27.8	387.71	330.34	189.29	302.45	36.73	38.51	36.83	37.36
							Fu	zzy Log	ic Control	ler						
1	2.25	2.23	2.25	2.24	2.37	2.35	2.39	2.37	11.85	11.74	11.84	11.81	22.32	22.31	22.33	22.32
2	2.23	2.15	2.05	2.14	2.37	2.26	2.17	2.26	2.520	2.410	2.140	2.446	5.230	2.070	2.690	3.330
3	5.80	5.83	5.90	5.84	6.57	5.26	7.06	6.29	11.83	11.78	12.24	11.95	22.15	22.23	22.95	22.44
4	4.53	4.52	4.54	4.86	2.36	2.35	2.35	2.35	11.79	11.74	11.84	11.79	22.29	22.30	22.29	22.29
5	1.48	1.46	1.51	1.48	2.35	2.32	2.40	2.35	11.78	11.81	11.81	11.80	22.33	22.35	22.36	22.35
6	NA	NA	NA	NA	10.30	4.90	10.25	8.48	27.44	29.52	28.63	28.53	23.20	23.97	24.65	23.94

Table 5 shows that average THD of load voltage (V_L) of UPQC-BES system supplied by PV in 3P3W system for scenarios 1 to 5 using PI control is within limits in IEEE 519. The highest and lowest average THD load voltages are achieved under scenario 6 and 2 as 25.25% and 2.34% respectively. PI controller is also able to migitate average THD source voltage in scenario 6 from not accessible (NA) to 25.25% on the load side. The highest and lowest average THD of source current are achieved in scenario 6 and 2 as 230.82% and 2.41%. Table 5 also indicates that average THD of load voltage of UPQC system supplied by PV with BES using FLC in scenarios 1 to 5, has fulfilled limits in IEEE 519. The highest and lowest average THD of load voltage are achieved under scenario 6 and 2 of 10.27% and 2.38%. The use of FLC method is also able to reduce average THD of source current are achieved in scenario 6 and 2 of 32.30% and 2.413%.

Table 6 shows that average THD of load voltage of UPQC-BES system supplied by wind in 3P3W system for interference scenarios 1 to 5 using PI is within limits prescribed in IEEE 519. The highest and lowest average THD load voltages is achieved under scenario 6 and scenario 2 as 28.14% and 1.90% respectively. PI controller is also able to reduce average THD source voltage in scenario 6 from NA to 28.14% on the load side. The highest and lowest average THD of source current areachieved in scenario 6

and 2 as 186.95% and 2.24% respectively. Table 6 also shows that average THD of load voltage of UPQC-BES supplied by wind using FLC in scenarios 1 to 5, has fulfilled limits prescribed in IEEE 519. The highest and lowest average THD of load voltage are achieved under scenario 6 and 4of 8.33% and 1.90%. FLC method is also able to reduce average THD on source voltage in scenario 6 from NA to 7.33% on load side. The highest and lowest average THD source current are achieved in scenario 6 and 2 of 27.33% and 2.22%. Table 7shows that average THD of load voltage (VL) of UPQC-BES system supplied by PV-wind hybrid in 3P3W system for scenarios 1 to 5 using PI is within limits in IEEE 519. The highest and lowest average THD load voltages are achieved under scenario 6 and 2 as 27.8% and 2.22% respectively. PI is also able to migitate average THD source voltage in scenario 6 from NA to 27.8% on load side. The highest and lowest average THD of source current are achieved in scenario 6and 2 as 302.45% and 2.407% respectively. Table 7 also indicates that average THD of load voltage of UPQC-BES system supplied by PV-wind hybrid using FLC for scenarios 1 to 5, has fulfilled limits in IEEE 519. The highest and lowest average THD of load voltage are achieved under scenario 6 and 2 of 8.48% and 2.26%. FLC method is also able to reduce average THD on source voltage in scenario 6 from NA to 8.48% on load side. The highest and lowest average THD of source current are achieved in scenario 6and 2 of 28.53% and 2.446%. Overall for UPQC-BES systemsystem supplied by three RE sources in scenarios 1 to 5 using PI and FLC is able to improve average THD of source current better on average THD of load current. Figure 9 presents UPQC-BES system performance supplied by three RE sources using FLC in scenario 6.



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c. (vi) DC Link Voltage for UPQC-BES + PV-Wind Hybrid

Figure 9.UPQC-BES system performance using FLC in scenario 6 (Inter-NL)

Figure 9.a.(i) shows that in scenario 6, UPQC-BES system supplied by PV at t = 0.2 s to t = 0.5 s, average source voltage (Vs) falls as 100% to 0.4062 V. During the disturbance, PV is able to generate power to UPQC DC link and injecting full average compensation voltage (V_C) in Figure 9.a.(iii) through injection transformer on series active filter so that average load voltage (VL) in Figure 9.a.(ii) remains stable at 304.1 V. As long as fault period, although nominal of average source current (I_S) in Figure 9.a.(iv) drops to 3.804 A, combination of PV and BES is able to generate power, store excess energy of PV, and inject current into load through shunt active filter so that average load current (IL) in Figure 9.a.(v) remains as 8.421 A.Figure 9.b.(i) presents on UPQC-BES supplied by wind at t = 0.2 s to t = 0.5 s average source voltage (V_s) drops 100% to 0.3828 V. During the disturbance, wind is able to generate power to UPQC DC link and injecting full average compensation voltage (V_C) in Figure 9.b.(iii) through injection transformer on series active filter so that average load voltage (VL) in Figure 9.b.(ii) remains stable at 306.4 V. During fault period, although nominal of average source current (Is) falls to 3.420 A, combination of wind and BES is able to generate power, store excess energy of wind, and inject current into load through shunt active filter so that average load current (IL) in Figure 9.b.(v) remains as 8.569 A.Figure 9.c.(i) indicates on UPQC-BES supplied by PV-Wind Hybrid at t = 0.2 s to t = 0.5 s average source voltage (V_S) drops 100% to 0.4175 V. During the disturbance, PV-wind hybrid is able to generate power to UPQC DC link and injecting full average compensation voltage (V_C) in Figure 9.c.(iii) through injection transformer on series active filter so that average load voltage (VL) in Figure 9.b.(ii) remains stable at 305.9V. As long as disturbance period, although nominal of average source current (Is) falls to 3.640 A, combination of PV-wind hybrid and BES is able to generate power, store excess energy of wind, and inject current into load through shunt active filter so that average load current (IL) in Figure 9.c.(v) remains as 8.488 A.Figure 10 shows spectra of load voltage harmonics on phase A of UPQC-BES system supplied by three RE sources using FLC in scenario 6. Figure 11 shows performance of average THD of load voltage and source current on UPQC-BES system supplied by three RE sources.







Figure 10. Spectra of load voltage harmonics on phase A of UPQC-BES using FLC in scenario 6 (Inter-NL)



Figure 11. Performance of UPQC-BES supplied by three RE sources using PI and FLC

Figure 11(a) shows that in scenario 1 to 5, the implementation of FLC on UPQC-BES system supplied by three RE sources is able to obtain average THD of load voltage slightly better than PI controller and both method have already met the limit in IEEE 519. Further under scenario 6, FLC applied on UPQC-BES system supplied by three RE sources gives significantly better result of average THD of load voltage than PI controller. In six disturbance scenarios, both PI controller and FLC applied on UPQC-BES system supplied by three RE sources, PV is able to obtain the highest average THD of load voltages. Figure 11(b) shows that in disturbance scenario 1 to 5, implementation of FLC on UPQC-BES system supplied by three RE sources is able to obtain average THD of source current slightly better than PI controller. Furthermore under scenario 6, FLC applied on UPQC-BES system supplied by three RE sources gives significantly better result of average THD of source current than PI controller. Both PI controller and FLC on UPQC-BES system supplied by three RE sources in six disturbance scenarios, PV is able to obtain the highest average THD of source current.

4. CONCLUSION

Comparative performance analysis of UPQC-BES system supplied by three RE sources i.e. PV, wind, and PV-wind hybrid respectively using PI controller and FLC have been discussed. In disturbance scenario 1 to 5, implementation of FLC on UPQC-BES system supplied by three RE sources is able to obtain average THD of load voltage slightly better than PI and both methods have already met the limit in IEEE 519. Under scenario 6, FLC applied on UPQC-BES system supplied by three RE sources gives significantly better result average THD of load voltage than PI. In six disturbance scenarios, both PI and FLC applied on UPQC-BES system supplied by three RE sources THD of load voltage than PI. In six disturbance scenarios, both PI and FLC applied on UPQC-BES system supplied by three RE sources, PV is able to obtain the highest average THD of load

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voltage. In interference scenario 1 to 5, FLC method on UPQC-BES system supplied by three RE sources is able to obtain average THD of source current slightly better than PI. Furthermore under scenario 6, FLC applied on UPQC-BES system supplied by three RE sources gives significantly better result of average THD of source current than PI. Both PI and FLC on UPQC-BES system supplied by three RE sources in six scenarios, PV is able to obtain the highest average THD of source current.

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APPENDIX

Three phase grid: RMS voltage 380 volt (L-L), 50 Hz, line impedance: $R_s = 0.1$ Ohm $L_s = 15$ mH; series and shunt active filter: series inductance $L_{se} = 0.015$ mH; shunt inductance $L_{sh} = 15$ mH; injection transformers: rating 10 kVA, 50 Hz, turn ratio (N_1/N_2) = 1:1; non linear load: resistance $R_L = 60$ ohm, inductance $L_L = 0.15$ mH, load impedance $R_e = 0.4$ ohm and $L_c = 15$ mH; unbalance load: resistance $R_1 = 24$ ohm, $R_2 = 12$ ohm, and $R_3 = 6$ ohm, capacitance $C_1, C_2, C_3 = 2200$ µF; DC-link: voltage $V_{DC} = 650$ volt and capacitance $C_{DC} = 3000$ µF; battery energe storage: type = nickel metal hybrid, DC voltage = 650 volt, rated capacity = 200 Ah, initial SOC = 100%, inductance $L_1 = 6$ mH, capacitance $C_1 = 200$ µF; photovoltaic: active power = 0.6 kW temperature = 25^o C, irradiance = 1000 W/m²; PMSG wind turbine active power = 0.6 kW, voltage = 380 volt, 50 Hz, wind speed = 5 m/s, picth angle = 2; PI controller: $K_p = 0.2$, $K_i = 1.5$; fuzzy model: method = mamdani, composition = max-min; input membership function: error (V_{dc}) = trapmf, trimf delta error (ΔV_{dc}) = trapmf, trimf; output membership function: \bar{p}_{loss} = trapmf, trimf.

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Lampiran 2.4 Revisi kedua makalah

Matlab/simulink simulation of unified power quality conditioner-battery energy storage system supplied by PV-wind hybrid usingfuzzy logic controller

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Article Info

ABSTRACT

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This paper presents performance analysis of Unified Power Quality Conditioner-Battery Energy Storage (UPQC-BES) system supplied by Photovoltaic (PV)-Wind Hybrid connected to three phase three wire (3P3W) of 380 volt (L-L) and 50 hertz distribution system. The performance of supply system is compared with two renewable energy (RE) sources i.e. PV and Wind, respectively. Fuzzy Logic Controller (FLC) is implemented to maintain DC voltage across the capacitor under disturbance scenarios of source and load as well as to compare the results with Proportional Intergral (PI) controller. There are six scenarios of disturbance i.e. (1) non-linear load (NL), (2) unbalance and nonlinear load (Unba-NL), (3) distortion supply and non-linear load (Dis-NL), (4) sag and non-linear load (Sag-NL), (5) swell and non-linear load (Swell-NL), and (6) interruption and non-linear load (Inter-NL). In disturbance scenario 1 to 5, implementation of FLC on UPQC-BES system supplied by three RE sources is able to obtain average THD of load voltage/source current slightly better than PI. Furthermore under scenario 6, FLC applied on UPQC-BES system supplied by three RE sources gives significantly better result of average THD of load voltage/source current than PI. This research is simulated using Matlab/Simulink.

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1. INTRODUCTION

PV and windare the most REdistributed generations (DGs) because they are able to convertsunlight and wind into power. PV and solararethepotential DGs sources since it only need sunlight to generate electricity, where the resources are available in abundance, free and relatively clean. Indonesia has enormous energy potential from the sunbecause it lies on the equator. Almost all areas of Indonesia get sunlight about 10 to 12 hours per day, with an average intensity of irradiation of 4.5 kWh/m² or equivalent to 112.000 GW. The potential of wind energy in Indonesia generally has a speed between 4 to 5 m/s and classified as medium scale with potential capacity of 10 to 100 kW. The weakness of PV and wind turbine besidesable to generate power, they also produces a number voltage and current harmonics resulted bypresence of several types of PV and wind turbine devices and power converters as well as to increase a number of non-linear loads connected to the grid, so finally resulting inthe decrease in power quality.

In order to overcome and improve power quality due to presence of non-linear loads and integration of PV and wind turbine to grid, UPQC is a proposed. UPQCserves to compensate for source voltage quality problemsi.e. sag, swell unbalance, flicker, harmonics, and load current quality problems i.e. harmonics,

unbalance, reactive currents, and neutral current. B. Han et. al and Vinod Khadkikar have investigated UPQC as one part of active power filter consisting of shunt and series active filters connected in parallel and serves as superior controller to overcome a number of power quality problems simultaneously. Series component has been responsible for reducing a number of interference on source side i.e. voltage sag/swell, flicker, unbalanced voltage, and harmonics. Shunt component has been responsible for addressing a current quality problems i.e. low power factor, load current harmonics, and unbalanced load. [1,2].UPQC based on RE has been investigated by some researchers. There are two methods used to overcome this problem i.e. using conventional and artificial intelligence.Shafiuzzaman K.K., et.al have proposed system includes a series inverter, shunt inverter, and a DG connected to a DC link through a rectifier using PI. The system was capable of increase source voltage quality i.e. sag and interruption and load current quality, as well as transfer of active power on/off grid mode [3]. The influence of DG on UPQC performance in reducing sag under conditions of some phase to ground faults to using DSTATCOM has been implemented byNorshafinash S., et.al.The DG was effective enough to help UPQC to improve sag [4]. It was connected in series with load resulting better sagmigitationcompared to system without DG. Implementation of UPOC using UVTG method with PI to reduce sag, swell, voltage/current harmonics has been donebyS. N. Gohil, et.al. Simulation of voltage distortion was made by adding 5th and 7th harmonics at fundamental source voltage, resulting in a reduction of THD source current and THD load voltage [5].

UPQC supplied byPV panels using boost converter, PI, MPPT P and O, and p-q theoryhas been proposed byYahiaBouzelata at.al[6]. The system was capable of compensate reactive power and reduce source current/load voltage harmonics, butdid not discuss migitation of sag and interuption caused by PV penetration. Power quality enhancement of sag and source voltage harmonics on grid using UPQC supplied by PV array connected to DC link using PI compared with FLC has been done by Ramalengswara Rao, et.al. Combination of UPQC and PV using FLC can improve source voltage THD better than PI [7]. Amirullah et.al haveresearched a method for balancing current and line voltage, as a result of DGs of a single phase PV generator unit in randomly installed at homes through on a three phase four wire 220 kV and 50 Hz distribution line using BES and three of single phase bidirectional inverter. Both devices was capable of reduce unbalanced line current/voltage, but both of them were also capable of increase current/voltage harmonics on PCC bus [8]. Power quality migitation of UPQC on microgrid supplied by PV and wind turbine has been implemented by K S Srikanth et. al. It resulted that PI and FLC was able to improve power quality and reduce distortion in output power [9]. The UPQC-wind turbine to provide active power to overcome low sag and interruption voltage to grid has been investigated by H.Toodeji, et.al. The model was used VSC as a rectifier on generator output and controlled so that maximum power desired can be generated by different speed wind turbines using PI[10]. The UPQC-wind turbine connected to UPQC DC link was implemented by M. Hosseinpour, et al. The proposed combination using PI was capable of compensate swell, interruption voltage, and reactive power both on on/off grid [11]. R.Bhavani, et, al have researched on UPQC controlled by FLC to improve power quality in a DFIG wind turbine connected grid. FLC can improve power quality i.e. sag voltage and load current harmonics better than PI[12]. Power quality enhancement on wind turbine and BES with PI connected grid on PCC bus using UPQC has been implemented by S.RajeshRajan, et al. BES was installed to maintain and stabilize active power supply under different windspeed [13].

This researchwill analyze UPQC-BES performance supplied by PV-wind hybrid connected to 3P3W of 380 volt (L-L) and 50 hertz distribution system. The performance of supply system is compared with two RE sources i.e. PV and Wind, respectively. BES serves to store excess energy produced by three RE sources and distribute it to load if necessary, to prevent interruption voltage, and to adjust charging and discharging of energy in battery. BES is also expected to store excess power produced by three RE combinations and use it as backup power. FLC is proposed and compared with PI to control variable of DC voltage and DC reference voltage input to generate reference current source in current hysteresis controller on shunt active filter. DC voltage controller in shunt active filter and series active filter is used to migitate power quality of load voltage and source current. Performance of two controllers are used to determine load voltage, source current, load voltage THD, and source current THD based on IEEE 519. This paper is presented as follow. Section 2 describes proposed method, model of UPQC-BES system supplied by three RE sources i.e. PV, wind, and PV-wind hybrid, simulation parameters, PV and PMSG wind turbine model, series and shunt active filter, as well as application of PI and FLC method for proposed model. Section 3 shows results and analysis about performance of THD analysis on the proposed model of three RE sources connected to DC link of UPQC-BES system using PI and FLC. In this section, six disturbance scenarios are presented and the results are verified with Matlab/Simulink. Finally, this paper in concluded in Section 4.

2. RESEARCH METHOD

2.1. Proposed method

Figure 1 shows proposed model in this research. The RE sources based DGs used i.e. PV, Wind Turbine, and PV-Wind Turbine Hybrid connected to 3P3W distribution system with 380 volt (L-L) and 50 Hz frequency, through UPQC-BES system. PV array produce power under fixed temperature and radiation as well as connect to UPQC-DC link through a DC/DC boost converter. The maximum power point tracking (MPPT) method with Pertub and Observer (P and O) algorithms helps PV produce maximum power and generate output voltage, as the input voltage for DC/DC boost converter. The converter serves to adjust dutycycle value and output voltage of PV as its input voltage to produce an output voltage corresponding to UPQC DC link voltage. Wind turbine type used is a permanent magnetic synchronous generator (PMSG) with variable speed and fixed voltage which generating power and is connected to UPQC DC link circuit through AC/DC bridge rectifier. The rectifier helps to change AC PSMG stator output voltage to DC voltage through LC circuit that serves to filter and smooth it before connected to UPQC-DC link.BES connected to the UPQC-DC link circuit serves as energy storage and is expected to overcome interruption voltage and overall help UPQC performance to improve voltage and current quality on source and load bus. Simulation parameters proposed in this study is shown in Appendix Section. Power quality analysis is performed on PV, Wind, PV-Wind Hybrid respectively, connected to 3P3W system through UPOC DC-link (on-grid) using BES circuit. Single phase circuit breakers (CBs) are used to connect and disconnect PV, Wind, and Hybrid PV-Wind respectively with UPQC DC-link.

There are six disturbance scenarios i.e.(1) NL, (2) Unba-NL, (3) Dis-NL, (4) Sag-NL, (5) Swell-NL, and (6) Inter-NL. In scenario 1, the model is connected a non-linear load with R_L and L_L of 60 Ohm and 0.15 mH respectively. In scenario 2, the model is connected to non-linear load and during 0.3 s since t=0.2 s to t=0.5 s connected to unbalance three phase load with R₁, R₂, R₃ as 6 Ohm, 12 Ohm, 24 Ohm respectively, and value of C₁, C₂, C₃ as 2200 µF. In scenario 3, the model is connected to non-linear load and source voltage generating 5th and 7th harmonic components with individual harmonic distortion values of 5% and 2% respectively. In scenario 4, the model is connected to non-linear load and source experiences a sag voltage disturbance of 50% for 0.3 s between t=0.2 s to t=0.5 s. In scenario 5, the model is connected to a non-linear load and source experiences a swell voltage disturbance of 50% for 0.3 s between t=0.2 s to t=0.5 s. In scenario 6, the model is connected to non-linear load and source experiences an interruption voltage interference of 100% for 0.3 s between t=0.2 s to t=0.5 s.FLC is used as a DC voltage control in a shunt active filter to improve the power quality of the load voltage and current source and compare it with PI controller. Each disturbance scenario uses a PI controller and FLC so that the total of 12 disturbances. The result analysis of research was carried out i.e. (1) voltage and current on source or poin common coupling (PCC) bus, (2) voltage and current on load bus, (3) harmonic voltage and harmonic current on source bus and (4) harmonic voltage and harmonic current on load bus. The final phase is to compare performance of UPQC-BES system on-grid supplied by PV, Wind, PV-Wind Hybrid respectively using two controllers to improve power quality of load voltage and source current under six disturbance conditions.



Figure 1. Proposed model of UPQC-BES system supplied by PV, Wind, and PV-Wind Hybrid

2.2. Photovoltaic model

Figure 2 shows the equivalent circuit and V-I characteristic of a solar panel. A solar panel is composed of several PV cells that have series, parallel, or series-parallel external connections [14].



Figure 2. Equivalent circuit and V-I characteristic of solar panel

The V-I characteristic of a solar panel is showed in (1):

$$I = I_{PV} - I_o \left[\exp\left(\frac{V + R_s I}{aV_t}\right) - 1 \right] - \frac{V + R_s I}{R_p}$$
(1)

where I_{PV} is the photovoltaic current, I_o is saturated reverse current, 'a' is the ideal diode constant, $V_t=N_SKTq^{-1}$ is the thermal voltage, N_S is the number of series cells, q is the electron charge, K is the Boltzmann constant, T is the temperature of p–n junction, R_S and R_P are series and parallel equivalent resistance of the solar panels. I_{PV} has a linear relation with light intensity and also varies with temperature variations. I_o is dependent on temperature variations. The values of I_{PV} and I_o are calculated as following (2) and (3):

$$I_{PV} = (I_{PV,n} + K_1 \Delta T) \frac{G}{G_n} I$$
⁽²⁾

$$I_o = \frac{I_{SC,n} + K_I \Delta T}{\exp(V_{OC,n} + K_V \Delta T) / aV_I - 1}$$
(3)

In which $I_{PV,n}$, $I_{SC,n}$ and $V_{OC,n}$ are photovoltaic current, short circuit current and open circuit voltage in standard conditions ($T_n=25$ C and $G_n=1000$ Wm⁻²) respectively. K_I is the coefficient of short circuit current to temperature, $\Delta T=T-T_n$ is the temperature deviation from standard temperature, G is the light intensity and K_V is the ratio coefficient of open circuit voltage to temperature. Open circuit voltage, short circuit current and voltage-current corresponding to the maximum power are three important points of I-V characteristic of solar panel. These points are changed by variations of atmospheric conditions. By using (4) and (5) which are derived from PV model equations, short circuit current and open circuit voltage can be calculated in different atmospheric conditions.

$$I_{SC} = (I_{SC} + K_1 \Delta T) \frac{G}{G_n}$$
(4)

$$V_{oc} = V_{oc} + K_v \Delta T \tag{5}$$

2.3. PMSG wind turbine

Wind turbine is onother part of an integrated system, which can be divided into two types i.e. fixed and variable speed wind turbines. In fixed speed type, rotating speedof turbine is fixed and hence, frequency of generated voltage remains constant, so it can be directly connected to the network. In this case, maximum power can not always be extracted by wind. On the other hand, on variable speed, turbine can rotate at different speeds, so maximum power can be generated in each wind speed by MPPT method [10]. The advantage of using a PMSG over a synchronous generator and DFIG machine because it has high efficiency and reliability. Due to the elimination of rotor external excitation, machine size, and cost also decreases, making PMSG be more controlled easily with feedback control system. PMSG has become an attractive solution on wind generation systems with variable speed wind turbine applications [15]. Figure 3 and 4 shows model of PMSG wind turbine and wind turbinpower characteristiccurve.



Figure 3. Model of PMSG wind turbine



Figure 4. Wind turbin power characteristic curve

The output power of wind turbine can be expressed using (6), (7), and (8) [11].

$$\lambda = \frac{\omega_r R}{V_{wind}} \tag{6}$$

$$P_M = \frac{1}{2} \rho \pi R^2 C_p V_{wind}^3 \tag{7}$$

$$T_{M} = \frac{P_{M}}{\omega_{r}} = \frac{1}{2} \rho \pi R^{5} C_{p} \frac{\omega_{M}^{3}}{\lambda^{3}}$$

$$\tag{8}$$

Where λ is the speed-tip ratio, V_{wind} is wind speed, R is blade radius, ω_r is rotor speed (rad/sec), ρ is the air density, C_P is the power coefficient, P_M is the output mechanical power, and T_M is output torque of wind turbine. The C_P coefficient is dependent on the pitch angle value, at which rotor blade can rotate along axis and tip-speed ratio λ expressed in (9).

$$C_{P} = (0.44 - 0.167\beta)\sin\frac{\pi(\lambda - 2)}{(13 - 0.3\beta)}$$
(9)

Where β is a pitch angle blade. In a fixed pitch type, the value of β is set to a fixed value.

2.4. Control of series active filter

The main function of series active filter is as a sensitive load protection against a number of voltage interference at PCC bus. The control strategy algorithm of the source and load voltage in series active filter circuit is shown in Figure 5. It extracts the unit vector templates from the distorted input supply. Furthermore, the templates are expected to be ideal sinusoidal signal with unity amplitude. The distorted supply voltages are measured and divided by peak amplitude of fundamental input voltage V_m givenin (10) [6].

$$V_m = \sqrt{\frac{2}{3} \left(V_{sa}^2 + V_{sb}^2 + V_{sc}^2 \right)}$$
(10)

A three phase locked loop (PLL) is used in order to generate a sinusoidal unit vector templates with a phase lagging by the use of sinus function. The reference load voltage signal is determined by multiplying the unit vector templates with the peak amplitude of the fundamental input voltage V_m . The load reference voltage (V_{La}^* , V_{Lb}^* , V_c^*) is then compared against to sensed load voltage (V_{La} , V_{Lb} , V_{Lc}) by a pulse width modulation (PWM) controller used to generate the desired trigger signal on series active filter.



Figure 5. Control strategy of series active filter

2.5. Control of shunt active filter

The main function of shunt active filter is migitation of power quality problems on the load side. The control methodology in shunt active filter is that the absorbed current from the PCC bus is a balanced positive sequence current including unbalanced sag voltage conditions in the PCC bus or unbalanced conditions or non-linear loads. In order to obtain satisfactory compensation caesed by disturbance due to non-linear load, many algorithms have been used in the literature. This research used instantaneous reactive power theory method "p-q theory". The voltages and currents in Cartesian *abc*coordinates can be transformed to Cartesian $\alpha\beta$ coordinates as expressed in (11) and (12) [16].

$$\begin{bmatrix} v_{\alpha} \\ v_{\beta} \end{bmatrix} = \begin{bmatrix} 1 & -1/2 & -1/2 \\ 1 & \sqrt{3}/2 & -\sqrt{3}/2 \end{bmatrix} \begin{bmatrix} V_{a} \\ V_{b} \\ V_{c} \end{bmatrix}$$
(11)

$$\begin{bmatrix} i_{\alpha} \\ i_{\beta} \end{bmatrix} = \begin{bmatrix} 1 & -1/2 & -1/2 \\ 1 & \sqrt{3}/2 & -\sqrt{3}/2 \end{bmatrix} \begin{bmatrix} i_{La} \\ i_{Lb} \\ i_{Lc} \end{bmatrix}$$
(12)

The computation of the real power (p) and imaginary power (q) is showed in (13). The real power and imaginary are measured instantaneously power and in matrix it is form is given as. The presence of oscillating and average components in instantaneous power is presented in (14) [17].

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$$\begin{bmatrix} p \\ q \end{bmatrix} = \begin{bmatrix} v_{\alpha} & v_{\beta} \\ -v_{\beta} & v_{\alpha} \end{bmatrix} \begin{bmatrix} i_{\alpha} \\ i_{\beta} \end{bmatrix}$$
(13)

$$p = \overline{p} + \widetilde{p} \quad ; q = \overline{q} + \widetilde{q} \tag{14}$$

Where \bar{p} =direct component of real power, \tilde{p} = fluctuating component of real power, \bar{q} = direct component of imaginary power, \tilde{q} = fluctuating component of imaginary power. The total imaginary power (q)and the fluctuating component of real power are selected as power references and current references and are utilized through the use of (15) for compensating harmonic and reactive power [18].

$$\begin{bmatrix} i_{c\alpha}^{*} \\ i_{c\beta}^{*} \end{bmatrix} = \frac{1}{v_{\alpha}^{2} + v_{\beta}^{2}} \begin{bmatrix} v_{\alpha} & v_{\beta} \\ v_{\beta} & -v_{\alpha} \end{bmatrix} \begin{bmatrix} -\widetilde{p} + \overline{p}_{loss} \\ -q \end{bmatrix}$$
(15)

The signal \bar{p}_{loss} , is obtained from voltage regulator and is utilized as average real power. It can also be specified as the instantaneous active power which corresponds to the resistive loss and switching loss of the UPQC. The error obtained on comparing the actual DC-link capacitor voltage with the reference value is processed in FLC, engaged by voltage control loop as it minimizes the steady state error of the voltage across the DC link to zero. The compensating currents $(i_{c\alpha}^*, i_{c\beta}^*)$ as required to meet the power demand of load are shown in (15). These currents are represented in α - β coordinates. The phase current required to acquire using (16) for compensation. These source phase currents $(i_{s\alpha}^*, i_{sb}^*, i_{sc}^*)$ are represented in a-b-c axis obtained from the compensating current in the α - β coordinates presented in (16) [18].Figure 6 shows a control of shunt active filter.

$$\begin{bmatrix} i_{sa}^{*} \\ i_{sb}^{*} \\ i_{sc}^{*} \end{bmatrix} = \sqrt{\frac{2}{3}} \begin{bmatrix} 1 & 0 \\ -1/2 & \sqrt{3}/2 \\ -1/2 & -\sqrt{3}/2 \end{bmatrix} \begin{bmatrix} i_{ca}^{*} \\ i_{c\beta}^{*} \end{bmatrix}$$
(16)



Figure 6.Control strategy of shunt active filter

The proposed model of UPQC-BES system supplied by three RE sources is shown in Figure 1. From the figure, we can see that PV is connected to the DC link through a DC-DC boost converter circuit. The PV partially distributes power to the load and the remains istransfered to three phase grid. The load consists of non linearand unbalanced load. The non-linear load is a diode rectifier circuit with the RL load type, while the unbalanced load is a three phase RC load with different R value on each phase. To be economically efficient, PV must always work in MPP condition. In this research, MPPT method used is P and O algorithm. The model is also applied for UPQC-BES system which is supplied by wind and PV-wind hybrid respectively. In order to operate properly, UPQC-BES system device must have a minimum DC link

voltage (V_{dc}). The value of common DC link voltage depends on the nstantaneous energy avialable to UPQC is defined by in (17) [16]:

$$V_{dc} = \frac{2\sqrt{2}V_{IL}}{\sqrt{3}m} \tag{17}$$

where m is modulation index and V_{LL} is the AC grid line voltage of UPQC. Considering that modulation index as 1 and forline to line grid voltage (V_{LL} =380 volt), the V_{dc} is obtained 620, 54 volt and selected as 650 volt.

The input of shunt active filter showed in Figure 5 is DC voltage (V_{dc}) and reference DC voltage (V_{dc}^*), while the output is \bar{p}_{loss} by using PI controller. Then, the \bar{p}_{loss} is as one of input variable to generate the reference source current (I_{sa}^* , I_{sb}^* , and I_{sc}^*). The reference source current output is then compared to source current (I_{sa} , I_{sb} , and I_{sc}) by the current hysteresis control to generate trigger signal in IGBT circuit of shunt active filter. In this research, FLC as DC voltage control algorithm on shunt active filter is proposed and compared with PI controller. The FLC is capable of reduce oscilation and generate quick convergence calculation during disturbances. This method is also used to overcome the weakness of PI controller in determining proportional gain (K_p) and integral gain constant (K_i) which still use trial and error method.

2.6. Fuzzy logic controller

The research is started by determine \overline{p}_{loss} as the input variable to result the reference source current on current hysteresis controller to generate trigger signal on the IGBT shunt active filter of UPQC using PI controller (K_p=0.2 and K_i=1.5). By using the same procedure, \overline{p}_{loss} is also determined by using FLC. The FLC has been widely used in recent industrial processes because it has heuristic, simpler, more effective and has multi rule based variables in both linear and non-linear system variations. The main components of FLC are fuzzification, decision making (rulebase, database, reason mechanism) and defuzzification in Figure 7.The output membership function is generated using inference blocks and the basic rules of FLC as shown in Table 1.



The fuzzy rule algorithm collects a number of fuzzy control rules in a particular order. This rule is used to control the system to meet the desired performance requirements and they are designed from a number of intelligent system control knowledge. The fuzzy inference of FLC using Mamdani method related to max-min composition. The fuzzy inference system in FLC consists of three parts: rule base, database, and reasoning mechanism [19]. The FLC method is performed by determining input variables V_{dc} (V_{dc-error}) and delta Vdc ($\Delta V_{dc-error}$), seven linguistic fuzzy sets, operation fuzzy block system (fuzzyfication, fuzzy rule base and defuzzification), V_{dc-error} and $\Delta V_{dc-error}$ during fuzzification process, fuzzy rule base table, crisp value to determine \bar{p}_{loss} in defuzzification phase. The \bar{p}_{loss} is one of input variable to obtain compensating currents ($i_{c\alpha}^{*}, i_{c\beta}^{*}$) in (16).During fuzzification process, a number of input variables are calculated and converted into linguistic variables based on a subset called membership function. The error Vdc (V_{dc-error}) and delta error Vdc ($\Delta V_{dc-error}$) are proposed input variable system and output variable is \bar{p}_{loss} . To translate these variables, each input and output variable is designed using seven membership functions: Negative Big (NB), Negative Medium (NM), Negative Small (NS), Zero (Z), Positive Small (PS), Positive Medium (PM) and Positive Big (PB). The membership functions of crisp input and output are presented with triangular and trapezoidal membership functions. The value of V_{dc-error} range from -650 to 650, $\Delta V_{dc-error}$ from -650 to 650, and \bar{p}_{loss} from -100 to 100. The input and output MFs are shown in Figure 8.



Figure 8. Membership functions (a) $V_{dc-error}$, (b) $\Delta V_{dc-error}$, and (c) \overline{p}_{loss}

After the V_{dc-error} and Δ V_{dc-error} are obtained, then two input membership functions are converted to linguistic variables and uses them as input functions for FLC. The output membership function is generated using inference blocks and the basic rules of FLC as shown in Table 1. Finally the defuzzification block operates to convert generated \bar{p}_{loss} output from linguistic to numerical variable again. Then it becomes input variable for current hysteresis controller to produce trigger signal on the IGBT circuit of UPQC shunt active filter to reduce source current and load voltage harmonics. While simultaneously, it also improve power quality of 3P3W system under six scenarios due to the integration of three RE sourcesto UPQC-BES system.

3. RESULTS AND ANALYSIS

The analysis of proposed model is investigated through determination of six disturbance scenarios i.e. (1) NL, (2) Unba-NL, (3) Dis-NL, (4) Sag-NL, (5) Swell-NL, and (6) Inter-NL. Each scenario of UPQC uses PI controller and FLC so total number of disturbance are 12 scenarios. By using Matlab/Simulink, the model is then executed according to the desired scenario to obtain curve of source voltage (V_s), load voltage (V_L), compensation voltage (V_c), source current (V_s), load current (I_L), and DC voltage DC link (V_{dc}). Then, THD value of source voltage, source current, load voltage, and load current in each phase as well as average THD value (Avg THD) are obtained base on the curves. THD in each phase is determined in one cycle started at t = 0.35 s. The results of average of source voltage, source current, load voltage, and load current of 3P3Wsystem using UPQC-BES system supplied by three RE sources i.e. PV, wind, and PV-wind hybrid are presented in Table 2, 3, and 4. Next THD in each phase and average THD are showed in Table 5, 6 and 7.

Table 2 shows UPQC-BES system supplied PV connected 3P3W system using PI and FLC, disturbance scenarios 1 to 5 produce an average load voltage above 307 V. While in scenario 6, FLC

produces a higher average load voltage of 304.1 V than if using a PIof 286.7 V. If reviewed from average source current with PI, the highest and lowest average source currents are generated by disturbance scenarios 2 and 4 of 28.15 A and 7,246 A. Whereas if using FLC the highest and lowest average source currents are achieved in scenario 2 and 6 of 28.84 A and 3.804 A.Table 3 shows UPQC-BES supplied by windconnected to 3P3W with PI and FLC, scenarios 1 to 5 is able to obtain a stable load voltage above 308 V. The difference is that in scenario 6, PI generates a load voltage of 274.8 V, otherwise if using FLC, load voltage increases to 306.4 V. If reviewed from source current using PI, the highest and lowest average source currents are resulted by scenarios 2 and 4 of 28.28 A and 7.417 A. Rather, if using FLC, the highest and lowest average source currents are achieved in scenario 2 and 6 of 28.82 A and 3,420 A.Table 4 shows UPQC-BES supplied PV-wind hybrid connected 3P3W using PI and FLC, scenarios 1 to 5 produce an average load voltage above 307 V. While in scenario 6, FLC generates an average load voltage 305.9 V higher than if using PI control of 283.9 V. If reviewed from average source current with PI, the highest and lowest average source currents are resulted by scenarios 2 and 4 of 28.21 A and 6,773 A. Otherwise if using FLC the highest and lowest average source currents are achieved in scenario 2 and 4 of 28.21 A and 6,773 A. Otherwise if using FLC the highest and lowest average source currents are achieved in scenario 2 and 6 of 28.82 A and 3.640 A respectively.

Table 2. Voltage and Current of 3P3W System Using UPQC-BES System Supplied by PV

				0					0 -	•		J	F F			
Con	So	urce Vol	tage V _S ((V)		Load Vo	ltage V _L (V)	Se	ource Cu	rrent I _S (.	A)	1	Load Cu	rent I _L (A	A)
Scii	Ph A	Ph B	Ph C	Avg	Ph A	Ph B	Ph C	Avg	Ph A	Ph B	Ph C	Avg	Ph A	Ph B	Ph C	Avg
							PI	Controlle	er							
1	309.6	309.6	309.6	309.6	307.6	307.8	307.7	307.7	7.766	7.793	7.759	7.773	8.528	8.529	8.533	8.530
2	307.4	308.0	308.0	307.8	308.3	308.7	308.3	308.4	31.00	24.84	28.73	28.15	22.50	34.12	34.52	30.38
3	309.6	309.6	309.6	309.6	313,8	314.3	317.4	317.4	7.897	7.919	7.867	7.895	8.748	8.704	8.785	8.746
4	154.5	154.5	154.5	154.5	307.1	307.3	307.3	307.2	7.235	7.276	7.226	7.246	8.509	8.514	8.510	8.511
5	464.7	464.7	464.7	464.7	308.6	308.7	308.6	308.6	7.979	7.980	7.964	7.975	8.550	8.553	8.554	8.553
6	0.536	1.385	0.850	0.924	310.2	259.8	290.2	286.7	7.392	12.67	6.045	8.703	8.707	7.747	7.637	8.031
							Fuzzy I	Logic Con	troller							
1	309.5	309.5	309.5	309.5	307.7	307.9	307.7	307.8	8.420	8.426	8.416	8.421	8.527	8.532	8.531	8.530
2	307.4	307.9	308.0	307.8	308.5	308.7	308.4	308.5	31.66	25.50	29.36	28.84	22.52	34.11	35.52	30.72
3	309.6	309.5	309.5	309.5	313.4	312.9	315.9	314.1	8.516	8.565	8.496	8.526	8.741	8.677	8.736	8.718
4	154.4	154.4	154.4	154.4	307.3	307.3	307.2	307.3	8.563	8.560	8.561	8.561	8.514	8.517	8.512	8.515
5	464.6	464.6	464.6	464.6	308.6	308.8	308.6	308.7	8.396	8.389	8.389	8.392	8.552	8.556	8.554	8.554
6	0.447	0.392	0.380	0.407	314.0	293.4	304.9	304.1	4.024	3.778	3.608	3.804	8.874	8.195	8.193	8.421

Table 3. Voltage and Current of 3P3W System Using UPQC-BES System Supplied by Wind

C	So	urce Vol	tage Vs (V)	L	oad Volt	age V _L (V	/)	Se	ource Cu	rrent Is (A	A)		Load Curr	ent I _L (A)	
Scn	Ph A	Ph B	Ph C	Avg	Ph A	Ph B	Ph C	Avg	Ph A	Ph B	Ph C	Avg	Ph A	Ph B	Ph C	Avg
								PI Cont	roller							
1	309.5	309.6	309.6	309.6	308.6	308.6	308.2	308.5	7.863	7.875	7.840	7.869	8.554	8.553	8.546	8.551
2	307.4	308.0	308.0	308.0	308.9	309.2	308.7	308.9	31.07	24.97	28.81	28.28	22.55	34.17	34.57	30.43
3	309.6	309.5	309.6	309.6	312.9	312.9	315.4	313.8	7.993	8.015	7.947	7.985	8.817	8.682	8.741	8.747
4	154.5	154.5	154.5	154.5	308.0	308.1	307.8	307.9	7.428	7.455	7.368	7.417	8.527	8.535	8.532	8.531
5	464.7	464.7	464.7	464.7	309.3	309.3	309.0	309.2	8.015	8.020	8.002	8.012	8.564	8.573	8.568	8.568
6	1.256	1.022	0.592	0.957	234.0	316.4	274.0	274.8	11.27	9.866	7.028	9.388	5.958	8.697	8.204	7.619
							Fuz	zy Logic	Controll	er						
1	309.5	309.5	309.5	309.5	308.5	308.6	308.3	308.5	8.418	8.410	8.414	8.414	8.545	8.552	8.549	8.549
2	307.4	307.9	308.0	307.8	309.0	309.3	308.9	309.1	31.64	25.47	29.34	28.82	22.56	34.18	34.59	30.44
3	309.5	309.5	309.5	309.5	313.2	313.7	314.1	313.7	8.519	8.531	8.531	8.527	8.713	8.714	8.718	8.715
4	154.4	154.4	154.4	154.4	308.0	308.1	307.7	307.9	8.557	8.539	8.561	8.552	8.528	8.541	8.525	8.531
5	464.6	464.7	464.7	464.7	309.2	309.3	309.2	309.2	8.391	8.385	8.388	8.388	8.565	8.570	8.567	8.567
6	0.357	0.396	0.397	0.383	303.7	300.0	315.3	306.4	3.358	3.464	3.542	3.420	8.557	8.418	8.731	8.569

Table 4. Voltage and Current of 3P3W System Using UPQC-BES System Supplied PV-Wind Hybrid

			0			-		0	~		2				2	
Son	So	urce Vol	tage V _S (V)	L	oad Volta	ge V _L (V)	Se	ource Cu	rrent I _S (A	A)	Ι	Load Cur	rent I _L (A	.)
Sell	Ph A	Ph B	Ph C	Avg	Ph A	Ph B	Ph C	Avg	Ph A	Ph B	Ph C	Avg	Ph A	Ph B	Ph C	Avg
							PI	Controll	er							
1	309.6	309.6	309.6	309.6	307.8	308.0	307.7	307.8	7.790	7.802	7.770	7.787	8.527	8.537	8.533	8.533
2	307.4	308.0	308.0	307.8	308.4	308.8	308.4	308.6	31.02	24.87	28.74	28.21	22.52	34.13	34.53	31.40
3	309.6	309.5	309.6	309.6	314.0	315.5	316.9	315.5	7.942	7.939	7.918	7.933	8.739	8.750	8.783	8.757
4	154.5	154.5	154.5	154.5	307.3	307.4	307.2	307.3	7.289	7.309	7.251	7.283	8.513	8.516	8.515	8.515
5	464.7	464.7	464.7	464.7	308.7	308.9	308.7	308.8	7.985	7.985	7.975	7.982	8.552	8.558	8.558	8.556
6	1.048	0.825	0.845	0.906	247.5	300.7	303.7	283.9	5.119	5.927	9.271	6.773	7.016	7.893	8.793	7.867
							Fuzzy I	logic Co	ntroller							
1	309.5	309.5	309.5	309.5	307.8	308.0	307.7	307.8	8.419	8.418	8.409	8.413	8.529	8.539	8.533	8.534
2	307.4	307.9	308.0	307.8	308.7	308.7	308.9	308.8	31.66	25.47	29.32	28.82	22.54	34.13	34.56	30.41
3	309.5	309.5	309.5	309.5	314.4	315.5	316.6	315.5	8.581	8.593	8.568	8.581	8.761	8.722	8.761	8.748
4	154.4	154.4	154.4	154.4	307.3	307.5	307.3	307.4	8.566	8.572	8.563	8.567	8.511	8.520	8.519	8.517
5	464.6	464.6	464.6	464.6	308.8	308.8	308.7	308.8	8.391	8.394	8.396	8.394	22.33	22.35	22.36	22.35
6	0.412	0.403	0.402	0.418	311.6	295.7	310.4	305.9	3.774	3.544	3.593	3.640	8.855	8.321	8.288	8.488

Con	Sou	ce Volta	ge THD ((%)	Loa	ad Voltag	ge THD ((%)	Sc	ource Curre	ent THD (9	%)		Load Cu	rrent (%)	
SCII	Ph A	Ph B	Ph C	Avg	Ph A	Ph B	Ph C	Avg	Ph A	Ph B	Ph C	Avg	Ph A	Ph B	Ph C	Avg
								PI Co	ntroller							
1	2.35	2.36	2.32	2.34	2.48	2.50	2.46	2.48	12.89	12.72	12.92	12.84	22.32	22.34	22.32	22.33
2	2.29	2.20	2.24	2.24	2.43	2.23	2.37	2.34	2.660	2.330	2.240	2.410	5.230	2.070	2.660	3.320
3	5.84	5.86	5.94	5.88	6.36	5.90	6.58	6.28	12.75	12.64	13.06	12.82	21.92	22.16	22.33	22.14
4	4.69	4.75	4.81	4.75	2.46	2.48	2.53	2.49	14.26	13.96	14.16	14.13	22.28	22.31	22.28	22.29
5	1.56	1.53	1.55	1.55	2.47	2.43	2.45	2.45	12.51	12.36	12.44	12.44	22.34	22.32	22.32	22.33
6	NA	NA	NA	NA	32.11	15.09	28.54	25.25	270.90	145.89	275.67	230.82	47.70	34.58	36.29	39.53
							F	uzzy Log	ic Controll	er						
1	2.35	2.33	2.35	2.34	2.48	2.46	2.49	2.47	11.83	11.82	11.84	11.83	22.33	22.32	22.33	22.33
2	2.25	2.27	2.20	2.24	2.39	2.41	2.34	2.38	2.620	2.400	2.220	2.413	5.230	2.100	2.640	3.323
3	5.83	5.88	5.93	5.88	6.23	5.93	6.69	6.28	11.83	11.90	12.14	11.96	21.84	22.34	22.53	22.24
4	4.71	4.76	4.79	4.75	2.46	2.48	2.50	2.48	11.91	11.88	11.86	11.89	22.27	22.32	22.32	22.31
5	1.55	1.54	1.54	1.54	2.45	2.44	2.46	2.45	11.90	11.84	11.85	11.86	22.36	22.33	22.35	22.35
6	NA	NA	NA	NA	13.05	6.60	11.15	10.27	30.61	34.72	31.57	32.30	24.25	24.25	24.71	24.40

Table 5. Harmonics of 3P3W System Using UPQC-BESSystem Supplied by PV

Table 6. Harmonics of 3P3W System Using UPQC-BESSystem Supplied by Wind

Son	Sour	ce Volta	ge THD	(%)	Lo	ad Voltag	ge THD ((%)	Se	ource Curr	ent THD (9	%)		Load Cu	rrent (%)	
Sen	Ph A	Ph B	Ph C	Avg	Ph A	Ph B	Ph C	Avg	Ph A	Ph B	Ph C	Avg	Ph A	Ph B	Ph C	Avg
								PI Co	ntroller							
1	1.88	1.87	1.94	1.89	1.99	1.97	2.05	2.00	12.63	12.37	12.70	12.57	12.30	12.30	12.34	12.31
2	1.83	1.76	1.82	1.80	1.92	1.85	1.93	1.90	2.460	2.070	2.200	2.240	5.260	2.070	2.690	3.340
3	5.67	5.71	5.77	5.72	6.00	6.83	6.02	6.28	12.48	12.26	12.66	12.47	22.01	22.12	22.08	22.07
4	3.76	3.86	3.86	1.83	1.97	2.02	2.03	2.01	13.59	13.17	13.51	13.42	22.29	22.31	22.30	22.30
5	1.26	1.24	1.29	1.26	1.99	1.97	2.05	2.00	12.31	12.20	12.31	12.27	22.36	22.33	22.37	22.35
6	NA	NA	NA	NA	14.09	35.59	34.73	28.14	157.76	139.01	266.07	186.95	37.60	34.39	46.97	39.65
							Fι	ızzy Logi	c Controll	er						
1	1.89	1.88	1.93	1.90	1.99	1.98	2.04	2.00	11.71	11.72	11.77	11.73	22.34	22.31	22.32	22.32
2	1.85	1.79	1.78	1.81	1.95	1.87	1.88	1.90	2.43	2.11	2.12	2.220	5.240	2.070	2.700	3.240
3	5.67	5.71	5.78	5.72	5.99	6.39	6.13	6.17	11.72	11.62	11.90	11.75	22.08	21.94	22.47	22.16
4	3.79	3.81	3.86	3.82	1.97	1.99	2.03	1.99	11.72	11.69	11.74	11.72	22.28	22.30	22.35	22.31
5	1.27	1.24	1.28	1.26	2.00	1.96	2.04	2.00	11.66	11.76	11.76	11.73	22.31	22.33	22.35	22.33
6	NA	NA	NA	NA	7.59	6.44	10.95	8.33	27.33	28.27	26.39	27.33	25.39	23.65	24.31	24.45

Table 7. Harmonics of 3P3W System Using UPQC-BES System Supplied by PV-Wind Hybrid

Scn	Source Voltage THD (%)				Load Voltage THD (%)				Source Current THD (%)				Load Current (%)			
	Ph A	Ph B	Ph C	Avg	Ph A	Ph B	Ph C	Avg	Ph A	Ph B	Ph C	Avg	Ph A	Ph B	Ph C	Avg
	PI Controller															
1	2.25	2.19	2.29	2.24	2.37	2.31	2.42	3.37	12.85	12.62	12.74	12.74	22.33	22.31	22.34	22.33
2	2.18	2.08	2.15	2.13	2.30	2.19	2.18	2.22	2.630	2.300	2.290	2.407	5.230	2.070	2.670	3.323
3	5.81	5.82	5.89	5.84	6.12	5.88	6.75	6.25	12.71	12.63	12.98	12.77	22.05	22.13	22.54	22.24
4	4.53	4.48	4.51	4.51	2.37	2.35	2.37	2.36	14.16	13.50	13.99	13.88	22.27	22.30	22.28	22.28
5	1.49	1.46	1.51	1.49	2.37	2.31	2.40	2.36	12.43	12.29	12.41	12.38	22.34	22.32	22.33	22.33
6	NA	NA	NA	NA	18.61	36.38	28.42	27.8	387.71	330.34	189.29	302.45	36.73	38.51	36.83	37.36
Fuzzy Logic Controller																
1	2.25	2.23	2.25	2.24	2.37	2.35	2.39	2.37	11.85	11.74	11.84	11.81	22.32	22.31	22.33	22.32
2	2.23	2.15	2.05	2.14	2.37	2.26	2.17	2.26	2.520	2.410	2.140	2.446	5.230	2.070	2.690	3.330
3	5.80	5.83	5.90	5.84	6.57	5.26	7.06	6.29	11.83	11.78	12.24	11.95	22.15	22.23	22.95	22.44
4	4.53	4.52	4.54	4.86	2.36	2.35	2.35	2.35	11.79	11.74	11.84	11.79	22.29	22.30	22.29	22.29
5	1.48	1.46	1.51	1.48	2.35	2.32	2.40	2.35	11.78	11.81	11.81	11.80	22.33	22.35	22.36	22.35
6	NA	NA	NA	NA	10.30	4.90	10.25	8.48	27.44	29.52	28.63	28.53	23.20	23.97	24.65	23.94

Table 5 shows that average THD of load voltage (V_L) of UPQC-BES system supplied by PV in 3P3W system for scenarios 1 to 5 using PI control is within limits in IEEE 519. The highest and lowest average THD load voltages are achieved under scenario 6 and 2 as 25.25% and 2.34% respectively. PI controller is also able to migitate average THD source voltage in scenario 6 from not accessible (NA) to 25.25% on the load side. The highest and lowest average THD of source current are achieved in scenario 6 and 2 as 230.82% and 2.41%. Table 5 also indicates that average THD of load voltage of UPQC system supplied by PV with BES using FLC in scenarios 1 to 5, has fulfilled limits in IEEE 519. The highest and lowest average THD of load voltage are achieved under scenario 6 and 2 of 10.27% and 2.38%. The use of FLC method is also able to reduce average THD on source voltage in scenario 6 from NA to 10.27% on load side. The highest average THD of source current are achieved in scenario 6 and 2 of 32.30% and 2.413%.

Table 6 shows that average THD of load voltage of UPQC-BES system supplied by wind in 3P3W system for interference scenarios 1 to 5 using PI is within limits prescribed in IEEE 519. The highest and lowest average THD load voltages is achieved under scenario 6 and scenario 2 as 28.14% and 1.90%

respectively. PI controller is also able to reduce average THD source voltage in scenario 6 from NA to 28.14% on the load side. The highest and lowest average THD of source current areachieved in scenario 6 and 2 as 186.95% and 2.24% respectively. Table 6also shows that average THD of load voltage of UPQC-BES supplied by wind using FLC in scenarios 1 to 5, has fulfilled limits prescribed in IEEE 519. The highest and lowest average THD of load voltage are achieved under scenario 6 and 4 of 8.33% and 1.90%. FLC method is also able to reduce average THD on source voltage in scenario 6 from NA to 7.33% on load side. The highest and lowest average THD source current are achieved in scenario 6 and 2 of 27.33% and 2.22%.

Table 7shows that average THD of load voltage (V_L) of UPQC-BES system supplied by PV-wind hybrid in 3P3W system for scenarios 1 to 5 using PI is within limits in IEEE 519. The highest and lowest average THD load voltages are achieved under scenario 6 and 2 as 27.8% and 2.22% respectively. PI is also able to migitate average THD source voltage in scenario 6 from NA to 27.8% on load side. The highest and lowest average THD of source current are achieved in scenario 6and 2 as 302.45% and 2.407% respectively. Table 7 also indicates that average THD of load voltage of UPQC-BES system supplied by PV-wind hybrid using FLC for scenarios 1 to 5, has fulfilled limits in IEEE 519. The highest and lowest average THD of load voltage are achieved under scenario 6 and 2 of 8.48% and 2.26%. FLC method is also able to reduce average THD on source voltage in scenario 6 from NA to 8.48% on load side. The highest and lowest average THD of source current are achieved in scenario 6 and 2 of 28.53% and 2.446%. Overall for UPQC-BES systemsystem supplied by three RE sources in scenarios 1 to 5 using PI and FLC is able to improve average THD of source current better on average THD of load current. Figure 9 presents UPQC-BES system performance supplied by three RE sources using FLC in scenario 6.









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Figure 9.UPQC-BES system performance using FLC in scenario 6 (Inter-NL): (a) UPQC-BES + PV; (b) UPQC-BES + Wind; (c) UPQC-BES + PV-Wind Hybrid(*continue*)

Figure 9.a.(i) shows that in scenario 6, UPQC-BES system supplied by PV at t=0.2 s to t=0.5 s, average source voltage (V_S) falls as 100% to 0.4062 V. During the disturbance, PV is able to generate power to UPQC DC link and injecting full average compensation voltage (V_C) in Figure 9.a.(iii) through injection transformer on series active filter so that average load voltage (V_L) in Figure 9.a.(ii) remains stable at 304.1 V. As long as fault period, although nominal of average source current (I_s) in Figure 9.a.(iv) drops to 3.804 A, combination of PV and BES is able to generate power, store excess energy of PV, and inject current into load through shunt active filter so that average load current (I_L) in Figure 9.a.(v) remains as 8.421 A.Figure 9.b.(i) presents on UPQC-BES supplied by wind at t=0.2 s to t=0.5 s average source voltage (Vs) drops 100% to 0.3828 V. During the disturbance, wind is able to generate power to UPQC DC link and injecting full average compensation voltage (V_C) in Figure 9.b.(iii) through injection transformer on series active filter so that average load voltage (V_L) in Figure 9.b.(ii) remains stable at 306.4 V. During fault period, although nominal of average source current (Is) fallsto 3.420 A, combination of wind and BES is able to generate power, store excess energy of wind, and inject current into load through shunt active filter so that average load current (I₁) in Figure 9.b.(v) remains as 8.569 A.Figure 9.c.(i) indicates on UPQC-BES supplied by PV-Wind Hybrid at t=0.2 s to t=0.5 s average source voltage (V_s) drops 100% to 0.4175 V. During the disturbance, PV-wind hybrid is able to generate power to UPQC DC link and injecting full average

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compensation voltage (V_C) in Figure 9.c.(iii) through injection transformer on series active filter so that average load voltage (V_L) in Figure 9.b.(ii) remains stable at 305.9V. As long as disturbance period, although nominal of average source current (I_S) falls to 3.640 A, combination of PV-wind hybrid and BES is able to generate power, store excess energy of wind, and inject current into load through shunt active filter so that average load current (I_L) in Figure 9.c.(v) remains as 8.488 A.Figure 10 shows spectra of load voltage harmonics on phase A of UPQC-BES system supplied by three RE sources using FLC in scenario 6. Figure 11 shows performance of average THD of load voltage and source current on UPQC-BES system supplied by three RE sources.



Figure 10. Spectra of load voltage harmonics on phase Aof UPQC-BES using FLC in scenario 6 (Inter-NL)



(a) Average load voltage harmonics

(b) Average source current harmonics

Figure 11. Performance of UPQC-BES supplied by threeRE sources using PI and FLC

Figure 11(a) shows that in scenario 1 to 5, the implementation of FLC on UPQC-BES system supplied by three RE sources is able to obtain average THD of load voltage slightly better than PI controller and both method have already met the limit in IEEE 519. Further under scenario 6, FLC applied on UPQC-BES system supplied by three RE sourcesgivessignificantly better result of average THD of load voltage than PI controller. In six disturbance scenarios, both PI controller and FLC applied on UPQC-BES system supplied by three RE sources, PV is ableto obtainthe highest average THD of load voltages.Figure 11(b) shows that in disturbance scenario 1 to 5, implementation of FLC on UPQC-BES system suppliedby three RE sources able to obtain average THD of source current slightly better than PI controller. Furthermore under scenario 6, FLC applied on UPQC-BES system supplied by three RE sources gives significantly better result of average THD of source current than PI controller. Both PI controller and FLC on UPQC-BES system supplied by three RE sources is able to obtain the PI controller. Both PI controller and FLC on UPQC-BES system supplied by three RE sources is six disturbance scenarios, PV is able toobtain the highest average THD of source current.

4. CONCLUSION

Comparative performance analysis of UPQC-BES system supplied by three RE sources i.e. PV, wind, and PV-wind hybrid respectively using PI controller and FLC have been discussed. In disturbance scenario 1 to 5, implementation of FLC on UPQC-BES system supplied by three RE sources able to obtain average THD of load voltage slightly better than PI and both methods have already met the limit in IEEE 519. Under scenario 6, FLC applied on UPQC-BES system supplied by three RE sources givessignificantly better result average THD of load voltage than PI. In six disturbance scenarios, both PI and FLC applied on UPQC-BES system supplied by three RE sources THD of load voltage. In interference scenario 1 to 5, FLC method on UPQC-BES system supplied by three RE sources able to obtain average THD of source current slightly better than PI. Furthermore under scenario 6, FLC applied on UPQC-BES system supplied by three RE sources givessignificantly better result of average THD of source current slightly better than PI. Furthermore under scenario 6, FLC applied on UPQC-BES system supplied by three RE sources givessignificantly better result of average THD of source current slightly better than PI. Furthermore under scenario 6, FLC applied on UPQC-BES system supplied by three RE sources givessignificantly better result of average THD of source current than PI. Both PI and FLC on UPQC-BES system supplied by three RE sources in six scenarios, PV is able to obtain the highest average THD of source current.

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APPENDIX

Three phase grid: RMS voltage 380 volt (L-L), 50 Hz, line impedance: $R_s = 0.1$ Ohm $L_s = 15$ mH; series and shunt active filter: series inductance $L_{se} = 0.015$ mH; shunt inductance $L_{sh} = 15$ mH; injection transformers: rating 10 kVA, 50 Hz, turn ratio (N_1/N_2) = 1:1; non linear load: resistance $R_L = 60$ ohm, inductance $L_L = 0.15$ mH, load impedance $R_c = 0.4$ ohm and $L_c = 15$ mH; unbalance load: resistance $R_1 = 24$ ohm, $R_2 = 12$ ohm, and $R_3 = 6$ ohm, capacitance $C_1, C_2, C_3 = 2200 \ \mu\text{F}$; DC-link: voltage $V_{DC} = 650$ volt and capacitance $C_{DC} = 3000 \ \mu\text{F}$; battery energe storage: type = nickel metal hybrid, DC voltage = 650 volt, rated capacity = 200 Ah, initial SOC = 100%, inductance $L_1 = 6$ mH, capacitance $C_1 = 200 \ \mu\text{F}$; photovoltaic: active power = 0.6 kW temperature = 25° C, irradiance = 1000 W/m²; PMSG wind turbine active power = 0.6 kW, voltage = 380 volt, 50 Hz, wind speed = 5 m/s, picth angle = 2; PI controller: $K_p = 0.2$, $K_i = 1.5$; fuzzy model: method = mamdani, composition = max-min; input membership function: error (V_{dc}) = trapmf, trimf; output membership function: \bar{p}_{loss} = trapmf,trimf.

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Amirullahwas born inSampang East Java Indonesia, in 1977. He received bachelor and master degree in electrical engineering from University of Brawijaya Malang and ITS Surabaya, in 2000 and 2008, respectively. He also worked as a lecturer in University of Bhayangkara Surabaya. He is currently working toward the doctoral degree, in electrical engineering in Power System and Simulation Laboratory (PSSL) ITS Surabaya. His research interest includes power distribution modeling and simulation, power quality, harmonics migitation, design of filter/PFC, and RE.



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Matlab/simulink simulation of unified power quality conditioner-battery energy storage... (Amirullah)

Lampiran 2.5 Revisi ketiga makalah

Matlab/simulink simulation of unified power quality conditioner-battery energy storage system supplied by PV-wind hybrid using fuzzy logic controller

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ABSTRACT

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This paper presents performance analysis of Unified Power Quality Conditioner-Battery Energy Storage (UPQC-BES) system supplied by Photovoltaic (PV)-Wind Hybrid connected to three phase three wire (3P3W) of 380 volt (L-L) and 50 hertz distribution system. The performance of supply system is compared with two renewable energy (RE) sources i.e. PV and Wind, respectively. Fuzzy Logic Controller (FLC) is implemented to maintain DC voltage across the capacitor under disturbance scenarios of source and load as well as to compare the results with Proportional Intergral (PI) controller. There are six scenarios of disturbance i.e. (1) non-linear load (NL), (2) unbalance and nonlinear load (Unba-NL), (3) distortion supply and non-linear load (Dis-NL), (4) sag and non-linear load (Sag-NL), (5) swell and non-linear load (Swell-NL), and (6) interruption and non-linear load (Inter-NL). In disturbance scenario 1 to 5, implementation of FLC on UPQC-BES system supplied by three RE sources is able to obtain average THD of load voltage/source current slightly better than PI. Furthermore under scenario 6, FLC applied on UPQC-BES system supplied by three RE sources gives significantly better result of average THD of load voltage/source current than PI. This research is simulated using Matlab/Simulink.

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1. INTRODUCTION

PV and wind are the most RE distributed generations (DGs) because they are able to convert sunlight and wind into power. PV and solar are the potential DGs sources since it only need sunlight to generate electricity, where the resources are available in abundance, free and relatively clean. Indonesia has enormous energy potential from the sun because it lies on the equator. Almost all areas of Indonesia get sunlight about 10 to 12 hours per day, with an average intensity of irradiation of 4.5 kWh/m² or equivalent to 112.000 GW. The potential of wind energy in Indonesia generally has a speed between 4 to 5 m/s and classified as medium scale with potential capacity of 10 to 100 kW. The weakness of PV and wind turbine besides able to generate power, they also produces a number voltage and current harmonics resulted by presence of several types of PV and wind turbine devices and power converters as well as to increase a number of non-linear loads connected to the grid, so finally resulting in the decrease in power quality.

In order to overcome and improve power quality due to presence of non-linear loads and integration of PV and wind turbine to grid, UPQC is a proposed. UPQC serves to compensate for source voltage quality problemsi.e. sag, swell unbalance, flicker, harmonics, and load current quality problems i.e. harmonics,

unbalance, reactive currents, and neutral current. B. Han et. al and Vinod Khadkikar have investigated UPQC as one part of active power filter consisting of shunt and series active filters connected in parallel and serves as superior controller to overcome a number of power quality problems simultaneously. Series component has been responsible for reducing a number of interference on source side i.e. voltage sag/swell, flicker, unbalanced voltage, and harmonics. Shunt component has been responsible for addressing a current quality problems i.e. low power factor, load current harmonics, and unbalanced load. [1, 2]. UPQC based on RE has been investigated by some researchers. There are two methods used to overcome this problem i.e. using conventional and artificial intelligence. Shafiuzzaman K.K., et.al have proposed system includes a series inverter, shunt inverter, and a DG connected to a DC link through a rectifier using PI. The system was capable of increase source voltage quality i.e. sag and interruption and load current quality, as well as transfer of active power on/off grid mode [3]. The influence of DG on UPQC performance in reducing sag under conditions of some phase to ground faults to using DSTATCOM has been implemented by Norshafinash S., et.al. The DG was effective ough to help UPQC to improve sag [4]. It was connected in series with load resulting better sag million compared to system without DG. Implementation of UPQC using UVTG method with PI to reduce sag, swell, voltage/current harmonics has been doneby S. N. Gohil, et.al. Simulation of voltage distortion was made by adding 5th and 7th harmonics at fundamental source voltage, resulting in a reduction of THD source current and THD load voltage [5].

UPQC supplied by PV panels using boost converter, PI, MPPT P and O, and p-q theory has been proposed by Yahia Bouzelata at.al [6]. The system was capable of compensate reactive power and reduce source current/load voltage harmonics, but did not discuss migitation of sag and interuption caused by PV penetration. Power quality enhancement of sag and source voltage harmonics on grid using UPQC supplied by PV array connected to DC link using PI compared with FLC has been done by Ramalengswara Rao, et.al. Combination of UPQC and PV using FLC can improve source voltage THD better than PI [7]. Amirullah et.al have researched a method for balancing current and line voltage, as a result of DGs of a single phase PV generator unit in randomly installed at homes through on a three phase four wire 220 kV and 50 Hz distribution line using BES and three of single phase bidirectional inverter. Both devices was capable of reduce unbalanced line current/voltage, but both of them were also capable of increase current/voltage harmonics on PCC bus [8]. Power quality migitation of UPQC on microgrid supplied by PV and wind turbine has been implemented by K S Srikanth et. al. It resulted that PI and FLC was able to improve power quality and reduce distortion in output power [9]. The UPQC-wind turbine to provide active power to overcome low sag and interruption voltage to grid has been investigated by H.Toodeji, et.al. The model was used VSC as a rectifier on generator output and controlled so that maximum power desired can be generated by different speed wind turbines using PI [10]. The UPQC-wind turbine connected to UPQC DC link was implemented by M. Hosseinpour, et al. The proposed combination using PI was capable of compensate swell, interruption voltage, and reactive power both on on/off grid [11]. R.Bhavani, et, al have researched on UPOC controlled by FLC to improve power quality in a DFIG wind turbine connected grid. FLC can improve power quality i.e. sag voltage and load current harmonics better than PI [12]. Power quality enhancement on wind turbine and BES with PI connected grid on PCC bus using UPQC has been implemented by S.RajeshRajan, et al. BES was installed to maintain and stabilize active power supply under different wind speed [13].

This research will analyze UPQC-BES performance supplied by PV-wind hybrid connected to 3P3W of 380 volt (L-L) and 50 hertz distribution system. The performance of supply system is compared with two RE sources i.e. PV and Wind, respectively. BES serves to store excess energy produced by three RE sources and distribute it to load if necessary, to prevent interruption voltage, and to adjust charging and discharging of energy in battery. BES is also expected to store excess power produced by three RE combinations and use it as backup power. FLC is proposed and compared with PI to control variable of DC voltage and DC reference voltage input to generate reference current source in current hysteresis controller on shunt active filter. DC voltage controller in shunt active filter and series active filter is used to migitate power quality of load voltage and source current.Performance of two controllers are used to determine load voltage, source current, load voltage THD, and source current THD based on IEEE 519. This paper is presented as follow. Section 2 describes proposed method, model of UPQC-BES system supplied by three RE sources i.e. PV, wind, and PV-wind hybrid, simulation parameters, PV and PMSG wind turbine model, series and shunt active filter, as well as application of PI and FLC method for proposed model. Section 3 shows results and analysis about performance of THD analysis on the proposed model of three RE sources connected to DC link of UPQC-BES system using PI and FLC. In this section, six disturbance scenarios are presented and the results are verified with Matlab/Simulink. Finally, this paper in concluded in Section 4.

2. RESEARCH METHOD

2.1. Proposed method

Figure 1 shows proposed model in this research. The RE sources based DGs used i.e. PV, Wind Turbine, and PV-Wind Turbine Hybrid connected to 3P3W distribution system with 380 volt (L-L) and 50 Hz frequency, through UPQC-BES system. PV array produce power under fixed temperature and radiation as well as connect to UPQC-DC link through a DC/DC boost converter. The maximum power point tracking (MPPT) method with Pertub and Observer (P and O) algorithms helps PV produce maximum power and generate output voltage, as the input voltage for DC/DC boost converter. The converter serves to adjust dutycycle value and output voltage of PV as its input voltage to produce an output voltage corresponding to UPQC DC link voltage. Wind turbine type used is a permanent magnetic synchronous generator (PMSG) with variable speed and fixed voltage which generating power and is connected to UPQC DC link circuit through AC/DC bridge rectifier. The rectifier helps to change AC PSMG stator output voltage to DC voltage through LC circuit that serves to filter and smooth it before connected to UPQC-DC link.BES connected to the UPQC-DC link circuit serves as energy storage and is expected to overcome interruption voltage and overall help UPQC performance to improve voltage and current quality on source and load bus. Simulation parameters proposed in this study is shown in Appendix Section. Power quality analysis is performed on PV, Wind, PV-Wind Hybrid respectively, connected to 3P3W system through UPQC DC-link (on-grid) using BES circuit. Single phase circuit breakers (CBs) are used to connect and disconnect PV, Wind, and Hybrid PV-Wind respectively with UPOC DC-link.

There are six disturbance scenarios i.e. (1) NL, (2) Unba-NL, (3) Dis-NL, (4) Sag-NL, (5) Swell-NL, and (6) Inter-NL. In scenario 1, the model is connected a non-linear load with R_L and L_L of 60 Ohm and 0.15 mH respectively. In scenario 2, the model is connected to non-linear load and during 0.3 s since t=0.2 s to t=0.5 s connected to unbalance three phase load with R1, R2, R3 as 6 Ohm, 12 Ohm, 24 Ohm respectively, and value of C1, C2, C3 as 2200 µF. In scenario 3, the model is connected to non-linear load and source voltage generating 5th and 7th harmonic components with individual harmonic distortion values of 5% and 2% respectively. In scenario 4, the model is connected to non-linear load and source experiences a sag voltage disturbance of 50% for 0.3 s between t=0.2 s to t=0.5 s. In scenario 5, the model is connected to a non-linear load and source experiences a swell voltage disturbance of 50% for 0.3 s between t=0.2 s to t=0.5 s. In scenario 6, the model is connected to non-linear load and source experiences an interruption voltage interference of 100% for 0.3 s between t=0.2 s to t=0.5 s. FLC is used as a DC voltage control in a shunt active filter to improve the power quality of the load voltage and current source and compare it with PI controller. Each disturbance scenario uses a PI controller and FLC so that the total of 12 disturbances. The result analysis of research was carried out i.e. (1) voltage and current on source or poin common coupling (PCC) bus, (2) voltage and current on load bus, (3) harmonic voltage and harmonic current on source bus and (4) harmonic voltage and harmonic current on load bus. The final phase is to compare performance of UPQC-BES system on-grid supplied by PV, Wind, PV-Wind Hybrid respectively using two controllers to improve power quality of load voltage and source current under six disturbance conditions.



Figure 1. Proposed model of UPQC-BES system supplied by PV, Wind, and PV-Wind Hybrid

2.2. Photovoltaic model

Figure 2 shows the equivalent circuit and V-I characteristic of a solar panel. A solar panel is composed of several PV cells that have series, parallel, or series-parallel external connections [14].



Figure 2. Equivalent circuit and V-I characteristic of solar panel

The V-I characteristic of a solar panel is showed in (1):

$$I = I_{PV} - I_o \left[\exp\left(\frac{V + R_s I}{aV_t}\right) - 1 \right] - \frac{V + R_s I}{R_p}$$
(1)

where I_{PV} is the photovoltaic current, I_o is saturated reverse current, 'a' is the ideal diode constant, $V_t = N_S K T q^{-1}$ is the thermal voltage, N_S is the number of series cells, q is the electron charge, K is the Boltzmann constant, T is the temperature of p–n junction, R_S and R_P are series and parallel equivalent resistance of the solar panels. I_{PV} has a linear relation with light intensity and also varies with temperature variations. I_o is dependent on temperature variations. The values of I_{pv} and I_o are calculated as following (2) and (3):

$$I_{PV} = (I_{PV,n} + K_1 \Delta T) \frac{G}{G_n} I$$
⁽²⁾

$$I_o = \frac{I_{SC,n} + K_I \Delta T}{\exp(V_{OC,n} + K_V \Delta T) / aV_I - 1}$$
(3)

In which $I_{PV,n}$, $I_{SC,n}$ and $V_{OC,n}$ are photovoltaic current, short circuit current and open circuit voltage in standard conditions ($T_n=25$ C and $G_n=1000$ Wm⁻²) respectively. K_I is the coefficient of short circuit current to temperature, $\Delta T=T-T_n$ is the temperature deviation from standard temperature, G is the light intensity and K_I is the ratio coefficient of open circuit voltage to temperature. Open circuit voltage, short circuit current and voltage-current corresponding to the maximum power are three important points of I-V characteristic of solar panel. These points are changed by variations of atmospheric conditions. By using (4) and (5) which are derived from PV model equations, short circuit current and open circuit voltage can be calculated in different atmospheric conditions.

$$I_{SC} = (I_{SC} + K_1 \Delta T) \frac{G}{G_n}$$
(4)

$$V_{OC} = V_{OC} + K_V \Delta T \tag{5}$$

2.3. PMSG wind turbine

Wind turbine is **onother** part of an integrated system, which can be divided into two types i.e. fixed and variable speed wind turbines. In fixed speed type, rotating speed of turbine is fixed and hence, frequency of generated voltage remains constant, so it can be directly connected to the network. In this case, maximum power can not always be extracted by wind. On the other hand, on variable speed, turbine can rotate at different speeds, so maximum power can be generated in each wind speed by MPPT method [10]. The advantage of using a PMSG over a synchronous generator and DFIG machine because it has high efficiency and reliability. Due to the elimination of rotor external excitation, machine size, and cost also decreases, making PMSG to be more controlled easily with feedback control system. PMSG has become an attractive solution on wind generation systems with variable speed wind turbine applications [15]. Figure 3 and 4 shows model of PMSG wind turbine and wind turbin power characteristic curve.



Figure 3. Model of PMSG wind turbine



Figure 4. Wind turbin power characteristic curve

The output power of wind turbine can be expressed using (6), (7), and (8) [11].

$$\lambda = \frac{\omega_r R}{V_{wind}} \tag{6}$$

$$P_M = \frac{1}{2} \rho \pi R^2 C_p V_{wind}^3 \tag{7}$$

$$T_{M} = \frac{P_{M}}{\omega_{r}} = \frac{1}{2} \rho \pi R^{5} C_{p} \frac{\omega_{M}^{3}}{\lambda^{3}}$$

$$\tag{8}$$

Where λ is the speed-tip ratio, V_{wind} is wind speed, R is blade radius, ω_r is rotor speed (rad/sec), ρ is the air density, C_P is the power coefficient, P_M is the output mechanical power, and T_M is output torque of wind turbine. The C_P coefficient is dependent on the pitch angle value, at which rotor blade can rotate along axis and tip-speed ratio λ expressed in (9).

$$C_{p} = (0.44 - 0.167\beta)\sin\frac{\pi(\lambda - 2)}{(13 - 0.3\beta)}$$
(9)

Where β is a pitch angle blade. In a fixed pitch type, the value of β is set to a fixed value.

2.4. Control of series active filter

The main function of series active filter is as a sensitive load protection against a number of voltage interference at PCC bus. The control strategy algorithm of the source and load voltage in series active filter circuit is shown in Figure 5. It extracts the unit vector templates from the distorted input supply. Furthermore, the templates are expected to be ideal sinusoidal signal with unity amplitude. The ported supply voltages are measured and divided by peak amplitude of fundamental input voltage V_m gives V_m (10) [6].

$$V_m = \sqrt{\frac{2}{3}} \left(V_{sa}^2 + V_{sb}^2 + V_{sc}^2 \right) \tag{10}$$

A three phase locked loop (PLL) is used in order to generate a sinusoidal unit vector templates with a phase lagging by the use of sinus function. The reference load voltage signal is determined by multiplying the unit vector templates with the peak amplitude of the fundamental input voltage V_m . The load reference voltage (V_{La}^* , V_{Lb}^* , V_c^*) is then compared against to sensed load voltage (V_{La} , V_{Lb} , V_{Lc}) by a pulse width modulation (PWM) controller used to generate the desired trigger signal on series active filter.



Figure 5. Control strategy of series active filter

2.5. Control of shunt active filter

The main function of shunt active filter is migration of power quality problems on the load side. The control methodology in shunt active filter is that the absorbed current from the PCC bus is a balanced positive sequence current including unbalanced sag voltage conditions in the PCC bus or unbalanced conditions or non-linear loads. In order to obtain satisfactory compensation caesed by disturbance due to non-linear load, many algorithms have been used in the literature. This research used instantaneous reactive power theory method "p-q theory". The voltages and currents in Cartesian *abcoordinates* can be transformed to Cartesian $\alpha\beta$ coordinates as expressed in (11) and (12) [16].

$$\begin{bmatrix} v_{\alpha} \\ v_{\beta} \end{bmatrix} = \begin{bmatrix} 1 & -1/2 & -1/2 \\ 1 & \sqrt{3}/2 & -\sqrt{3}/2 \end{bmatrix} \begin{bmatrix} V_{a} \\ V_{b} \\ V_{c} \end{bmatrix}$$
(11)

$$\begin{bmatrix} i_{\alpha} \\ i_{\beta} \end{bmatrix} = \begin{bmatrix} 1 & -1/2 & -1/2 \\ 1 & \sqrt{3}/2 & -\sqrt{3}/2 \end{bmatrix} \begin{bmatrix} i_{La} \\ i_{Lb} \\ i_{Lc} \end{bmatrix}$$
(12)

The computation of the real power (p) and imaginary power (q) is showed in (13). The real power and imaginary are measured instantaneously power and in matrix it is form is given as. The presence of oscillating and average components in instantaneous power is presented in (14) [17].

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$$\begin{bmatrix} p \\ q \end{bmatrix} = \begin{bmatrix} v_{\alpha} & v_{\beta} \\ -v_{\beta} & v_{\alpha} \end{bmatrix} \begin{bmatrix} i_{\alpha} \\ i_{\beta} \end{bmatrix}$$
(13)

$$p = \overline{p} + \widetilde{p} \quad ; q = \overline{q} + \widetilde{q} \tag{14}$$

Where \bar{p} = direct component of real power, \tilde{p} = fluctuating component of real power, \bar{q} = direct component of imaginary power, \tilde{q} = fluctuating component of imaginary power. The total imaginary power (q) and the fluctuating component of real power are selected as power references and current references and are utilized through the use of (15) for compensating harmonic and reactive power [18].

$$\begin{bmatrix} i_{c\alpha}^{*} \\ i_{c\beta}^{*} \end{bmatrix} = \frac{1}{v_{\alpha}^{2} + v_{\beta}^{2}} \begin{bmatrix} v_{\alpha} & v_{\beta} \\ v_{\beta} & -v_{\alpha} \end{bmatrix} \begin{bmatrix} -\widetilde{p} + \overline{p}_{loss} \\ -q \end{bmatrix}$$
(15)

The signal \overline{p}_{loss} , is obtained from voltage regulator and is utilized as average real power. It can also be specified as the instantaneous active power which corresponds to the resistive loss and switching loss of the UPQC. The error obtained on comparing the actual DC-link capacitor voltage with the reference value is processed in FLC, engaged by voltage control loop as it minimizes the steady state error of the voltage across the DC link to zero. The compensating currents $(i_{c\alpha}^*, i_{c\beta}^*)$ as required to meet the power mand of load are shown in (15). These currents are represented in α - β coordinates. The phase current required to acquire using (16) for compensation. These source phase currents $(i_{s\alpha}^*, i_{sb}^*, i_{sc}^*)$ are represented in a-b-c axis obtained from the compensating current in the α - β coordinates presented in (16) [18]. Figure 6 shows a control of shunt active filter.

$$\begin{bmatrix} i_{s_{\alpha}}^{*} \\ i_{s_{b}}^{*} \\ i_{s_{c}}^{*} \end{bmatrix} = \sqrt{\frac{2}{3}} \begin{bmatrix} 1 & 0 \\ -1/2 & \sqrt{3}/2 \\ -1/2 & -\sqrt{3}/2 \end{bmatrix} \begin{bmatrix} i_{c\alpha}^{*} \\ i_{c\beta}^{*} \end{bmatrix}$$
(16)



Figure 6. Control strategy of shunt active filter

The proposed model of UPQC-BES system supplied by three RE sources is shown in Figure 1. From the figure, we can see that PV is connected to the DC link through OC-DC boost converter circuit. The PV partially distributes power to the load and the remains istransfered to three phase grid. The load consists of non linear and unbalanced load. The non-linear load is a diode rectifier circuit with the RL bod type, while the unbalanced load is a three phase RC load with different R value on each phase. The economically efficient, PV must always work in MPP condition. In this research, MPPT method used is P and O algorithm. The model is also applied for UPQC-BES system which is supplied by wind and PV-wind hybrid respectively. In order to operate properly, UPQC-BES system device must have a minimum DC link voltage (V_{dc}). The value of common DC link voltage depends on the nstantaneous energy avialable to UPQC is defined by in (17) [16]:

$$V_{dc} = \frac{2\sqrt{2}V_{LL}}{\sqrt{3}m} \tag{17}$$

where m is modu index and V_{LL} is the AC grid line voltage of UPQC. Considering that modulation index as 1 and forline to line grid voltage (V_{LL} =380 volt), the V_{dc} is obtained 620, 54 volt and selected as 650 volt.

The input of shunt active filter showed in Figure 5 is DC voltage (V_{dc}) and reference DC voltage (V_{dc}^*), while the output is \bar{p}_{loss} by using PI controller. Then, the \bar{p}_{loss} is as one of input variable to generate the reference source current (I_{sa}^* , I_{sb}^* , and I_{sc}^*). The reference source current output is then compared to source current (I_{sa} , I_{sb} , and I_{sc}) by the current hysteresis control to generate trigger signal in IGBT circuit of shunt active filter. In this research, FLC as DC voltage control algorithm on shunt active filter is proposed and compared with PI controller. The FLC is capable of reduce oscilation and generate quick convergence calculation during disturbances. This method is also used to overcome the weakness of PI controller in determining proportional gain (K_p) and integral gain constant (K_i) which still use trial and error method.

2.6. Fuzzy logic controller

The research is started by determine \overline{p}_{loss} as the input variable to result the reference source current on current hysteresis controller to generate trigger signal on the IGBT shunt active filter of UPQC using PI controller (K_p=0.2 and K_i=1.5). By using the same procedure, \overline{p}_{loss} is also determined by using FLC. The FLC has been widely used in recent industrial processes because it has heuristic, simpler, more effective and has multi-rule based variables in both linear and non-linear system variations. The main components of FLC are fuzzification, decision making (rulebase, database, reason mechanism) and defuzzification in Figure 7. The output membership function is generated using inference blocks and the basic rules of FLC as shown in Table 1.



The fuzzy rule algorithm collects a number of fuzzy control rules in a particular order. This rule is used to control the system to meet the desired performance requirements and they are designed from a number of intelligent system control knowledge. The fuzzy inference of FLC using Mamdani method related to max-min composition. The fuzzy inference system in FLC consists of three parts: rule base, database, and reasoning mechanism [19]. The FLC method is performed by determining input variables V_{dc} (V_{dc-error}) and delta Vdc ($\Delta V_{dc-error}$), seven linguistic fuzzy sets, operation fuzzy block system (fuzzyfication, fuzzy rule base and defuzzification), $V_{dc-error}$ and $\Delta V_{dc-error}$ during fuzzification process, fuzzy rule base table, crisp value to determine \bar{p}_{loss} in defuzzification phase. The \bar{p}_{loss} is one of input variable to obtain compensating currents $(i_{ca}^*, i_{c\beta}^*)$ in (16). During fuzzification process, a number of input variables are calculated and converted into linguistic variables based on a subset called membership function. The error Vdc (V_{dc-error}) and delta error Vdc ($\Delta V_{dc-error}$) are proposed input variable system and output variable is \overline{p}_{loss} . To translate these variables, each input and output variable is designed using seven membership functions: Negative Big (NB), Negative Medium (NM), Negative Small (NS), Zero (Z), Positive Small (PS), Positive Medium (PM) and Positive Big (PB). The membership functions of crisp input and output are presented with triangular and trapezoidal membership functions. The value of V_{dc-error} range from -650 to 650, $\Delta V_{dc-error}$ from -650 to 650, and \bar{p}_{lass} from -100 to 100. The input and output MFs are shown in Figure 8.


Figure 8. Membership functions (a) $V_{dc-error}$, (b) $\Delta V_{dc-error}$, and (c) \overline{p}_{lass}

After the V_{dc-error} and Δ V_{dc-error} are obtained, then two input membership functions are converted to linguistic variables and uses them as input functions for FLC. The output membership function is generated using inference blocks and the basic rules of FLC as shown in Table 1. Finally the defuzzification block operates to convert generated \bar{p}_{loss} output from linguistic to numerical variable again. Then it becomes input variable for current hysteresis controller to produce trigger signal on the IGBT circuit of UPQC shunt active filter to reduce source current and load voltage harmonics. While simultaneously, it also improve power quality of 3P3W system under six scenarios due to the integration of three RE sources to UPQC-BES system.

3. RESULTS AND ANALYSIS

The analysis of proposed model is investigated through determination of six disturbance scenarios i.e. (1) NL, (2) Unba-NL, (3) Dis-NL, (4) Sag-NL, (5) Swell-NL, and (6) Inter-NL. Each scenario of UPQC uses PI controller and FLC so total number of disturbance are 12 scenarios.By using Matlab/Simulink, the model is then executed according to the desired scenario to obtain curve of source voltage (V_s), load voltage (V_L), compensation voltage (V_c), source current (V_s), load current (I_L), and DC voltage DC link (V_{dc}). Then, THD value of source voltage, source current, load voltage, and load current in each phase as well as average THD value (Avg THD) are obtained base on the curves. THD in each phase is determined in one cycle started at t = 0.35 s. The results of average of source voltage, source current, load voltage, source current of 3P3W system using UPQC-BES system supplied by three RE sources i.e. PV, wind, and PV-wind hybrid are presented in Table 2, 3, and 4. Next THD in each phase and average THD are showed in Table 5, 6 and 7.

Table 2 shows UPQC-BES system supplied PV connected 3P3W system using PI and FLC, disturbance scenarios 1 to 5 produce an average load voltage above 307 V. While in scenario 6, FLC produces a higher average load voltage of 304.1 V than if using a PIof 286.7 V. If reviewed from average source current with PI, the highest and lowest average source currents are generated by disturbance scenarios

2 and 4 of 28.15 A and 7,246 A. Whereas if using FLC the highest and lowest average source currents are achieved in scenario 2 and 6 of 28.84 A and 3.804 A. Table 3 shows UPQC-BES supplied by windermetted to 3P3W with PI and FLC, scenarios 1 to 5 is able to obtain a stable load voltage above 308 V. The difference is that in scenario 6, PI generates a load voltage of 274.8 V, otherwise if using FLC, load voltage increases to 306.4 V. If reviewed from the urrent using PI, the highest and lowest average source currents are resulted by scenarios 2 and 4 of 28.28 A and 7.417 A. Rather, if using FLC, the highest and lowest average source currents are achieved in scenario 2 and 6 of 28.82 A and 3,420 A. Table 4 shows UPQC-BES supplied PV-wind hybrid connected 3P3W using PI and FLC, scenarios 1 to 5 produce an average load voltage above 307 V. While in scenario 6, FLC generates an average load voltage 305.9 V higher than if using PI control of 283.9 V. If reviewed from average source current with PI, the highest and lowest average source currents are resulted by scenarios 2 and 4 of 28.21 A and 6,773 A. Otherwise if using FLC the highest and lowest average source currents are achieved in scenario 2 and 6 of 28.82 A and 3.640 A respectively.

Table 2. Voltage and Current of 3P3W System Using UPQC-BES System Supplied by PV

Con	So	urce Vol	tage V _S ((V)		Load Vo	ltage V _L (V)	Se	ource Cu	rrent I _S (.	A)	I	Load Cu	rent I _L (A	<i>I</i>)
Self	Ph A	Ph B	Ph C	Avg	Ph A	Ph B	Ph C	Avg	Ph A	Ph B	Ph C	Avg	Ph A	Ph B	Ph C	Avg
							PI	Controlle	er							
1	309.6	309.6	309.6	309.6	307.6	307.8	307.7	307.7	7.766	7.793	7.759	7.773	8.528	8.529	8.533	8.530
2	307.4	308.0	308.0	307.8	308.3	308.7	308.3	308.4	31.00	24.84	28.73	28.15	22.50	34.12	34.52	30.38
3	309.6	309.6	309.6	309.6	313,8	314.3	317.4	317.4	7.897	7.919	7.867	7.895	8.748	8.704	8.785	8.746
4	154.5	154.5	154.5	154.5	307.1	307.3	307.3	307.2	7.235	7.276	7.226	7.246	8.509	8.514	8.510	8.511
5	464.7	464.7	464.7	464.7	308.6	308.7	308.6	308.6	7.979	7.980	7.964	7.975	8.550	8.553	8.554	8.553
6	0.536	1.385	0.850	0.924	310.2	259.8	290.2	286.7	7.392	12.67	6.045	8.703	8.707	7.747	7.637	8.031
							Fuzzy l	Logic Cor	ıtroller							
1	309.5	309.5	309.5	309.5	307.7	307.9	307.7	307.8	8.420	8.426	8.416	8.421	8.527	8.532	8.531	8.530
2	307.4	307.9	308.0	307.8	308.5	308.7	308.4	308.5	31.66	25.50	29.36	28.84	22.52	34.11	35.52	30.72
3	309.6	309.5	309.5	309.5	313.4	312.9	315.9	314.1	8.516	8.565	8.496	8.526	8.741	8.677	8.736	8.718
4	154.4	154.4	154.4	154.4	307.3	307.3	307.2	307.3	8.563	8.560	8.561	8.561	8.514	8.517	8.512	8.515
5	464.6	464.6	464.6	464.6	308.6	308.8	308.6	308.7	8.396	8.389	8.389	8.392	8.552	8.556	8.554	8.554
6	0.447	0.392	0.380	0.407	314.0	293.4	304.9	304.1	4.024	3.778	3.608	3.804	8.874	8.195	8.193	8.421

Table 3. Voltage and Current of 3P3W System Using UPQC-BES System Supplied by Wind

C	So	urce Vol	tage Vs (V)	L	oad Volt	age V _L (V	V)	Se	ource Cu	rrent Is (A	A)		Load Curr	ent I _L (A)	
SCII	Ph A	Ph B	Ph C	Avg	Ph A	Ph B	Ph C	Avg	Ph A	Ph B	Ph C	Avg	Ph A	Ph B	Ph C	Avg
								PI Cont	roller							
1	309.5	309.6	309.6	309.6	308.6	308.6	308.2	308.5	7.863	7.875	7.840	7.869	8.554	8.553	8.546	8.551
2	307.4	308.0	308.0	308.0	308.9	309.2	308.7	308.9	31.07	24.97	28.81	28.28	22.55	34.17	34.57	30.43
3	309.6	309.5	309.6	309.6	312.9	312.9	315.4	313.8	7.993	8.015	7.947	7.985	8.817	8.682	8.741	8.747
4	154.5	154.5	154.5	154.5	308.0	308.1	307.8	307.9	7.428	7.455	7.368	7.417	8.527	8.535	8.532	8.531
5	464.7	464.7	464.7	464.7	309.3	309.3	309.0	309.2	8.015	8.020	8.002	8.012	8.564	8.573	8.568	8.568
6	1.256	1.022	0.592	0.957	234.0	316.4	274.0	274.8	11.27	9.866	7.028	9.388	5.958	8.697	8.204	7.619
							Fuz	zy Logic	Controll	er						
1	309.5	309.5	309.5	309.5	308.5	308.6	308.3	308.5	8.418	8.410	8.414	8.414	8.545	8.552	8.549	8.549
2	307.4	307.9	308.0	307.8	309.0	309.3	308.9	309.1	31.64	25.47	29.34	28.82	22.56	34.18	34.59	30.44
3	309.5	309.5	309.5	309.5	313.2	313.7	314.1	313.7	8.519	8.531	8.531	8.527	8.713	8.714	8.718	8.715
4	154.4	154.4	154.4	154.4	308.0	308.1	307.7	307.9	8.557	8.539	8.561	8.552	8.528	8.541	8.525	8.531
5	464.6	464.7	464.7	464.7	309.2	309.3	309.2	309.2	8.391	8.385	8.388	8.388	8.565	8.570	8.567	8.567
6	0.357	0.396	0.397	0.383	303.7	300.0	315.3	306.4	3.358	3.464	3.542	3.420	8.557	8.418	8.731	8.569

Table 4. Voltage and Current of 3P3W System Using UPQC-BES System Supplied PV-Wind Hybrid

Son	So	purce Voltage $V_S(V)$ Load Voltage $V_L(V)$ Source Current $I_S(A)$ Load Current						rent I _L (A	.)							
Self	Ph A	Ph B	Ph C	Avg	Ph A	Ph B	Ph C	Avg	Ph A	Ph B	Ph C	Avg	Ph A	Ph B	Ph C	Avg
							PI	Controll	er							
1	309.6	309.6	309.6	309.6	307.8	308.0	307.7	307.8	7.790	7.802	7.770	7.787	8.527	8.537	8.533	8.533
2	307.4	308.0	308.0	307.8	308.4	308.8	308.4	308.6	31.02	24.87	28.74	28.21	22.52	34.13	34.53	31.40
3	309.6	309.5	309.6	309.6	314.0	315.5	316.9	315.5	7.942	7.939	7.918	7.933	8.739	8.750	8.783	8.757
4	154.5	154.5	154.5	154.5	307.3	307.4	307.2	307.3	7.289	7.309	7.251	7.283	8.513	8.516	8.515	8.515
5	464.7	464.7	464.7	464.7	308.7	308.9	308.7	308.8	7.985	7.985	7.975	7.982	8.552	8.558	8.558	8.556
6	1.048	0.825	0.845	0.906	247.5	300.7	303.7	283.9	5.119	5.927	9.271	6.773	7.016	7.893	8.793	7.867
							Fuzzy I	ogic Co	ntroller							
1	309.5	309.5	309.5	309.5	307.8	308.0	307.7	307.8	8.419	8.418	8.409	8.413	8.529	8.539	8.533	8.534
2	307.4	307.9	308.0	307.8	308.7	308.7	308.9	308.8	31.66	25.47	29.32	28.82	22.54	34.13	34.56	30.41
3	309.5	309.5	309.5	309.5	314.4	315.5	316.6	315.5	8.581	8.593	8.568	8.581	8.761	8.722	8.761	8.748
4	154.4	154.4	154.4	154.4	307.3	307.5	307.3	307.4	8.566	8.572	8.563	8.567	8.511	8.520	8.519	8.517
5	464.6	464.6	464.6	464.6	308.8	308.8	308.7	308.8	8.391	8.394	8.396	8.394	22.33	22.35	22.36	22.35
6	0.412	0.403	0.402	0.418	311.6	295.7	310.4	305.9	3.774	3.544	3.593	3.640	8.855	8.321	8.288	8.488

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		Ta	ble 5.	Harm	onics	of 3P3	W Sys	stem U	sing UF	QC-BE	ES Syste	em Supp	olied b	y PV		
C	Sou	rce Volta	ge THD ((%)	Lo	ad Voltag	ge THD ((%)	Se	ource Curr	ent THD (%)		Load Cu	rrent (%)	
Scii	Ph A	Ph B	Ph C	Avg	Ph A	Ph B	Ph C	Avg	Ph A	Ph B	Ph C	Avg	Ph A	Ph B	Ph C	Avg
								PI Co	ntroller							
1	2.35	2.36	2.32	2.34	2.48	2.50	2.46	2.48	12.89	12.72	12.92	12.84	22.32	22.34	22.32	22.33
2	2.29	2.20	2.24	2.24	2.43	2.23	2.37	2.34	2.660	2.330	2.240	2.410	5.230	2.070	2.660	3.320
3	5.84	5.86	5.94	5.88	6.36	5.90	6.58	6.28	12.75	12.64	13.06	12.82	21.92	22.16	22.33	22.14
4	4.69	4.75	4.81	4.75	2.46	2.48	2.53	2.49	14.26	13.96	14.16	14.13	22.28	22.31	22.28	22.29
5	1.56	1.53	1.55	1.55	2.47	2.43	2.45	2.45	12.51	12.36	12.44	12.44	22.34	22.32	22.32	22.33
6	NA	NA	NA	NA	32.11	15.09	28.54	25.25	270.90	145.89	275.67	230.82	47.70	34.58	36.29	39.53
							F	uzzy Log	ic Controll	ler						
1	2.35	2.33	2.35	2.34	2.48	2.46	2.49	2.47	11.83	11.82	11.84	11.83	22.33	22.32	22.33	22.33
2	2.25	2.27	2.20	2.24	2.39	2.41	2.34	2.38	2.620	2.400	2.220	2.413	5.230	2.100	2.640	3.323
3	5.83	5.88	5.93	5.88	6.23	5.93	6.69	6.28	11.83	11.90	12.14	11.96	21.84	22.34	22.53	22.24
4	4.71	4.76	4.79	4.75	2.46	2.48	2.50	2.48	11.91	11.88	11.86	11.89	22.27	22.32	22.32	22.31
5	1.55	1.54	1.54	1.54	2.45	2.44	2.46	2.45	11.90	11.84	11.85	11.86	22.36	22.33	22.35	22.35
6	NA	NA	NA	NA	13.05	6.60	11.15	10.27	30.61	34.72	31.57	32.30	24.25	24.25	24.71	24.40

Table 6. Harmonics of 3P3W System Using UPQC-BES System Supplied by Wind

Con	Sour	ce Volta	ge THD	(%)	Lo	ad Voltag	ge THD ((%)	Sc	ource Curr	ent THD (9	%)		Load Cu	rrent (%)	
SCII	Ph A	Ph B	Ph C	Avg	Ph A	Ph B	Ph C	Avg	Ph A	Ph B	Ph C	Avg	Ph A	Ph B	Ph C	Avg
								PI Co	ntroller							
1	1.88	1.87	1.94	1.89	1.99	1.97	2.05	2.00	12.63	12.37	12.70	12.57	12.30	12.30	12.34	12.31
2	1.83	1.76	1.82	1.80	1.92	1.85	1.93	1.90	2.460	2.070	2.200	2.240	5.260	2.070	2.690	3.340
3	5.67	5.71	5.77	5.72	6.00	6.83	6.02	6.28	12.48	12.26	12.66	12.47	22.01	22.12	22.08	22.07
4	3.76	3.86	3.86	1.83	1.97	2.02	2.03	2.01	13.59	13.17	13.51	13.42	22.29	22.31	22.30	22.30
5	1.26	1.24	1.29	1.26	1.99	1.97	2.05	2.00	12.31	12.20	12.31	12.27	22.36	22.33	22.37	22.35
6	NA	NA	NA	NA	14.09	35.59	34.73	28.14	157.76	139.01	266.07	186.95	37.60	34.39	46.97	39.65
							Fι	ızzy Logi	c Controll	er						
1	1.89	1.88	1.93	1.90	1.99	1.98	2.04	2.00	11.71	11.72	11.77	11.73	22.34	22.31	22.32	22.32
2	1.85	1.79	1.78	1.81	1.95	1.87	1.88	1.90	2.43	2.11	2.12	2.220	5.240	2.070	2.700	3.240
3	5.67	5.71	5.78	5.72	5.99	6.39	6.13	6.17	11.72	11.62	11.90	11.75	22.08	21.94	22.47	22.16
4	3.79	3.81	3.86	3.82	1.97	1.99	2.03	1.99	11.72	11.69	11.74	11.72	22.28	22.30	22.35	22.31
5	1.27	1.24	1.28	1.26	2.00	1.96	2.04	2.00	11.66	11.76	11.76	11.73	22.31	22.33	22.35	22.33
6	NA	NA	NA	NA	7.59	6.44	10.95	8.33	27.33	28.27	26.39	27.33	25.39	23.65	24.31	24.45

Table 7. Harmonics of 3P3W System Using UPQC-BES System Supplied by PV-Wind Hybrid

								-	-		-					
Son	Sour	rce Voltag	ge THD	(%)	Loa	d Voltag	e THD (9	%)	Sc	ource Curre	ent THD (%)		Load Cu	rrent (%)	
Self	Ph A	Ph B	Ph C	Avg	Ph A	Ph B	Ph C	Avg	Ph A	Ph B	Ph C	Avg	Ph A	Ph B	Ph C	Avg
								PI Co	ntroller							
1	2.25	2.19	2.29	2.24	2.37	2.31	2.42	3.37	12.85	12.62	12.74	12.74	22.33	22.31	22.34	22.33
2	2.18	2.08	2.15	2.13	2.30	2.19	2.18	2.22	2.630	2.300	2.290	2.407	5.230	2.070	2.670	3.323
3	5.81	5.82	5.89	5.84	6.12	5.88	6.75	6.25	12.71	12.63	12.98	12.77	22.05	22.13	22.54	22.24
4	4.53	4.48	4.51	4.51	2.37	2.35	2.37	2.36	14.16	13.50	13.99	13.88	22.27	22.30	22.28	22.28
5	1.49	1.46	1.51	1.49	2.37	2.31	2.40	2.36	12.43	12.29	12.41	12.38	22.34	22.32	22.33	22.33
6	NA	NA	NA	NA	18.61	36.38	28.42	27.8	387.71	330.34	189.29	302.45	36.73	38.51	36.83	37.36
							Fuz	zy Log	ic Control	ler						
1	2.25	2.23	2.25	2.24	2.37	2.35	2.39	2.37	11.85	11.74	11.84	11.81	22.32	22.31	22.33	22.32
2	2.23	2.15	2.05	2.14	2.37	2.26	2.17	2.26	2.520	2.410	2.140	2.446	5.230	2.070	2.690	3.330
3	5.80	5.83	5.90	5.84	6.57	5.26	7.06	6.29	11.83	11.78	12.24	11.95	22.15	22.23	22.95	22.44
4	4.53	4.52	4.54	4.86	2.36	2.35	2.35	2.35	11.79	11.74	11.84	11.79	22.29	22.30	22.29	22.29
5	1.48	1.46	1.51	1.48	2.35	2.32	2.40	2.35	11.78	11.81	11.81	11.80	22.33	22.35	22.36	22.35
6	NA	NA	NA	NA	10.30	4.90	10.25	8.48	27.44	29.52	28.63	28.53	23.20	23.97	24.65	23.94

Table 5 shows that average THD of load voltage (V_L) of UPQC-BES system supplied by PV in 3P3W system for scenarios 1 to 5 using PI control is within limits in IEEE 519. The highest and lowest average THD load voltages are bieved under scenario 6 and 2 as 25.25% and 2.34% respectively. PI controller is also able to migitate average THD source voltage in scenario 6 from not accessible (NA) to 25.25% on the load side. The highest and lowest average THD of source current are achieved in scenario 6 and 2 as 230.82% and 2.41%. Table 5 also indicates that average THD of load voltage of UPQC system supplied by PV with BES using FLC in scenarios 1 to 5, has fulfilled limits in IEEE 519. The highest and lowest average THD of load voltage are achieved under scenario 6 and 2 of 10.27% and 2.38%. The use of FLC method is also able to reduce average THD on source voltage in scenario 6 from NA to 10.27% on load side. The highest average THD of source current are achieved in scenario 6 and 2 of 32.30% and 2.413%.

Table 6 shows that average THD of load voltage of UPQC-BES system supplied by wind in 3P3W system for interference scenarios 1 to 5 using PI is within limits prescribed in IEEE 519. The highest and lowest average THD load voltages is achieved under scenario 6 and scenario 2 as 28.14% and 1.90% respectively. PI controller is also able to reduce average THD source voltage in scenario 6 from NA to 28.14% on the load side. The highest and lowest average THD of source current areachieved in scenario 6 and 2 as 186.95% and 2.24% respectively. Table 6 also shows that average THD of load voltage of UPQC-BES supplied by wind using FLC in scenarios 1 to 5, has fulfilled limits prescribed in IEEE 519. The highest and lowest average THD of load voltage are achieved under scenario 6 and 4of 8.33% and 1.90%. FLC method is also able to reduce average THD on source voltage in scenario 6 from NA to 7.33% on load side. The highest and lowest average THD source current are achieved in scenario 6 and 2 of 27.33% and 2.22%.

Table 7 shows that average THD of load voltage (V_L) of UPQC-BES system supplied by PV-wind hybrid in 3P2W system for scenarios 1 to 5 using PI is within limits in IEEE 519. The highest and lowest average THE d voltages are achieved under scenario 6 and 2 as 27.8% and 2.22% respectively. PI is also able to migitate average THD source voltage in scenario 6 from NA to 27.8% on load side. The highest and lowest average THD of source current are achieved in scenario 6 and 2 as 302.45% and 2.407% respectively. Table 7 also indicates that average THD of load voltage of UPQC-BES system supplied by PV-wind hybrid using FLC for scenarios 1 to 5, has fulfilled limits in IEEE 519. The highest and lowest average THD of load voltage are achieved under scenario 6 and 2 of 8.48% and 2.26%. FLC method is also able to reduce average THD on source voltage in scenario 6 from NA to 8.48% on load side. The highest and lowest average THD of source current are achieved in scenario 5 and 2 of 28.53% and 2.446%. Overall for UPQC-BES systemsystem supplied by three RE sources in scenarios 1 to 5 using PI and FLC is able to improve average THD of load current. Figure 9 presents UPQC-BES system performance supplied by three RE sources using FLC in scenario 6.

Figure 9 a(i) shows that in scenario 6, UPQC-BES system supplied by PV at t=0.2 s to t=0.5 s, average source voltage (V_8) falls as 100% to 0.4062 V. During the disturbance, PV is able to generate power to UPQC DC link and injecting full average compensation voltage (V_c) in Figure 9 a(iii) through injection transformer on series active filter so that average load voltage (VL) in Figure 9 a(ii) remains stable at 304.1 V. As long as fault period, although nominal of average source current (I_s) in Figure 9 a(iv) drops to 3.804 A, combination of PV and BES is able to generate power, store excess energy of PV, and inject current into load through shunt active filter so that average load current (IL) in Figure 9 a(v) remains as 8.421 A. Figure 9 b(i) presents on UPQC-BES supplied by wind at t=0.2 s to t=0.5 s average source voltage (Vs) drops 100% to 0.3828 V. During the disturbance, wind is able to generate power to UPQC DC link and injecting full average compensation voltage (V_C) in Figure 9 b(iii) through injection transformer on series active filter so that average load voltage (V_L) in Figure 9 b(ii) remains stable at 306.4 V. During fault period, although nominal of average source current (I_s) falls to 3.420 A, combination of wind and BES is able to generate power, store excess energy of wind, and inject current into load through shunt active filter so that average load current (I₁) in Figure 9 b(v) remains as 8.569 A. Figure 9 c(i) indicates on UPQC-BES supplied by PV-Wind Hybrid at t=0.2 s to t=0.5 s average source voltage (V_s) drops 100% to 0.4175 V. During the disturbance, PV-wind hybrid is able to generate power to UPQC DC link and injecting full average compensation voltage (V_c) in Figure 9 c(iii) through injection transformer on series active filter so that average load voltage (V_L) in Figure 9 b(ii) remains stable at 305.9 V. As long as disturbance period, although nominal of average source current (Is) falls to 3.640 A, combination of PV-wind hybrid and BES is able to generate power, store excess energy of wind, and inject current into load through shunt active filter so that average load current (I_L) in Figure 9 c(v) remains as 8.488 A.

Figure 10 shows spectra of load voltage harmonics on phase A of UPQC-BES system supplied by three RE sources using FLC in scenario 6. Figure 11 shows performance of average THD of load voltage and source current on UPQC-BES system supplied by three RE sources. Figure 11(a) shows that in scenario 1 to 5, the implementation of FLC on UPQC-BES system supplied by three RE sources is able to obtain average THD of load voltage slightly better than PI controller and both method have already met the limit in IEEE 519. Further under scenario 6, FLC applied on UPQC-BES system supplied by three RE sources gives significantly better result of average THD of load voltage than PI controller. In six disturbance scenarios, both PI controller and FLC applied on UPQC-BES system supplied by three RE sources, PV is able to obtain the highest average THD of load voltages. Figure 11(b) shows that in disturbance scenario 1 to 5, implementation of FLC on UPQC-BES system supplied by three RE sources is able to obtain average THD of source current slightly better than PI controller. Furthermore under scenario 6, FLC applied on UPQC-BES system supplied by three RE sources is able to obtain average THD of source current slightly better than PI controller. Furthermore under scenario 6, FLC applied on UPQC-BES system supplied by three RE sources is able to obtain average THD of source current slightly better than PI controller. Furthermore under scenario 6, FLC applied on UPQC-BES system supplied by three RE sources is able to obtain average THD of source current than PI controller. Both PI controller and FLC on UPQC-BES system supplied by three RE sources in six disturbance scenarios, PV is able to obtain the highest average THD of source current.



Matlab/simulink simulation of unified power quality conditioner-battery energy storage... (Amirullah)



Figure 10. Spectra of load voltage harmonics on phase A of UPQC-BES using FLC in scenario 6 (Inter-NL)



(a) Average load voltage harmonics



(b) Average source current harmonics

Figure 11. Performance of UPQC-BES supplied by three RE sources using PI and FLC

4. CONCLUSION

Comparative performance analysis of UPQC-BES system supplied by three RE sources i.e. PV, wind, and PV-wind hybrid respectively using PI controller and FLC have been discussed. In disturbance scenario 1 to 5, implementation of FLC on UPQC-BES system supplied by three RE sources is able to obtain average THD of load voltage slightly better than PI and both methods have already met the limit in IEEE 519. Under scenario 6, FLC applied on UPQC-BES system supplied by three RE sources gives significantly better result average THD of load voltage than PI. In six disturbance scenarios, both PI and FLC applied on UPQC-BES system supplied by three RE sources is able to obtain the highest average THD of load voltage. In interference scenario 1 to 5, FLC method on UPQC-BES system supplied by three RE sources is able to obtain average THD of source current slightly better than PI. Furthermore under scenario 6, FLC applied on UPQC-BES system supplied by three RE sources gives significantly better result of average THD of source current slightly better than PI. Furthermore under scenario 6, FLC applied on UPQC-BES system supplied by three RE sources gives significantly better result of average THD of source current slightly better than PI. Furthermore under scenario 6, FLC applied on UPQC-BES system supplied by three RE sources gives significantly better result of average THD of source current than PI. Both PI and FLC on UPQC-BES system supplied by three RE sources in six scenarios, PV is able to obtain the highest average THD of source current.

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APPENDIX

Three phase grid: RMS voltage 380 volt (L-L), 50 Hz, line impedance: $R_s=0.1$ Ohm $L_s=15$ mH; series and shunt active filter: series inductance $L_{se}=0.015$ mH; shunt inductance $L_{sh}=15$ mH; injection transformers: rating 10 kVA, 50 Hz, turn ratio $(N_1/N_2)=1:1$; non linear load: resistance $R_L=60$ ohm, inductance $L_L=0.15$ mH, load impedance $R_c=0.4$ ohm and $L_c=15$ mH; unbalance load: resistance $R_1=24$ ohm, $R_2=12$ ohm, and $R_3=6$ ohm, capacitance $C_1, C_2, C_3=2200 \ \mu\text{F}$; DC-link: voltage $V_{DC}=650$ volt and capacitance $C_{DC}=3000 \ \mu\text{F}$; battery energe storage: type=nickel metal hybrid, DC voltage=650 volt, rated capacity= 200 Ah, initial SOC=100%, inductance $L_1=6$ mH, capacitance $C_1=200 \ \mu\text{F}$; photovoltaic: active power= 0.6 kW temperature=25° C, irradiance=1000 W/m²; PMSG wind turbine active power=0.6 kW, voltage= 380 volt, 50 Hz, wind speed=5 m/s, picth angle=2; PI controller: $K_p=0.2$, $K_i=1.5$; fuzzy model: method= mamdani, composition=max-min; input membership function: error (V_{dc})=trapmf, trimf delta error (ΔV_{dc})= trapmf, trimf; output membership function: \overline{p}_{loss} =trapmf,trimf.

BIOGRAPHIES OF AUTHORS



Amirullah was born in Sampang East Java Indonesia, in 1977. He received bachelor and master degree in electrical engineering from University of Brawijaya Malang and ITS Surabaya, in 2000 and 2008, respectively. He also worked as a lecturer in University of Bhayangkara Surabaya. He is currently working toward the doctoral degree, in electrical engineering in Power System and Simulation Laboratory (PSSL) ITS Surabaya. His research interest includes power distribution modeling and simulation, power quality, harmonics migitation, design of filter/PFC, and RE.



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Lampiran 2.6 Revisi keempat makalah

Matlab/simulink simulation of unified power quality conditioner-battery energy storage system supplied by PV-wind hybrid using fuzzy logic controller

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ABSTRACT

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This paper presents performance analysis of Unified Power Quality Conditioner-Battery Energy Storage (UPQC-BES) system supplied by Photovoltaic (PV)-Wind Hybrid connected to three phase three wire (3P3W) of 380 volt (L-L) and 50 hertz distribution system. The performance of supply system is compared with two renewable energy (RE) sources i.e. PV and Wind, respectively. Fuzzy Logic Controller (FLC) is implemented to maintain DC voltage across the capacitor under disturbance scenarios of source and load as well as to compare the results with Proportional Intergral (PI) controller. There are six scenarios of disturbance i.e. (1) non-linear load (NL), (2) unbalance and nonlinear load (Unba-NL), (3) distortion supply and non-linear load (Dis-NL), (4) sag and non-linear load (Sag-NL), (5) swell and non-linear load (Swell-NL), and (6) interruption and non-linear load (Inter-NL). In disturbance scenario 1 to 5, implementation of FLC on UPQC-BES system supplied by three RE sources is able to obtain average THD of load voltage/source current slightly better than PI. Furthermore under scenario 6, FLC applied on UPQC-BES system supplied by three RE sources gives significantly better result of average THD of load voltage/source current than PI. This research is simulated using Matlab/Simulink.

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1. INTRODUCTION

PV and wind are the most RE distributed generations (DGs) because they are able to convert sunlight and wind into power. PV and solar are the potential DGs sources since it only need sunlight to generate electricity, where the resources are available in abundance, free and relatively clean. Indonesia has enormous energy potential from the sun because it lies on the equator. Almost all areas of Indonesia get sunlight about 10 to 12 hours per day, with an average intensity of irradiation of 4.5 kWh/m² or equivalent to 112.000 GW. The potential of wind energy in Indonesia generally has a speed between 4 to 5 m/s and classified as medium scale with potential capacity of 10 to 100 kW. The weakness of PV and wind turbine besides able to generate power, they also produces a number voltage and current harmonics resulted by presence of several types of PV and wind turbine devices and power converters as well as to increase a number of non-linear loads connected to the grid, so finally resulting in the decrease in power quality.

In order to overcome and improve power quality due to presence of non-linear loads and integration of PV and wind turbine to grid, UPQC is a proposed. UPQC serves to compensate for source voltage quality problemsi.e. sag, swell unbalance, flicker, harmonics, and load current quality problems i.e. harmonics,

unbalance, reactive currents, and neutral current. B. Han et. al and Vinod Khadkikar have investigated UPQC as one part of active power filter consisting of shunt and series active filters connected in parallel and serves as superior controller to overcome a number of power quality problems simultaneously. Series component has been responsible for reducing a number of interference on source side i.e. voltage sag/swell, flicker, unbalanced voltage, and harmonics. Shunt component has been responsible for addressing a current quality problems i.e. low power factor, load current harmonics, and unbalanced load. [1, 2]. UPQC based on RE has been investigated by some researchers. There are two methods used to overcome this problem i.e. using conventional and artificial intelligence. Shafiuzzaman K.K., et.al have proposed system includes a series inverter, shunt inverter, and a DG connected to a DC link through a rectifier using PI. The system was capable of increase source voltage quality i.e. sag and interruption and load current quality, as well as transfer of active power on/off grid mode [3]. The influence of DG on UPQC performance in reducing sag under conditions of some phase to ground faults to using DSTATCOM has been implemented by Norshafinash S., et.al. The DG was effective enough to help UPQC to improve sag [4]. It was connected in series with load resulting better sag mitigation compared to system without DG. Implementation of UPQC using UVTG method with PI to reduce sag, swell, voltage/current harmonics has been doneby S. N. Gohil, et.al. Simulation of voltage distortion was made by adding 5th and 7th harmonics at fundamental source voltage, resulting in a reduction of THD source current and THD load voltage [5].

UPQC supplied by PV panels using boost converter, PI, MPPT P and O, and p-q theory has been proposed by Yahia Bouzelata at.al [6]. The system was capable of compensate reactive power and reduce source current/load voltage harmonics, but did not discuss migitation of sag and interuption caused by PV penetration. Power quality enhancement of sag and source voltage harmonics on grid using UPQC supplied by PV array connected to DC link using PI compared with FLC has been done by Ramalengswara Rao, et.al. Combination of UPQC and PV using FLC can improve source voltage THD better than PI [7]. Amirullah et.al have researched a method for balancing current and line voltage, as a result of DGs of a single phase PV generator unit in randomly installed at homes through on a three phase four wire 220 kV and 50 Hz distribution line using BES and three of single phase bidirectional inverter. Both devices was capable of reduce unbalanced line current/voltage, but both of them were also capable of increase current/voltage harmonics on PCC bus [8]. Power quality migitation of UPQC on microgrid supplied by PV and wind turbine has been implemented by K S Srikanth et. al. It resulted that PI and FLC was able to improve power quality and reduce distortion in output power [9]. The UPQC-wind turbine to provide active power to overcome low sag and interruption voltage to grid has been investigated by H.Toodeji, et.al. The model was used VSC as a rectifier on generator output and controlled so that maximum power desired can be generated by different speed wind turbines using PI [10]. The UPQC-wind turbine connected to UPQC DC link was implemented by M. Hosseinpour, et al. The proposed combination using PI was capable of compensate swell, interruption voltage, and reactive power both on on/off grid [11]. R.Bhavani, et, al have researched on UPOC controlled by FLC to improve power quality in a DFIG wind turbine connected grid. FLC can improve power quality i.e. sag voltage and load current harmonics better than PI [12]. Power quality enhancement on wind turbine and BES with PI connected grid on PCC bus using UPQC has been implemented by S.RajeshRajan, et al. BES was installed to maintain and stabilize active power supply under different wind speed [13].

This research will analyze UPQC-BES performance supplied by PV-wind hybrid connected to 3P3W of 380 volt (L-L) and 50 hertz distribution system. The performance of supply system is compared with two RE sources i.e. PV and Wind, respectively. BES serves to store excess energy produced by three RE sources and distribute it to load if necessary, to prevent interruption voltage, and to adjust charging and discharging of energy in battery. BES is also expected to store excess power produced by three RE combinations and use it as backup power. FLC is proposed and compared with PI to control variable of DC voltage and DC reference voltage input to generate reference current source in current hysteresis controller on shunt active filter. DC voltage controller in shunt active filter and series active filter is used to migitate power quality of load voltage and source current.Performance of two controllers are used to determine load voltage, source current, load voltage THD, and source current THD based on IEEE 519. This paper is presented as follow. Section 2 describes proposed method, model of UPQC-BES system supplied by three RE sources i.e. PV, wind, and PV-wind hybrid, simulation parameters, PV and PMSG wind turbine model, series and shunt active filter, as well as application of PI and FLC method for proposed model. Section 3 shows results and analysis about performance of THD analysis on the proposed model of three RE sources connected to DC link of UPQC-BES system using PI and FLC. In this section, six disturbance scenarios are presented and the results are verified with Matlab/Simulink. Finally, this paper in concluded in Section 4.

2. RESEARCH METHOD

2.1. Proposed method

Figure 1 shows proposed model in this research. The RE sources based DGs used i.e. PV, Wind Turbine, and PV-Wind Turbine Hybrid connected to 3P3W distribution system with 380 volt (L-L) and 50 Hz frequency, through UPQC-BES system. PV array produce power under fixed temperature and radiation as well as connect to UPQC-DC link through a DC/DC boost converter. The maximum power point tracking (MPPT) method with Pertub and Observer (P and O) algorithms helps PV produce maximum power and generate output voltage, as the input voltage for DC/DC boost converter. The converter serves to adjust dutycycle value and output voltage of PV as its input voltage to produce an output voltage corresponding to UPQC DC link voltage. Wind turbine type used is a permanent magnetic synchronous generator (PMSG) with variable speed and fixed voltage which generating power and is connected to UPQC DC link circuit through AC/DC bridge rectifier. The rectifier helps to change AC PSMG stator output voltage to DC voltage through LC circuit that serves to filter and smooth it before connected to UPQC-DC link.BES connected to the UPQC-DC link circuit serves as energy storage and is expected to overcome interruption voltage and overall help UPQC performance to improve voltage and current quality on source and load bus. Simulation parameters proposed in this study is shown in Appendix Section. Power quality analysis is performed on PV, Wind, PV-Wind Hybrid respectively, connected to 3P3W system through UPQC DC-link (on-grid) using BES circuit. Single phase circuit breakers (CBs) are used to connect and disconnect PV, Wind, and Hybrid PV-Wind respectively with UPOC DC-link.

There are six disturbance scenarios i.e. (1) NL, (2) Unba-NL, (3) Dis-NL, (4) Sag-NL, (5) Swell-NL, and (6) Inter-NL. In scenario 1, the model is connected a non-linear load with R_L and L_L of 60 Ohm and 0.15 mH respectively. In scenario 2, the model is connected to non-linear load and during 0.3 s since t=0.2 s to t=0.5 s connected to unbalance three phase load with R1, R2, R3 as 6 Ohm, 12 Ohm, 24 Ohm respectively, and value of C1, C2, C3 as 2200 µF. In scenario 3, the model is connected to non-linear load and source voltage generating 5th and 7th harmonic components with individual harmonic distortion values of 5% and 2% respectively. In scenario 4, the model is connected to non-linear load and source experiences a sag voltage disturbance of 50% for 0.3 s between t=0.2 s to t=0.5 s. In scenario 5, the model is connected to a non-linear load and source experiences a swell voltage disturbance of 50% for 0.3 s between t=0.2 s to t=0.5 s. In scenario 6, the model is connected to non-linear load and source experiences an interruption voltage interference of 100% for 0.3 s between t=0.2 s to t=0.5 s. FLC is used as a DC voltage control in a shunt active filter to improve the power quality of the load voltage and current source and compare it with PI controller. Each disturbance scenario uses a PI controller and FLC so that the total of 12 disturbances. The result analysis of research was carried out i.e. (1) voltage and current on source or poin common coupling (PCC) bus, (2) voltage and current on load bus, (3) harmonic voltage and harmonic current on source bus and (4) harmonic voltage and harmonic current on load bus. The final phase is to compare performance of UPQC-BES system on-grid supplied by PV, Wind, PV-Wind Hybrid respectively using two controllers to improve power quality of load voltage and source current under six disturbance conditions.



Figure 1. Proposed model of UPQC-BES system supplied by PV, Wind, and PV-Wind Hybrid

2.2. Photovoltaic model

Figure 2 shows the equivalent circuit and V-I characteristic of a solar panel. A solar panel is composed of several PV cells that have series, parallel, or series-parallel external connections [14].



Figure 2. Equivalent circuit and V-I characteristic of solar panel

The V-I characteristic of a solar panel is showed in (1):

$$I = I_{PV} - I_o \left[\exp\left(\frac{V + R_s I}{aV_t}\right) - 1 \right] - \frac{V + R_s I}{R_p}$$
(1)

where I_{PV} is the photovoltaic current, I_o is saturated reverse current, 'a' is the ideal diode constant, $V_t = N_S K T q^{-1}$ is the thermal voltage, N_S is the number of series cells, q is the electron charge, K is the Boltzmann constant, T is the temperature of p–n junction, R_S and R_P are series and parallel equivalent resistance of the solar panels. I_{PV} has a linear relation with light intensity and also varies with temperature variations. I_o is dependent on temperature variations. The values of I_{pv} and I_o are calculated as following (2) and (3):

$$I_{PV} = (I_{PV,n} + K_1 \Delta T) \frac{G}{G_n} I$$
⁽²⁾

$$I_o = \frac{I_{SC,n} + K_I \Delta T}{\exp(V_{OC,n} + K_V \Delta T) / aV_t - 1}$$
(3)

In which $I_{PV,n}$, $I_{SC,n}$ and $V_{OC,n}$ are photovoltaic current, short circuit current and open circuit voltage in standard conditions ($T_n=25$ C and $G_n=1000$ Wm⁻²) respectively. K_I is the coefficient of short circuit current to temperature, $\Delta T=T-T_n$ is the temperature deviation from standard temperature, G is the light intensity and K_I is the ratio coefficient of open circuit voltage to temperature. Open circuit voltage, short circuit current and voltage-current corresponding to the maximum power are three important points of I-V characteristic of solar panel. These points are changed by variations of atmospheric conditions. By using (4) and (5) which are derived from PV model equations, short circuit current and open circuit voltage can be calculated in different atmospheric conditions.

$$I_{SC} = (I_{SC} + K_1 \Delta T) \frac{G}{G_n}$$
⁽⁴⁾

$$V_{OC} = V_{OC} + K_V \Delta T \tag{5}$$

2.3. PMSG wind turbine

Wind turbine is one of part of an integrated system, which can be divided into two types i.e. fixed and variable speed wind turbines. In fixed speed type, rotating speed of turbine is fixed and hence, frequency of generated voltage remains constant, so it can be directly connected to the network. In this case, maximum power can not always be extracted by wind. On the other hand, on variable speed, turbine can rotate at different speeds, so maximum power can be generated in each wind speed by MPPT method [10]. The advantage of using a PMSG over a synchronous generator and DFIG machine because it has high efficiency and reliability. Due to the elimination of rotor external excitation, machine size, and cost also decreases, making PMSG to be more controlled easily with feedback control system. PMSG has become an attractive solution on wind generation systems with variable speed wind turbine applications [15]. Figure 3 and 4 shows model of PMSG wind turbine and wind turbin power characteristic curve.



Figure 3. Model of PMSG wind turbine



Figure 4. Wind turbin power characteristic curve

The output power of wind turbine can be expressed using (6), (7), and (8) [11].

$$\lambda = \frac{\omega_r R}{V_{wind}} \tag{6}$$

$$P_M = \frac{1}{2} \rho \pi R^2 C_p V_{wind}^3 \tag{7}$$

$$T_{M} = \frac{P_{M}}{\omega_{r}} = \frac{1}{2} \rho \pi R^{5} C_{p} \frac{\omega_{M}^{3}}{\lambda^{3}}$$

$$\tag{8}$$

Where λ is the speed-tip ratio, V_{wind} is wind speed, R is blade radius, ω_r is rotor speed (rad/sec), ρ is the air density, C_P is the power coefficient, P_M is the output mechanical power, and T_M is output torque of wind turbine. The C_P coefficient is dependent on the pitch angle value, at which rotor blade can rotate along axis and tip-speed ratio λ expressed in (9).

$$C_p = (0.44 - 0.167\beta)\sin\frac{\pi(\lambda - 2)}{(13 - 0.3\beta)}$$
(9)

Where β is a pitch angle blade. In a fixed pitch type, the value of β is set to a fixed value.

2.4. Control of series active filter

The main function of series active filter is as a sensitive load protection against a number of voltage interference at PCC bus. The control strategy algorithm of the source and load voltage in series active filter circuit is shown in Figure 5. It extracts the unit vector templates from the distorted input supply. Furthermore, the templates are expected to be ideal sinusoidal signal with unity amplitude. The distorted supply voltages are measured and divided by peak amplitude of fundamental input voltage V_m give in (10) [6].

$$V_m = \sqrt{\frac{2}{3} \left(V_{sa}^2 + V_{sb}^2 + V_{sc}^2 \right)}$$
(10)

A three phase locked loop (PLL) is used in order to generate a sinusoidal unit vector templates with a phase lagging by the use of sinus function. The reference load voltage signal is determined by multiplying the unit vector templates with the peak amplitude of the fundamental input voltage V_m . The load reference voltage (V_{La}^* , V_{Lb}^* , V_c^*) is then compared against to sensed load voltage (V_{La} , V_{Lb} , V_{Lc}) by a pulse width modulation (PWM) controller used to generate the desired trigger signal on series active filter.



Figure 5. Control strategy of series active filter

2.5. Control of shunt active filter

The main function of shunt active filter is mitigation of power quality problems on the load side. The control methodology in shunt active filter is that the absorbed current from the PCC bus is a balanced positive sequence current including unbalanced sag voltage conditions in the PCC bus or unbalanced conditions or non-linear loads. In order to obtain satisfactory compensation caesed by disturbance due to non-linear load, many algorithms have been used in the literature. This research used instantaneous reactive power theory method "p-q theory". The voltages and currents in Cartesian *abc* coordinates can be transformed to Cartesian $\alpha\beta$ coordinates as expressed in (11) and (12) [16].

$$\begin{bmatrix} v_{\alpha} \\ v_{\beta} \end{bmatrix} = \begin{bmatrix} 1 & -1/2 & -1/2 \\ 1 & \sqrt{3}/2 & -\sqrt{3}/2 \end{bmatrix} \begin{bmatrix} V_{\alpha} \\ V_{b} \\ V_{c} \end{bmatrix}$$
(11)

$$\begin{bmatrix} i_{\alpha} \\ i_{\beta} \end{bmatrix} = \begin{bmatrix} 1 & -1/2 & -1/2 \\ 1 & \sqrt{3}/2 & -\sqrt{3}/2 \end{bmatrix} \begin{bmatrix} i_{La} \\ i_{Lb} \\ i_{Lc} \end{bmatrix}$$
(12)

The computation of the real power (p) and imaginary power (q) is showed in (13). The real power and imaginary are measured instantaneously power and in matrix it is form is given as. The presence of oscillating and average components in instantaneous power is presented in (14) [17].

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$$\begin{bmatrix} p \\ q \end{bmatrix} = \begin{bmatrix} v_{\alpha} & v_{\beta} \\ -v_{\beta} & v_{\alpha} \end{bmatrix} \begin{bmatrix} i_{\alpha} \\ i_{\beta} \end{bmatrix}$$
(13)

$$p = \overline{p} + \widetilde{p} \quad ; q = \overline{q} + \widetilde{q} \tag{14}$$

Where \overline{p} = direct component of real power, \widetilde{p} = fluctuating component of real power, \overline{q} = direct component of imaginary power, \widetilde{q} = fluctuating component of imaginary power. The total imaginary power (q) and the fluctuating component of real power are selected as power references and current references and are utilized through the use of (15) for compensating harmonic and reactive power [18].

$$\begin{bmatrix} i_{c\alpha}^{*} \\ i_{c\beta}^{*} \end{bmatrix} = \frac{1}{v_{\alpha}^{2} + v_{\beta}^{2}} \begin{bmatrix} v_{\alpha} & v_{\beta} \\ v_{\beta} & -v_{\alpha} \end{bmatrix} \begin{bmatrix} -\widetilde{p} + \overline{p}_{loss} \\ -q \end{bmatrix}$$
(15)

The signal \overline{p}_{loss} , is obtained from voltage regulator and is utilized as average real power. It can also be specified as the instantaneous active power which corresponds to the resistive loss and switching loss of the UPQC. The error obtained on comparing the actual DC-link capacitor voltage with the reference value is processed in FLC, engaged by voltage control loop as it minimizes the steady state error of the voltage across the DC link to zero. The compensating currents ($i_{c\alpha}^*$, $i_{c\beta}^*$) as required to meet the power demand of load are shown in (15). These currents are represented in α - β coordinates. The phase current is required to acquire using (16) for compensation. These source phase currents (i_{sa}^* , i_{sb}^* , i_{sc}^*) are represented in a-b-c axis obtained from the compensating current in the α - β coordinates presented in (16) [18]. Figure 6 shows a control of shunt active filter.

$$\begin{bmatrix} i_{s_{\alpha}}^{*} \\ i_{s_{b}}^{*} \\ i_{s_{c}}^{*} \end{bmatrix} = \sqrt{\frac{2}{3}} \begin{bmatrix} 1 & 0 \\ -1/2 & \sqrt{3}/2 \\ -1/2 & -\sqrt{3}/2 \end{bmatrix} \begin{bmatrix} i_{c\alpha}^{*} \\ i_{c\beta}^{*} \end{bmatrix}$$
(16)



Figure 6. Control strategy of shunt active filter

The proposed model of UPQC-BES system supplied by three RE sources is shown in Figure 1. From the figure, we can see that PV is connected to the DC link through a DC-DC boost converter circuit. The PV partially distributes power to the load and the remains is transfered to three phase grid. The load consists of non linear and unbalanced load. The non-linear load is a diode rectifier circuit with the RL load type, while the unbalanced load is a three phase RC load with different R value on each phase. In order to economically efficient, PV must always work in MPP condition. In this research, MPPT method used is P and O algorithm. The model is also applied for UPQC-BES system which is supplied by wind and PV-wind hybrid respectively. In order to operate properly, UPQC-BES system device must have a minimum DC link voltage (V_{dc}). The value of common DC link voltage depends on the nstantaneous energy avialable to UPQC is defined by in (17) [16]:

$$V_{dc} = \frac{2\sqrt{2}V_{LL}}{\sqrt{3}m} \tag{17}$$

where m is modulation index and V_{LL} is the AC grid line voltage of UPQC. Considering that modulation index as 1 and for line to line grid voltage (V_{LL} =380 volt), the V_{dc} is obtained 620, 54 volt and selected as 650 volt.

The input of shunt active filter showed in Figure 5 is DC voltage (V_{dc}) and reference DC voltage (V_{dc}^*), while the output is \bar{p}_{loss} by using PI controller. Then, the \bar{p}_{loss} is as one of input variable to generate the reference source current (I_{sa}^* , I_{sb}^* , and I_{sc}^*). The reference source current output is then compared to source current (I_{sa} , I_{sb} , and I_{sc}) by the current hysteresis control to generate trigger signal in IGBT circuit of shunt active filter. In this research, FLC as DC voltage control algorithm on shunt active filter is proposed and compared with PI controller. The FLC is capable of reduce oscilation and generate quick convergence calculation during disturbances. This method is also used to overcome the weakness of PI controller in determining proportional gain (K_p) and integral gain constant (K_i) which still use trial and error method.

2.6. Fuzzy logic controller

The research is started by determine \overline{p}_{loss} as the input variable to result the reference source current on current hysteresis controller to generate trigger signal on the IGBT shunt active filter of UPQC using PI controller (K_p=0.2 and K_i=1.5). By using the same procedure, \overline{p}_{loss} is also determined by using FLC. The FLC has been widely used in recent industrial process because it has heuristic, simpler, more effective and has multi rule based variables in both linear and non-linear system variations. The main components of FLC are fuzzification, decision making (rulebase, database, reason mechanism) and defuzzification in Figure 7. The output membership function is generated using inference blocks and the basic rules of FLC as shown in Table 1.



The fuzzy rule algorithm collects a number of fuzzy control rules in a particular order. This rule is used to control the system to meet the desired performance requirements and they are designed from a number of intelligent system control knowledge. The fuzzy inference of FLC using Mamdani method related to max-min composition. The fuzzy inference system in FLC consists of three parts: rule base, database, and reasoning mechanism [19]. The FLC method is performed by determining input variables V_{dc} (V_{dc-error}) and delta Vdc ($\Delta V_{dc-error}$), seven linguistic fuzzy sets, operation fuzzy block system (fuzzyfication, fuzzy rule base and defuzzification), $V_{dc-error}$ and $\Delta V_{dc-error}$ during fuzzification process, fuzzy rule base table, crisp value to determine \bar{p}_{loss} in defuzzification phase. The \bar{p}_{loss} is one of input variable to obtain compensating currents (i_{ca}^*, i_{cb}^*) in (16). During fuzzification process, a number of input variables are calculated and converted into linguistic variables based on a subset called membership function. The error Vdc (V_{dc-error}) and delta error Vdc ($\Delta V_{dc-error}$) are proposed input variable system and output variable is \overline{p}_{loss} . To translate these variables, each input and output variable is designed using seven membership functions: Negative Big (NB), Negative Medium (NM), Negative Small (NS), Zero (Z), Positive Small (PS), Positive Medium (PM) and Positive Big (PB). The membership functions of crisp input and output are presented with triangular and trapezoidal membership functions. The value of V_{dc-error} range from -650 to 650, $\Delta V_{dc-error}$ from -650 to 650, and \bar{p}_{lass} from -100 to 100. The input and output MFs are shown in Figure 8.



Figure 8. Membership functions (a) $V_{dc-error}$, (b) $\Delta V_{dc-error}$, and (c) \overline{p}_{lass}

After the V_{dc-error} and Δ V_{dc-error} are obtained, then two input membership functions are converted to linguistic variables and uses them as input functions for FLC. The output membership function is generated using inference blocks and the basic rules of FLC as shown in Table 1. Finally the defuzzification block operates to convert generated \overline{p}_{loss} output from linguistic to numerical variable again. Then it becomes input variable for current hysteresis controller to produce trigger signal on the IGBT circuit of UPQC shunt active filter to reduce source current and load voltage harmonics. While simultaneously, it also improve power quality of 3P3W system under six scenarios due to the integration of three RE sources to UPQC-BES system.

3. RESULTS AND ANALYSIS

The analysis of proposed model is investigated through determination of six disturbance scenarios i.e. (1) NL, (2) Unba-NL, (3) Dis-NL, (4) Sag-NL, (5) Swell-NL, and (6) Inter-NL. Each scenario of UPQC uses PI controller and FLC so total number of disturbance are 12 scenarios.By using Matlab/Simulink, the model is then executed according to the desired scenario to obtain curve of source voltage (V_s), load voltage (V_L), compensation voltage (V_c), source current (V_s), load current (I_L), and DC voltage DC link (V_{dc}). Then, THD value of source voltage, source current, load voltage, and load current in each phase as well as average THD value (Avg THD) are obtained base on the curves. THD in each phase is determined in one cycle started at t = 0.35 s. The results of average of source voltage, source current, load voltage, source current of 3P3W system using UPQC-BES system supplied by three RE sources i.e. PV, wind, and PV-wind hybrid are presented in Table 2, 3, and 4. Next THD in each phase and average THD are showed in Table 5, 6 and 7.

Table 2 shows UPQC-BES system supplied PV connected 3P3W system using PI and FLC, disturbance scenarios 1 to 5 produce an average load voltage above 307 V. While in scenario 6, FLC produces a higher average load voltage of 304.1 V than if using a PI of 286.7 V. If reviewed from average source current with PI, the highest and lowest average source currents are generated by disturbance scenarios

2 and 4 of 28.15 A and 7,246 A. Whereas if using FLC the highest and lowest average source currents are achieved in scenario 2 and 6 of 28.84 A and 3.804 A. Table 3 shows UPQC-BES supplied by wind connected to 3P3W with PI and FLC, scenarios 1 to 5 is able to obtain a stable load voltage above 308 V. The difference is that in scenario 6, PI generates a load voltage of 274.8 V, otherwise if using FLC, load voltage increases to 306.4 V. If reviewed from source current using PI, the highest and lowest average source currents are resulted by scenarios 2 and 4 of 28.28 A and 7.417 A. Rather, if using FLC, the highest and lowest average source currents are achieved in scenario 2 and 6 of 28.82 A and 3,420 A. Table 4 shows UPQC-BES supplied PV-wind hybrid connected 3P3W using PI and FLC, scenarios 1 to 5 produce an average load voltage above 307 V. While in scenario 6, FLC generates an average load voltage 305.9 V higher than if using PI control of 283.9 V. If reviewed from average source current with PI, the highest and lowest average source currents are resulted by scenarios 2 and 4 of 28.21 A and 6,773 A. Otherwise if using FLC the highest and lowest average source currents are achieved in scenario 2 and 6 of 28.82 A and 3.640 A respectively.

Table 2. Voltage and Current of 3P3W System Using UPQC-BES System Supplied by PV

Con	So	urce Vol	tage V _S ((V)		Load Vo	ltage V _L (V)	Se	ource Cu	rrent I _S (.	A)	I	Load Cu	rent I _L (A	<i>I</i>)
Self	Ph A	Ph B	Ph C	Avg	Ph A	Ph B	Ph C	Avg	Ph A	Ph B	Ph C	Avg	Ph A	Ph B	Ph C	Avg
							PI	Controlle	er							
1	309.6	309.6	309.6	309.6	307.6	307.8	307.7	307.7	7.766	7.793	7.759	7.773	8.528	8.529	8.533	8.530
2	307.4	308.0	308.0	307.8	308.3	308.7	308.3	308.4	31.00	24.84	28.73	28.15	22.50	34.12	34.52	30.38
3	309.6	309.6	309.6	309.6	313,8	314.3	317.4	317.4	7.897	7.919	7.867	7.895	8.748	8.704	8.785	8.746
4	154.5	154.5	154.5	154.5	307.1	307.3	307.3	307.2	7.235	7.276	7.226	7.246	8.509	8.514	8.510	8.511
5	464.7	464.7	464.7	464.7	308.6	308.7	308.6	308.6	7.979	7.980	7.964	7.975	8.550	8.553	8.554	8.553
6	0.536	1.385	0.850	0.924	310.2	259.8	290.2	286.7	7.392	12.67	6.045	8.703	8.707	7.747	7.637	8.031
							Fuzzy l	Logic Cor	troller							
1	309.5	309.5	309.5	309.5	307.7	307.9	307.7	307.8	8.420	8.426	8.416	8.421	8.527	8.532	8.531	8.530
2	307.4	307.9	308.0	307.8	308.5	308.7	308.4	308.5	31.66	25.50	29.36	28.84	22.52	34.11	35.52	30.72
3	309.6	309.5	309.5	309.5	313.4	312.9	315.9	314.1	8.516	8.565	8.496	8.526	8.741	8.677	8.736	8.718
4	154.4	154.4	154.4	154.4	307.3	307.3	307.2	307.3	8.563	8.560	8.561	8.561	8.514	8.517	8.512	8.515
5	464.6	464.6	464.6	464.6	308.6	308.8	308.6	308.7	8.396	8.389	8.389	8.392	8.552	8.556	8.554	8.554
6	0.447	0.392	0.380	0.407	314.0	293.4	304.9	304.1	4.024	3.778	3.608	3.804	8.874	8.195	8.193	8.421

Table 3. Voltage and Current of 3P3W System Using UPQC-BES System Supplied by Wind

C	So	urce Vol	tage Vs (V)	L	oad Volt	age V _L (V	V)	Se	ource Cu	rrent Is (A	A)		Load Curr	ent I _L (A)	
SCII	Ph A	Ph B	Ph C	Avg	Ph A	Ph B	Ph C	Avg	Ph A	Ph B	Ph C	Avg	Ph A	Ph B	Ph C	Avg
								PI Cont	roller							
1	309.5	309.6	309.6	309.6	308.6	308.6	308.2	308.5	7.863	7.875	7.840	7.869	8.554	8.553	8.546	8.551
2	307.4	308.0	308.0	308.0	308.9	309.2	308.7	308.9	31.07	24.97	28.81	28.28	22.55	34.17	34.57	30.43
3	309.6	309.5	309.6	309.6	312.9	312.9	315.4	313.8	7.993	8.015	7.947	7.985	8.817	8.682	8.741	8.747
4	154.5	154.5	154.5	154.5	308.0	308.1	307.8	307.9	7.428	7.455	7.368	7.417	8.527	8.535	8.532	8.531
5	464.7	464.7	464.7	464.7	309.3	309.3	309.0	309.2	8.015	8.020	8.002	8.012	8.564	8.573	8.568	8.568
6	1.256	1.022	0.592	0.957	234.0	316.4	274.0	274.8	11.27	9.866	7.028	9.388	5.958	8.697	8.204	7.619
							Fuz	zy Logic	Controll	er						
1	309.5	309.5	309.5	309.5	308.5	308.6	308.3	308.5	8.418	8.410	8.414	8.414	8.545	8.552	8.549	8.549
2	307.4	307.9	308.0	307.8	309.0	309.3	308.9	309.1	31.64	25.47	29.34	28.82	22.56	34.18	34.59	30.44
3	309.5	309.5	309.5	309.5	313.2	313.7	314.1	313.7	8.519	8.531	8.531	8.527	8.713	8.714	8.718	8.715
4	154.4	154.4	154.4	154.4	308.0	308.1	307.7	307.9	8.557	8.539	8.561	8.552	8.528	8.541	8.525	8.531
5	464.6	464.7	464.7	464.7	309.2	309.3	309.2	309.2	8.391	8.385	8.388	8.388	8.565	8.570	8.567	8.567
6	0.357	0.396	0.397	0.383	303.7	300.0	315.3	306.4	3.358	3.464	3.542	3.420	8.557	8.418	8.731	8.569

Table 4. Voltage and Current of 3P3W System Using UPQC-BES System Supplied PV-Wind Hybrid

Son	So	Source Voltage $V_{S}(V)$ Load Voltage $V_{L}(V)$ Source Current $I_{S}(A)$								I	load Curi	rent I _L (A	.)			
SCII	Ph A	Ph B	Ph C	Avg	Ph A	Ph B	Ph C	Avg	Ph A	Ph B	Ph C	Avg	Ph A	Ph B	Ph C	Avg
							PI	Controll	er							
1	309.6	309.6	309.6	309.6	307.8	308.0	307.7	307.8	7.790	7.802	7.770	7.787	8.527	8.537	8.533	8.533
2	307.4	308.0	308.0	307.8	308.4	308.8	308.4	308.6	31.02	24.87	28.74	28.21	22.52	34.13	34.53	31.40
3	309.6	309.5	309.6	309.6	314.0	315.5	316.9	315.5	7.942	7.939	7.918	7.933	8.739	8.750	8.783	8.757
4	154.5	154.5	154.5	154.5	307.3	307.4	307.2	307.3	7.289	7.309	7.251	7.283	8.513	8.516	8.515	8.515
5	464.7	464.7	464.7	464.7	308.7	308.9	308.7	308.8	7.985	7.985	7.975	7.982	8.552	8.558	8.558	8.556
6	1.048	0.825	0.845	0.906	247.5	300.7	303.7	283.9	5.119	5.927	9.271	6.773	7.016	7.893	8.793	7.867
							Fuzzy I	logic Con	ntroller							
1	309.5	309.5	309.5	309.5	307.8	308.0	307.7	307.8	8.419	8.418	8.409	8.413	8.529	8.539	8.533	8.534
2	307.4	307.9	308.0	307.8	308.7	308.7	308.9	308.8	31.66	25.47	29.32	28.82	22.54	34.13	34.56	30.41
3	309.5	309.5	309.5	309.5	314.4	315.5	316.6	315.5	8.581	8.593	8.568	8.581	8.761	8.722	8.761	8.748
4	154.4	154.4	154.4	154.4	307.3	307.5	307.3	307.4	8.566	8.572	8.563	8.567	8.511	8.520	8.519	8.517
5	464.6	464.6	464.6	464.6	308.8	308.8	308.7	308.8	8.391	8.394	8.396	8.394	22.33	22.35	22.36	22.35
6	0.412	0.403	0.402	0.418	311.6	295.7	310.4	305.9	3.774	3.544	3.593	3.640	8.855	8.321	8.288	8.488

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		Ta	ble 5.	Harm	onics	of 3P3	W Sys	stem U	sing UF	QC-BE	ES Syste	em Supp	olied b	y PV		
C	Sou	rce Volta	ge THD ((%)	Lo	ad Voltag	ge THD ((%)	Se	ource Curr	ent THD (%)		Load Cu	rrent (%)	
Scii	Ph A	Ph B	Ph C	Avg	Ph A	Ph B	Ph C	Avg	Ph A	Ph B	Ph C	Avg	Ph A	Ph B	Ph C	Avg
								PI Co	ntroller							
1	2.35	2.36	2.32	2.34	2.48	2.50	2.46	2.48	12.89	12.72	12.92	12.84	22.32	22.34	22.32	22.33
2	2.29	2.20	2.24	2.24	2.43	2.23	2.37	2.34	2.660	2.330	2.240	2.410	5.230	2.070	2.660	3.320
3	5.84	5.86	5.94	5.88	6.36	5.90	6.58	6.28	12.75	12.64	13.06	12.82	21.92	22.16	22.33	22.14
4	4.69	4.75	4.81	4.75	2.46	2.48	2.53	2.49	14.26	13.96	14.16	14.13	22.28	22.31	22.28	22.29
5	1.56	1.53	1.55	1.55	2.47	2.43	2.45	2.45	12.51	12.36	12.44	12.44	22.34	22.32	22.32	22.33
6	NA	NA	NA	NA	32.11	15.09	28.54	25.25	270.90	145.89	275.67	230.82	47.70	34.58	36.29	39.53
							F	uzzy Log	ic Controll	ler						
1	2.35	2.33	2.35	2.34	2.48	2.46	2.49	2.47	11.83	11.82	11.84	11.83	22.33	22.32	22.33	22.33
2	2.25	2.27	2.20	2.24	2.39	2.41	2.34	2.38	2.620	2.400	2.220	2.413	5.230	2.100	2.640	3.323
3	5.83	5.88	5.93	5.88	6.23	5.93	6.69	6.28	11.83	11.90	12.14	11.96	21.84	22.34	22.53	22.24
4	4.71	4.76	4.79	4.75	2.46	2.48	2.50	2.48	11.91	11.88	11.86	11.89	22.27	22.32	22.32	22.31
5	1.55	1.54	1.54	1.54	2.45	2.44	2.46	2.45	11.90	11.84	11.85	11.86	22.36	22.33	22.35	22.35
6	NA	NA	NA	NA	13.05	6.60	11.15	10.27	30.61	34.72	31.57	32.30	24.25	24.25	24.71	24.40

Table 6. Harmonics of 3P3W System Using UPQC-BES System Supplied by Wind

Con	Sour	ce Volta	ge THD	(%)	Lo	ad Volta	ge THD ((%)	Sc	ource Curr	ent THD (9	%)		Load Cu	rrent (%)	
SCII	Ph A	Ph B	Ph C	Avg	Ph A	Ph B	Ph C	Avg	Ph A	Ph B	Ph C	Avg	Ph A	Ph B	Ph C	Avg
								PI Cor	ntroller							
1	1.88	1.87	1.94	1.89	1.99	1.97	2.05	2.00	12.63	12.37	12.70	12.57	12.30	12.30	12.34	12.31
2	1.83	1.76	1.82	1.80	1.92	1.85	1.93	1.90	2.460	2.070	2.200	2.240	5.260	2.070	2.690	3.340
3	5.67	5.71	5.77	5.72	6.00	6.83	6.02	6.28	12.48	12.26	12.66	12.47	22.01	22.12	22.08	22.07
4	3.76	3.86	3.86	1.83	1.97	2.02	2.03	2.01	13.59	13.17	13.51	13.42	22.29	22.31	22.30	22.30
5	1.26	1.24	1.29	1.26	1.99	1.97	2.05	2.00	12.31	12.20	12.31	12.27	22.36	22.33	22.37	22.35
6	NA	NA	NA	NA	14.09	35.59	34.73	28.14	157.76	139.01	266.07	186.95	37.60	34.39	46.97	39.65
							Fι	ızzy Logi	c Controll	er						
1	1.89	1.88	1.93	1.90	1.99	1.98	2.04	2.00	11.71	11.72	11.77	11.73	22.34	22.31	22.32	22.32
2	1.85	1.79	1.78	1.81	1.95	1.87	1.88	1.90	2.43	2.11	2.12	2.220	5.240	2.070	2.700	3.240
3	5.67	5.71	5.78	5.72	5.99	6.39	6.13	6.17	11.72	11.62	11.90	11.75	22.08	21.94	22.47	22.16
4	3.79	3.81	3.86	3.82	1.97	1.99	2.03	1.99	11.72	11.69	11.74	11.72	22.28	22.30	22.35	22.31
5	1.27	1.24	1.28	1.26	2.00	1.96	2.04	2.00	11.66	11.76	11.76	11.73	22.31	22.33	22.35	22.33
6	NA	NA	NA	NA	7.59	6.44	10.95	8.33	27.33	28.27	26.39	27.33	25.39	23.65	24.31	24.45

Table 7. Harmonics of 3P3W System Using UPQC-BES System Supplied by PV-Wind Hybrid

								-	-		-					
Son	Sour	rce Voltag	ge THD	(%)	Loa	d Voltag	e THD (9	%)	Sc	ource Curre	ent THD (%)		Load Cu	rrent (%)	
Self	Ph A	Ph B	Ph C	Avg	Ph A	Ph B	Ph C	Avg	Ph A	Ph B	Ph C	Avg	Ph A	Ph B	Ph C	Avg
								PI Co	ntroller							
1	2.25	2.19	2.29	2.24	2.37	2.31	2.42	3.37	12.85	12.62	12.74	12.74	22.33	22.31	22.34	22.33
2	2.18	2.08	2.15	2.13	2.30	2.19	2.18	2.22	2.630	2.300	2.290	2.407	5.230	2.070	2.670	3.323
3	5.81	5.82	5.89	5.84	6.12	5.88	6.75	6.25	12.71	12.63	12.98	12.77	22.05	22.13	22.54	22.24
4	4.53	4.48	4.51	4.51	2.37	2.35	2.37	2.36	14.16	13.50	13.99	13.88	22.27	22.30	22.28	22.28
5	1.49	1.46	1.51	1.49	2.37	2.31	2.40	2.36	12.43	12.29	12.41	12.38	22.34	22.32	22.33	22.33
6	NA	NA	NA	NA	18.61	36.38	28.42	27.8	387.71	330.34	189.29	302.45	36.73	38.51	36.83	37.36
							Fuz	zy Log	ic Control	ler						
1	2.25	2.23	2.25	2.24	2.37	2.35	2.39	2.37	11.85	11.74	11.84	11.81	22.32	22.31	22.33	22.32
2	2.23	2.15	2.05	2.14	2.37	2.26	2.17	2.26	2.520	2.410	2.140	2.446	5.230	2.070	2.690	3.330
3	5.80	5.83	5.90	5.84	6.57	5.26	7.06	6.29	11.83	11.78	12.24	11.95	22.15	22.23	22.95	22.44
4	4.53	4.52	4.54	4.86	2.36	2.35	2.35	2.35	11.79	11.74	11.84	11.79	22.29	22.30	22.29	22.29
5	1.48	1.46	1.51	1.48	2.35	2.32	2.40	2.35	11.78	11.81	11.81	11.80	22.33	22.35	22.36	22.35
6	NA	NA	NA	NA	10.30	4.90	10.25	8.48	27.44	29.52	28.63	28.53	23.20	23.97	24.65	23.94

Table 5 shows that average THD of load voltage (V_L) of UPQC-BES system supplied by PV in 3P3W system for scenarios 1 to 5 using PI control is within limits in IEEE 519. The highest and lowest average THD load voltages achieved under scenario 6 and 2 as 25.25% and 2.34% respectively. PI controller is also able to mitrgaron average THD source voltage in scenario 6 from not accessible (NA) to 25.25% on the load side. The highest and lowest average THD of source current are achieved in scenario 6 and 2 as 230.82% and 2.41%. Table 5 also indicates that average THD of load voltage of UPQC system supplied by PV with BES using FLC in scenarios 1 to 5, has fulfilled limits in IEEE 519. The highest and lowest average THD of load voltage are achieved under scenario 6 and 2 of 10.27% and 2.38%. The use of FLC method is also able to reduce average THD on source voltage in scenario 6 from NA to 10.27% on load side. The highest average THD of source current are achieved in scenario 6 and 2 of 32.30% and 2.413%.

Table 6 shows that average THD of load voltage of UPQC-BES system supplied by wind in 3P3W system for interference scenarios 1 to 5 using PI is within limits prescribed in IEEE 519. The highest and lowest average THD load voltages is achieved under scenario 6 and scenario 2 as 28.14% and 1.90% respectively. PI controller is also able to reduce average THD source voltage in scenario 6 from NA to 28.14% on the load side. The highest and lowest average THD of source current are achieved in scenario 6 and 2 as 186.95% and 2.24% respectively. Table 6 also shows that average THD of load voltage of UPQC-BES supplied by wind using FLC in scenarios 1 to 5, has fulfilled limits prescribed in IEEE 519. The highest and lowest average THD of load voltage are achieved under scenario 6 and 4 of 8.33% and 1.90%. FLC method is also able to reduce average THD on source voltage in scenario 6 from NA to 7.33% on load side. The highest and lowest average THD source current are achieved in scenario 6 and 2 of 27.33% and 2.22%.

Table 7 shows that average THD of load voltage (V_L) of UPQC-BES system supplied by PV-wind hybrid in 3P3W system for scenarios 1 to 5 using PI is within limits in IEEE 519. The highest and lowest average THD load voltages are achieved under scenario 6 and 2 as 27.8% and 2.22% respectively. PI is also able to mitigate average THD source voltage in scenario 6 from NA to 27.8% on load side. The highest and lowest average THD of source current are achieved in scenario 6and 2 as 302.45% and 2.407% respectively. Table 7 also indicates that average THD of load voltage of UPQC-BES system supplied by PV-wind hybrid using FLC for scenarios 1 to 5, has fulfilled limits in IEEE 519. The highest and lowest average THD of load voltage are achieved under scenario 6 and 2 of 8.48% and 2.26%. FLC method is also able to reduce average THD on source voltage in scenario 6 from NA to 8.48% on load side. The highest and lowest average THD of source current are achieved in scenario 5 and 2 of 28.53% and 2.446%. Overall for UPQC-BES systemsystem supplied by three RE sources in scenarios 1 to 5 using PI and FLC is able to improve average THD of source current better on average THD of load current. Figure 9 presents UPQC-BES system performance supplied by three RE sources using FLC in scenario 6.

Figure 9 a(i) shows that in scenario 6, UPQC-BES system supplied by PV at t=0.2 s to t=0.5 s, average source voltage (V_S) falls as 100% to 0.4062 V. During the disturbance, PV is able to generate power to UPQC DC link and injecting full average compensation voltage (V_c) in Figure 9 a(iii) through injection transformer on series active filter so that average load voltage (VL) in Figure 9 a(ii) remains stable at 304.1 V. As long as fault period, although nominal of average source current (I_s) in Figure 9 a(iv) drops to 3.804 A, combination of PV and BES is able to generate power, store excess energy of PV, and inject current into load through shunt active filter so that average load current (IL) in Figure 9 a(v) remains as 8.421 A. Figure 9 b(i) presents on UPQC-BES supplied by wind at t=0.2 s to t=0.5 s average source voltage (Vs) drops 100% to 0.3828 V. During the disturbance, wind is able to generate power to UPQC DC link and injecting full average compensation voltage (V_C) in Figure 9 b(iii) through injection transformer on series active filter so that average load voltage (V_L) in Figure 9 b(ii) remains stable at 306.4 V. During fault period, although nominal of average source current (Is) falls to 3.420 A, combination of wind and BES is able to generate power, store excess energy of wind, and inject current into load through shunt active filter so that average load current (I₁) in Figure 9 b(v) remains as 8.569 A. Figure 9 c(i) indicates on UPQC-BES supplied by PV-Wind Hybrid at t=0.2 s to t=0.5 s average source voltage (V_s) drops 100% to 0.4175 V. During the disturbance, PV-wind hybrid is able to generate power to UPQC DC link and injecting full average compensation voltage (V_c) in Figure 9 c(iii) through injection transformer on series active filter so that average load voltage (V_L) in Figure 9 b(ii) remains stable at 305.9 V. As long as disturbance period, although nominal of average source current (Is) falls to 3.640 A, combination of PV-wind hybrid and BES is able to generate power, store excess energy of wind, and inject current into load through shunt active filter so that average load current (I_L) in Figure 9 c(v) remains as 8.488 A.

Figure 10 shows spectra of load voltage harmonics on phase A of UPQC-BES system supplied by three RE sources using FLC in scenario 6. Figure 11 shows performance of average THD of load voltage and source current on UPQC-BES system supplied by three RE sources. Figure 11(a) shows that in scenario 1 to 5, the implementation of FLC on UPQC-BES system supplied by three RE sources is able to obtain average THD of load voltage slightly better than PI controller and both method have already met the limit in IEEE 519. Further under scenario 6, FLC applied on UPQC-BES system supplied by three RE sources gives significantly better result of average THD of load voltage than PI controller. In six disturbance scenarios, both PI controller and FLC applied on UPQC-BES system supplied by three RE sources, PV is able to obtain the highest average THD of load voltages. Figure 11(b) shows that in disturbance scenario 1 to 5, implementation of FLC on UPQC-BES system supplied by three RE sources is able to obtain average THD of source current slightly better than PI controller. Furthermore under scenario 6, FLC applied on UPQC-BES system supplied by three RE sources is able to obtain average THD of source current slightly better than PI controller. Furthermore under scenario 6, FLC applied on UPQC-BES system supplied by three RE sources is able to obtain average THD of source current slightly better than PI controller. Furthermore under scenario 6, FLC applied on UPQC-BES system supplied by three RE sources is able to obtain average THD of source current than PI controller. Both PI controller and FLC on UPQC-BES system supplied by three RE sources in six disturbance scenarios, PV is able to obtain the highest average THD of source current.



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Figure 9. UPQC-BES system performance using FLC in scenario 6 (Inter-NL): (a) UPQC-BES + PV; (b) UPQC-BES + Wind; (c) UPQC-BES + PV-Wind Hybrid







(a) Average load voltage harmonics



(b) Average source current harmonics

Figure 11. Performance of UPQC-BES supplied by three RE sources using PI and FLC

4. CONCLUSION

Comparative performance analysis of UPQC-BES system supplied by three RE sources i.e. PV, wind, and PV-wind hybrid respectively using PI controller and FLC have been discussed. In disturbance scenario 1 to 5, implementation of FLC on UPQC-BES system supplied by three RE sources is able to obtain average THD of load voltage slightly better than PI and both methods have already met the limit in IEEE 519. Under scenario 6, FLC applied on UPQC-BES system supplied by three RE sources gives significantly better result average THD of load voltage than PI. In six disturbance scenarios, both PI and FLC applied on UPQC-BES system supplied by three RE sources is able to obtain the highest average THD of load voltage. In interference scenario 1 to 5, FLC method on UPQC-BES system supplied by three RE sources is able to obtain average THD of source current slightly better than PI. Furthermore under scenario 6, FLC applied on UPQC-BES system supplied by three RE sources gives significantly better result of average THD of source current slightly better than PI. Furthermore under scenario 6, FLC applied on UPQC-BES system supplied by three RE sources gives significantly better result of average THD of source current slightly better than PI. Furthermore under scenario 6, FLC applied on UPQC-BES system supplied by three RE sources gives significantly better result of average THD of source current than PI. Both PI and FLC on UPQC-BES system supplied by three RE sources in six scenarios, PV is able to obtain the highest average THD of source current.

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APPENDIX

Three phase grid: RMS voltage 380 volt (L-L), 50 Hz, line impedance: $R_s=0.1$ Ohm $L_s=15$ mH; series and shunt active filter: series inductance $L_{se}=0.015$ mH; shunt inductance $L_{sh}=15$ mH; injection transformers: rating 10 kVA, 50 Hz, turn ratio $(N_1/N_2)=1:1$; non linear load: resistance $R_L=60$ ohm, inductance $L_L=0.15$ mH, load impedance $R_c=0.4$ ohm and $L_c=15$ mH; unbalance load: resistance $R_1=24$ ohm, $R_2=12$ ohm, and $R_3=6$ ohm, capacitance $C_1, C_2, C_3=2200 \ \mu\text{F}$; DC-link: voltage $V_{DC}=650$ volt and capacitance $C_{DC}=3000 \ \mu\text{F}$; battery energe storage: type=nickel metal hybrid, DC voltage=650 volt, rated capacity= 200 Ah, initial SOC=100%, inductance $L_1=6$ mH, capacitance $C_1=200 \ \mu\text{F}$; photovoltaic: active power= 0.6 kW temperature=25° C, irradiance=1000 W/m²; PMSG wind turbine active power=0.6 kW, voltage= 380 volt, 50 Hz, wind speed=5 m/s, picth angle=2; PI controller: $K_p=0.2$, $K_i=1.5$; fuzzy model: method= mamdani, composition=max-min; input membership function: error (V_{dc})=trapmf, trimf delta error (ΔV_{dc})= trapmf, trimf; output membership function: \overline{p}_{loss} =trapmf,trimf.

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Lampiran 2.7 Revisi kelima makalah

Matlab/simulink simulation of unified power quality conditioner-battery energy storage system supplied by PV-wind hybrid using fuzzy logic controller

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ABSTRACT

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This paper presents performance analysis of Unified Power Quality Conditioner-Battery Energy Storage (UPQC-BES) system supplied by Photovoltaic (PV)-Wind Hybrid connected to three phase three wire (3P3W) of 380 volt (L-L) and 50 hertz distribution system. The performance of supply system is compared with two renewable energy (RE) sources i.e. PV and Wind, respectively. Fuzzy Logic Controller (FLC) is implemented to maintain DC voltage across the capacitor under disturbance scenarios of source and load as well as to compare the results with Proportional Intergral (PI) controller. There are six scenarios of disturbance i.e. (1) non-linear load (NL), (2) unbalance and nonlinear load (Unba-NL), (3) distortion supply and non-linear load (Dis-NL), (4) sag and non-linear load (Sag-NL), (5) swell and non-linear load (Swell-NL), and (6) interruption and non-linear load (Inter-NL). In disturbance scenario 1 to 5, implementation of FLC on UPQC-BES system supplied by three RE sources is able to obtain average THD of load voltage/source current slightly better than PI. Furthermore under scenario 6, FLC applied on UPQC-BES system supplied by three RE sources gives significantly better result of average THD of load voltage/source current than PI. This research is simulated using Matlab/Simulink.

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1. INTRODUCTION

PV and wind are the most RE distributed generations (DGs) because they are able to convert sunlight and wind into power. PV and solar are the potential DGs sources since it only need sunlight to generate electricity, where the resources are available in abundance, free and relatively clean. Indonesia has enormous energy potential from the sun because it lies on the equator. Almost all areas of Indonesia get sunlight about 10 to 12 hours per day, with an average intensity of irradiation of 4.5 kWh/m² or equivalent to 112.000 GW. The potential of wind energy in Indonesia generally has a speed between 4 to 5 m/s and classified as medium scale with potential capacity of 10 to 100 kW. The weakness of PV and wind turbine besides able to generate power, they also produces a number voltage and current harmonics resulted by presence of several types of PV and wind turbine devices and power converters as well as to increase a number of non-linear loads connected to the grid, so finally resulting in the decrease in power quality.

In order to overcome and improve power quality due to presence of non-linear loads and integration of PV and wind turbine to grid, UPQC is a proposed. UPQC serves to compensate for source voltage quality problemsi.e. sag, swell unbalance, flicker, harmonics, and load current quality problems i.e. harmonics,

unbalance, reactive currents, and neutral current. B. Han et. al and Vinod Khadkikar have investigated UPQC as one part of active power filter consisting of shunt and series active filters connected in parallel and serves as superior controller to overcome a number of power quality problems simultaneously. Series component has been responsible for reducing a number of interference on source side i.e. voltage sag/swell, flicker, unbalanced voltage, and harmonics. Shunt component has been responsible for addressing a current quality problems i.e. low power factor, load current harmonics, and unbalanced load. [1, 2]. UPQC based on RE has been investigated by some researchers. There are two methods used to overcome this problem i.e. using conventional and artificial intelligence. Shafiuzzaman K.K., et.al have proposed system includes a series inverter, shunt inverter, and a DG connected to a DC link through a rectifier using PI. The system was capable of increase source voltage quality i.e. sag and interruption and load current quality, as well as transfer of active power on/off grid mode [3]. The influence of DG on UPQC performance in reducing sag under conditions of some phase to ground faults to using DSTATCOM has been implemented by Norshafinash S., et.al. The DG was effective enough to help UPQC to improve sag [4]. It was connected in series with load resulting better sag mitigation compared to system without DG. Implementation of UPQC using UVTG method with PI to reduce sag, swell, voltage/current harmonics has been doneby S. N. Gohil, et.al. Simulation of voltage distortion was made by adding 5th and 7th harmonics at fundamental source voltage, resulting in a reduction of THD source current and THD load voltage [5].

UPQC supplied by PV panels using boost converter, PI, MPPT P and O, and p-q theory has been proposed by Yahia Bouzelata at.al [6]. The system was capable of compensate reactive power and reduce source current/load voltage harmonics, but did not discuss migitation of sag and interuption caused by PV penetration. Power quality enhancement of sag and source voltage harmonics on grid using UPQC supplied by PV array connected to DC link using PI compared with FLC has been done by Ramalengswara Rao, et.al. Combination of UPQC and PV using FLC can improve source voltage THD better than PI [7]. Amirullah et.al have researched a method for balancing current and line voltage, as a result of DGs of a single phase PV generator unit in randomly installed at homes through on a three phase four wire 220 kV and 50 Hz distribution line using BES and three of single phase bidirectional inverter. Both devices was capable of reduce unbalanced line current/voltage, but both of them were also capable of increase current/voltage harmonics on PCC bus [8]. Power quality migitation of UPQC on microgrid supplied by PV and wind turbine has been implemented by K S Srikanth et. al. It resulted that PI and FLC was able to improve power quality and reduce distortion in output power [9]. The UPQC-wind turbine to provide active power to overcome low sag and interruption voltage to grid has been investigated by H.Toodeji, et.al. The model was used VSC as a rectifier on generator output and controlled so that maximum power desired can be generated by different speed wind turbines using PI [10]. The UPQC-wind turbine connected to UPQC DC link was implemented by M. Hosseinpour, et al. The proposed combination using PI was capable of compensate swell, interruption voltage, and reactive power both on on/off grid [11]. R.Bhavani, et, al have researched on UPOC controlled by FLC to improve power quality in a DFIG wind turbine connected grid. FLC can improve power quality i.e. sag voltage and load current harmonics better than PI [12]. Power quality enhancement on wind turbine and BES with PI connected grid on PCC bus using UPQC has been implemented by S.RajeshRajan, et al. BES was installed to maintain and stabilize active power supply under different wind speed [13].

This research will analyze UPQC-BES performance supplied by PV-wind hybrid connected to 3P3W of 380 volt (L-L) and 50 hertz distribution system. The performance of supply system is compared with two RE sources i.e. PV and Wind, respectively. BES serves to store excess energy produced by three RE sources and distribute it to load if necessary, to prevent interruption voltage, and to adjust charging and discharging of energy in battery. BES is also expected to store excess power produced by three RE combinations and use it as backup power. FLC is proposed and compared with PI to control variable of DC voltage and DC reference voltage input to generate reference current source in current hysteresis controller on shunt active filter. DC voltage controller in shunt active filter and series active filter is used to migitate power quality of load voltage and source current.Performance of two controllers are used to determine load voltage, source current, load voltage THD, and source current THD based on IEEE 519. This paper is presented as follow. Section 2 describes proposed method, model of UPQC-BES system supplied by three RE sources i.e. PV, wind, and PV-wind hybrid, simulation parameters, PV and PMSG wind turbine model, series and shunt active filter, as well as application of PI and FLC method for proposed model. Section 3 shows results and analysis about performance of THD analysis on the proposed model of three RE sources connected to DC link of UPQC-BES system using PI and FLC. In this section, six disturbance scenarios are presented and the results are verified with Matlab/Simulink. Finally, this paper in concluded in Section 4.

2. RESEARCH METHOD

2.1. Proposed method

Figure 1 shows proposed model in this research. The RE sources based DGs used i.e. PV, Wind Turbine, and PV-Wind Turbine Hybrid connected to 3P3W distribution system with 380 volt (L-L) and 50 Hz frequency, through UPQC-BES system. PV array produce power under fixed temperature and radiation as well as connect to UPQC-DC link through a DC/DC boost converter. The maximum power point tracking (MPPT) method with Pertub and Observer (P and O) algorithms helps PV produce maximum power and generate output voltage, as the input voltage for DC/DC boost converter. The converter serves to adjust dutycycle value and output voltage of PV as its input voltage to produce an output voltage corresponding to UPQC DC link voltage. Wind turbine type used is a permanent magnetic synchronous generator (PMSG) with variable speed and fixed voltage which generating power and is connected to UPQC DC link circuit through AC/DC bridge rectifier. The rectifier helps to change AC PSMG stator output voltage to DC voltage through LC circuit that serves to filter and smooth it before connected to UPQC-DC link.BES connected to the UPQC-DC link circuit serves as energy storage and is expected to overcome interruption voltage and overall help UPQC performance to improve voltage and current quality on source and load bus. Simulation parameters proposed in this study is shown in Appendix Section. Power quality analysis is performed on PV, Wind, PV-Wind Hybrid respectively, connected to 3P3W system through UPQC DC-link (on-grid) using BES circuit. Single phase circuit breakers (CBs) are used to connect and disconnect PV, Wind, and Hybrid PV-Wind respectively with UPOC DC-link.

There are six disturbance scenarios i.e. (1) NL, (2) Unba-NL, (3) Dis-NL, (4) Sag-NL, (5) Swell-NL, and (6) Inter-NL. In scenario 1, the model is connected a non-linear load with R_L and L_L of 60 Ohm and 0.15 mH respectively. In scenario 2, the model is connected to non-linear load and during 0.3 s since t=0.2 s to t=0.5 s connected to unbalance three phase load with R1, R2, R3 as 6 Ohm, 12 Ohm, 24 Ohm respectively, and value of C1, C2, C3 as 2200 µF. In scenario 3, the model is connected to non-linear load and source voltage generating 5th and 7th harmonic components with individual harmonic distortion values of 5% and 2% respectively. In scenario 4, the model is connected to non-linear load and source experiences a sag voltage disturbance of 50% for 0.3 s between t=0.2 s to t=0.5 s. In scenario 5, the model is connected to a non-linear load and source experiences a swell voltage disturbance of 50% for 0.3 s between t=0.2 s to t=0.5 s. In scenario 6, the model is connected to non-linear load and source experiences an interruption voltage interference of 100% for 0.3 s between t=0.2 s to t=0.5 s. FLC is used as a DC voltage control in a shunt active filter to improve the power quality of the load voltage and current source and compare it with PI controller. Each disturbance scenario uses a PI controller and FLC so that the total of 12 disturbances. The result analysis of research was carried out i.e. (1) voltage and current on source or poin common coupling (PCC) bus, (2) voltage and current on load bus, (3) harmonic voltage and harmonic current on source bus and (4) harmonic voltage and harmonic current on load bus. The final phase is to compare performance of UPQC-BES system on-grid supplied by PV, Wind, PV-Wind Hybrid respectively using two controllers to improve power quality of load voltage and source current under six disturbance conditions.



Figure 1. Proposed model of UPQC-BES system supplied by PV, Wind, and PV-Wind Hybrid

2.2. Photovoltaic model

Figure 2 shows the equivalent circuit and V-I characteristic of a solar panel. A solar panel is composed of several PV cells that have series, parallel, or series-parallel external connections [14].



Figure 2. Equivalent circuit and V-I characteristic of solar panel

The V-I characteristic of a solar panel is showed in (1):

$$I = I_{PV} - I_o \left[\exp\left(\frac{V + R_s I}{aV_t}\right) - 1 \right] - \frac{V + R_s I}{R_p}$$
(1)

where I_{PV} is the photovoltaic current, I_o is saturated reverse current, 'a' is the ideal diode constant, $V_t = N_S K T q^{-1}$ is the thermal voltage, N_S is the number of series cells, q is the electron charge, K is the Boltzmann constant, T is the temperature of p–n junction, R_S and R_P are series and parallel equivalent resistance of the solar panels. I_{PV} has a linear relation with light intensity and also varies with temperature variations. I_o is dependent on temperature variations. The values of I_{pv} and I_o are calculated as following (2) and (3):

$$I_{PV} = (I_{PV,n} + K_1 \Delta T) \frac{G}{G_n} I$$
⁽²⁾

$$I_o = \frac{I_{SC,n} + K_I \Delta T}{\exp(V_{OC,n} + K_V \Delta T) / aV_t - 1}$$
(3)

In which $I_{PV,n}$, $I_{SC,n}$ and $V_{OC,n}$ are photovoltaic current, short circuit current and open circuit voltage in standard conditions ($T_n=25$ C and $G_n=1000$ Wm⁻²) respectively. K_I is the coefficient of short circuit current to temperature, $\Delta T=T-T_n$ is the temperature deviation from standard temperature, G is the light intensity and K_I is the ratio coefficient of open circuit voltage to temperature. Open circuit voltage, short circuit current and voltage-current corresponding to the maximum power are three important points of I-V characteristic of solar panel. These points are changed by variations of atmospheric conditions. By using (4) and (5) which are derived from PV model equations, short circuit current and open circuit voltage can be calculated in different atmospheric conditions.

$$I_{SC} = (I_{SC} + K_1 \Delta T) \frac{G}{G_n}$$
⁽⁴⁾

$$V_{OC} = V_{OC} + K_V \Delta T \tag{5}$$

2.3. PMSG wind turbine

Wind turbine is one of part of an integrated system, which can be divided into two types i.e. fixed and variable speed wind turbines. In fixed speed type, rotating speed of turbine is fixed and hence, frequency of generated voltage remains constant, so it can be directly connected to the network. In this case, maximum power can not always be extracted by wind. On the other hand, on variable speed, turbine can rotate at different speeds, so maximum power can be generated in each wind speed by MPPT method [10]. The advantage of using a PMSG over a synchronous generator and DFIG machine because it has high efficiency and reliability. Due to the elimination of rotor external excitation, machine size, and cost also decreases, making PMSG to be more controlled easily with feedback control system. PMSG has become an attractive solution on wind generation systems with variable speed wind turbine applications [15]. Figure 3 and 4 shows model of PMSG wind turbine and wind turbin power characteristic curve.



Figure 3. Model of PMSG wind turbine



Figure 4. Wind turbin power characteristic curve

The output power of wind turbine can be expressed using (6), (7), and (8) [11].

$$\lambda = \frac{\omega_r R}{V_{wind}} \tag{6}$$

$$P_M = \frac{1}{2} \rho \pi R^2 C_p V_{wind}^3 \tag{7}$$

$$T_{M} = \frac{P_{M}}{\omega_{r}} = \frac{1}{2} \rho \pi R^{5} C_{p} \frac{\omega_{M}^{3}}{\lambda^{3}}$$

$$\tag{8}$$

Where λ is the speed-tip ratio, V_{wind} is wind speed, R is blade radius, ω_r is rotor speed (rad/sec), ρ is the air density, C_P is the power coefficient, P_M is the output mechanical power, and T_M is output torque of wind turbine. The C_P coefficient is dependent on the pitch angle value, at which rotor blade can rotate along axis and tip-speed ratio λ expressed in (9).

$$C_p = (0.44 - 0.167\beta)\sin\frac{\pi(\lambda - 2)}{(13 - 0.3\beta)}$$
(9)

Where β is a pitch angle blade. In a fixed pitch type, the value of β is set to a fixed value.

2.4. Control of series active filter

The main function of series active filter is as a sensitive load protection against a number of voltage interference at PCC bus. The control strategy algorithm of the source and load voltage in series active filter circuit is shown in Figure 5. It extracts the unit vector templates from the distorted input supply. Furthermore, the templates are expected to be ideal sinusoidal signal with unity amplitude. The distorted supply voltages are measured and divided by peak amplitude of fundamental input voltage V_m give in (10) [6].

$$V_m = \sqrt{\frac{2}{3} \left(V_{sa}^2 + V_{sb}^2 + V_{sc}^2 \right)}$$
(10)

A three phase locked loop (PLL) is used in order to generate a sinusoidal unit vector templates with a phase lagging by the use of sinus function. The reference load voltage signal is determined by multiplying the unit vector templates with the peak amplitude of the fundamental input voltage V_m . The load reference voltage (V_{La}^* , V_{Lb}^* , V_c^*) is then compared against to sensed load voltage (V_{La} , V_{Lb} , V_{Lc}) by a pulse width modulation (PWM) controller used to generate the desired trigger signal on series active filter.



Figure 5. Control strategy of series active filter

2.5. Control of shunt active filter

The main function of shunt active filter is mitigation of power quality problems on the load side. The control methodology in shunt active filter is that the absorbed current from the PCC bus is a balanced positive sequence current including unbalanced sag voltage conditions in the PCC bus or unbalanced conditions or non-linear loads. In order to obtain satisfactory compensation caesed by disturbance due to non-linear load, many algorithms have been used in the literature. This research used instantaneous reactive power theory method "p-q theory". The voltages and currents in Cartesian *abc* coordinates can be transformed to Cartesian $\alpha\beta$ coordinates as expressed in (11) and (12) [16].

$$\begin{bmatrix} v_{\alpha} \\ v_{\beta} \end{bmatrix} = \begin{bmatrix} 1 & -1/2 & -1/2 \\ 1 & \sqrt{3}/2 & -\sqrt{3}/2 \end{bmatrix} \begin{bmatrix} V_{\alpha} \\ V_{b} \\ V_{c} \end{bmatrix}$$
(11)

$$\begin{bmatrix} i_{\alpha} \\ i_{\beta} \end{bmatrix} = \begin{bmatrix} 1 & -1/2 & -1/2 \\ 1 & \sqrt{3}/2 & -\sqrt{3}/2 \end{bmatrix} \begin{bmatrix} i_{La} \\ i_{Lb} \\ i_{Lc} \end{bmatrix}$$
(12)

The computation of the real power (p) and imaginary power (q) is showed in (13). The real power and imaginary are measured instantaneously power and in matrix it is form is given as. The presence of oscillating and average components in instantaneous power is presented in (14) [17].

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$$\begin{bmatrix} p \\ q \end{bmatrix} = \begin{bmatrix} v_{\alpha} & v_{\beta} \\ -v_{\beta} & v_{\alpha} \end{bmatrix} \begin{bmatrix} i_{\alpha} \\ i_{\beta} \end{bmatrix}$$
(13)

$$p = \overline{p} + \widetilde{p} \quad ; q = \overline{q} + \widetilde{q} \tag{14}$$

Where \overline{p} = direct component of real power, \widetilde{p} = fluctuating component of real power, \overline{q} = direct component of imaginary power, \widetilde{q} = fluctuating component of imaginary power. The total imaginary power (q) and the fluctuating component of real power are selected as power references and current references and are utilized through the use of (15) for compensating harmonic and reactive power [18].

$$\begin{bmatrix} i_{c\alpha}^{*} \\ i_{c\beta}^{*} \end{bmatrix} = \frac{1}{v_{\alpha}^{2} + v_{\beta}^{2}} \begin{bmatrix} v_{\alpha} & v_{\beta} \\ v_{\beta} & -v_{\alpha} \end{bmatrix} \begin{bmatrix} -\widetilde{p} + \overline{p}_{loss} \\ -q \end{bmatrix}$$
(15)

The signal \overline{p}_{loss} , is obtained from voltage regulator and is utilized as average real power. It can also be specified as the instantaneous active power which corresponds to the resistive loss and switching loss of the UPQC. The error obtained on comparing the actual DC-link capacitor voltage with the reference value is processed in FLC, engaged by voltage control loop as it minimizes the steady state error of the voltage across the DC link to zero. The compensating currents ($i_{c\alpha}^*$, $i_{c\beta}^*$) as required to meet the power demand of load are shown in (15). These currents are represented in α - β coordinates. The phase current is required to acquire using (16) for compensation. These source phase currents (i_{sa}^* , i_{sb}^* , i_{sc}^*) are represented in a-b-c axis obtained from the compensating current in the α - β coordinates presented in (16) [18]. Figure 6 shows a control of shunt active filter.

$$\begin{bmatrix} i_{s_{\alpha}}^{*} \\ i_{s_{b}}^{*} \\ i_{s_{c}}^{*} \end{bmatrix} = \sqrt{\frac{2}{3}} \begin{bmatrix} 1 & 0 \\ -1/2 & \sqrt{3}/2 \\ -1/2 & -\sqrt{3}/2 \end{bmatrix} \begin{bmatrix} i_{c\alpha}^{*} \\ i_{c\beta}^{*} \end{bmatrix}$$
(16)



Figure 6. Control strategy of shunt active filter

The proposed model of UPQC-BES system supplied by three RE sources is shown in Figure 1. From the figure, we can see that PV is connected to the DC link through a DC-DC boost converter circuit. The PV partially distributes power to the load and the remains is transfered to three phase grid. The load consists of non linear and unbalanced load. The non-linear load is a diode rectifier circuit with the RL load type, while the unbalanced load is a three phase RC load with different R value on each phase. In order to economically efficient, PV must always work in MPP condition. In this research, MPPT method used is P and O algorithm. The model is also applied for UPQC-BES system which is supplied by wind and PV-wind hybrid respectively. In order to operate properly, UPQC-BES system device must have a minimum DC link voltage (V_{dc}). The value of common DC link voltage depends on the nstantaneous energy avialable to UPQC is defined by in (17) [16]:

$$V_{dc} = \frac{2\sqrt{2}V_{LL}}{\sqrt{3}m} \tag{17}$$

where m is modulation index and V_{LL} is the AC grid line voltage of UPQC. Considering that modulation index as 1 and for line to line grid voltage (V_{LL} =380 volt), the V_{dc} is obtained 620, 54 volt and selected as 650 volt.

The input of shunt active filter showed in Figure 5 is DC voltage (V_{dc}) and reference DC voltage (V_{dc}^*), while the output is \bar{p}_{loss} by using PI controller. Then, the \bar{p}_{loss} is as one of input variable to generate the reference source current (I_{sa}^* , I_{sb}^* , and I_{sc}^*). The reference source current output is then compared to source current (I_{sa} , I_{sb} , and I_{sc}) by the current hysteresis control to generate trigger signal in IGBT circuit of shunt active filter. In this research, FLC as DC voltage control algorithm on shunt active filter is proposed and compared with PI controller. The FLC is capable of reduce oscilation and generate quick convergence calculation during disturbances. This method is also used to overcome the weakness of PI controller in determining proportional gain (K_p) and integral gain constant (K_i) which still use trial and error method.

2.6. Fuzzy logic controller

The research is started by determine \overline{p}_{loss} as the input variable to result the reference source current on current hysteresis controller to generate trigger signal on the IGBT shunt active filter of UPQC using PI controller (K_p=0.2 and K_i=1.5). By using the same procedure, \overline{p}_{loss} is also determined by using FLC. The FLC has been widely used in recent industrial process because it has heuristic, simpler, more effective and has multi rule based variables in both linear and non-linear system variations. The main components of FLC are fuzzification, decision making (rulebase, database, reason mechanism) and defuzzification in Figure 7. The output membership function is generated using inference blocks and the basic rules of FLC as shown in Table 1.



The fuzzy rule algorithm collects a number of fuzzy control rules in a particular order. This rule is used to control the system to meet the desired performance requirements and they are designed from a number of intelligent system control knowledge. The fuzzy inference of FLC using Mamdani method related to max-min composition. The fuzzy inference system in FLC consists of three parts: rule base, database, and reasoning mechanism [19]. The FLC method is performed by determining input variables V_{dc} (V_{dc-error}) and delta Vdc ($\Delta V_{dc-error}$), seven linguistic fuzzy sets, operation fuzzy block system (fuzzyfication, fuzzy rule base and defuzzification), $V_{dc-error}$ and $\Delta V_{dc-error}$ during fuzzification process, fuzzy rule base table, crisp value to determine \bar{p}_{loss} in defuzzification phase. The \bar{p}_{loss} is one of input variable to obtain compensating currents (i_{ca}^*, i_{cb}^*) in (16). During fuzzification process, a number of input variables are calculated and converted into linguistic variables based on a subset called membership function. The error Vdc (V_{dc-error}) and delta error Vdc ($\Delta V_{dc-error}$) are proposed input variable system and output variable is \overline{p}_{loss} . To translate these variables, each input and output variable is designed using seven membership functions: Negative Big (NB), Negative Medium (NM), Negative Small (NS), Zero (Z), Positive Small (PS), Positive Medium (PM) and Positive Big (PB). The membership functions of crisp input and output are presented with triangular and trapezoidal membership functions. The value of V_{dc-error} range from -650 to 650, $\Delta V_{dc-error}$ from -650 to 650, and \bar{p}_{lass} from -100 to 100. The input and output MFs are shown in Figure 8.


Figure 8. Membership functions (a) $V_{dc-error}$, (b) $\Delta V_{dc-error}$, and (c) \overline{p}_{lass}

After the V_{dc-error} and Δ V_{dc-error} are obtained, then two input membership functions are converted to linguistic variables and uses them as input functions for FLC. The output membership function is generated using inference blocks and the basic rules of FLC as shown in Table 1. Finally the defuzzification block operates to convert generated \overline{p}_{loss} output from linguistic to numerical variable again. Then it becomes input variable for current hysteresis controller to produce trigger signal on the IGBT circuit of UPQC shunt active filter to reduce source current and load voltage harmonics. While simultaneously, it also improve power quality of 3P3W system under six scenarios due to the integration of three RE sources to UPQC-BES system.

3. RESULTS AND ANALYSIS

The analysis of proposed model is investigated through determination of six disturbance scenarios i.e. (1) NL, (2) Unba-NL, (3) Dis-NL, (4) Sag-NL, (5) Swell-NL, and (6) Inter-NL. Each scenario of UPQC uses PI controller and FLC so total number of disturbance are 12 scenarios.By using Matlab/Simulink, the model is then executed according to the desired scenario to obtain curve of source voltage (V_s), load voltage (V_L), compensation voltage (V_c), source current (V_s), load current (I_L), and DC voltage DC link (V_{dc}). Then, THD value of source voltage, source current, load voltage, and load current in each phase as well as average THD value (Avg THD) are obtained base on the curves. THD in each phase is determined in one cycle started at t = 0.35 s. The results of average of source voltage, source current, load voltage, source current of 3P3W system using UPQC-BES system supplied by three RE sources i.e. PV, wind, and PV-wind hybrid are presented in Table 2, 3, and 4. Next THD in each phase and average THD are showed in Table 5, 6 and 7.

Table 2 shows UPQC-BES system supplied PV connected 3P3W system using PI and FLC, disturbance scenarios 1 to 5 produce an average load voltage above 307 V. While in scenario 6, FLC produces a higher average load voltage of 304.1 V than if using a PIof 286.7 V. If reviewed from average source current with PI, the highest and lowest average source currents are generated by disturbance scenarios

2 and 4 of 28.15 A and 7,246 A. Whereas if using FLC the highest and lowest average source currents are achieved in scenario 2 and 6 of 28.84 A and 3.804 A. Table 3 shows UPQC-BES supplied by wind connected to 3P3W with PI and FLC, scenarios 1 to 5 is able to obtain a stable load voltage above 308 V. The difference is that in scenario 6, PI generates a load voltage of 274.8 V, otherwise if using FLC, load voltage increases to 306.4 V. If reviewed from source current using PI, the highest and lowest average source currents are resulted by scenarios 2 and 4 of 28.28 A and 7.417 A. Rather, if using FLC, the highest and lowest average source currents are achieved in scenario 2 and 6 of 28.82 A and 3,420 A. Table 4 shows UPQC-BES supplied PV-wind hybrid connected 3P3W using PI and FLC, scenarios 1 to 5 produce an average load voltage above 307 V. While in scenario 6, FLC generates an average load voltage 305.9 V higher than if using PI control of 283.9 V. If reviewed from average source current with PI, the highest and lowest average source currents are resulted by scenarios 2 and 4 of 28.21 A and 6,773 A. Otherwise if using FLC the highest and lowest average source currents are achieved in scenario 2 and 6 of 28.82 A and 3.640 A respectively.

Table 2. Voltage and Current of 3P3W System Using UPQC-BES System Supplied by PV

Con	So	urce Vol	tage V _S ((V)		Load Vo	ltage V _L (V)	Se	ource Cu	rrent I _S (.	A)	I	Load Cu	rent I _L (A	<i>I</i>)
Self	Ph A	Ph B	Ph C	Avg	Ph A	Ph B	Ph C	Avg	Ph A	Ph B	Ph C	Avg	Ph A	Ph B	Ph C	Avg
							PI	Controlle	er							
1	309.6	309.6	309.6	309.6	307.6	307.8	307.7	307.7	7.766	7.793	7.759	7.773	8.528	8.529	8.533	8.530
2	307.4	308.0	308.0	307.8	308.3	308.7	308.3	308.4	31.00	24.84	28.73	28.15	22.50	34.12	34.52	30.38
3	309.6	309.6	309.6	309.6	313,8	314.3	317.4	317.4	7.897	7.919	7.867	7.895	8.748	8.704	8.785	8.746
4	154.5	154.5	154.5	154.5	307.1	307.3	307.3	307.2	7.235	7.276	7.226	7.246	8.509	8.514	8.510	8.511
5	464.7	464.7	464.7	464.7	308.6	308.7	308.6	308.6	7.979	7.980	7.964	7.975	8.550	8.553	8.554	8.553
6	0.536	1.385	0.850	0.924	310.2	259.8	290.2	286.7	7.392	12.67	6.045	8.703	8.707	7.747	7.637	8.031
							Fuzzy l	Logic Cor	troller							
1	309.5	309.5	309.5	309.5	307.7	307.9	307.7	307.8	8.420	8.426	8.416	8.421	8.527	8.532	8.531	8.530
2	307.4	307.9	308.0	307.8	308.5	308.7	308.4	308.5	31.66	25.50	29.36	28.84	22.52	34.11	35.52	30.72
3	309.6	309.5	309.5	309.5	313.4	312.9	315.9	314.1	8.516	8.565	8.496	8.526	8.741	8.677	8.736	8.718
4	154.4	154.4	154.4	154.4	307.3	307.3	307.2	307.3	8.563	8.560	8.561	8.561	8.514	8.517	8.512	8.515
5	464.6	464.6	464.6	464.6	308.6	308.8	308.6	308.7	8.396	8.389	8.389	8.392	8.552	8.556	8.554	8.554
6	0.447	0.392	0.380	0.407	314.0	293.4	304.9	304.1	4.024	3.778	3.608	3.804	8.874	8.195	8.193	8.421

Table 3. Voltage and Current of 3P3W System Using UPQC-BES System Supplied by Wind

C	So	urce Vol	tage Vs (V)	L	oad Volt	age V _L (V	V)	Se	ource Cu	rrent Is (A	A)		Load Curr	ent I _L (A)	
SCII	Ph A	Ph B	Ph C	Avg	Ph A	Ph B	Ph C	Avg	Ph A	Ph B	Ph C	Avg	Ph A	Ph B	Ph C	Avg
								PI Cont	roller							
1	309.5	309.6	309.6	309.6	308.6	308.6	308.2	308.5	7.863	7.875	7.840	7.869	8.554	8.553	8.546	8.551
2	307.4	308.0	308.0	308.0	308.9	309.2	308.7	308.9	31.07	24.97	28.81	28.28	22.55	34.17	34.57	30.43
3	309.6	309.5	309.6	309.6	312.9	312.9	315.4	313.8	7.993	8.015	7.947	7.985	8.817	8.682	8.741	8.747
4	154.5	154.5	154.5	154.5	308.0	308.1	307.8	307.9	7.428	7.455	7.368	7.417	8.527	8.535	8.532	8.531
5	464.7	464.7	464.7	464.7	309.3	309.3	309.0	309.2	8.015	8.020	8.002	8.012	8.564	8.573	8.568	8.568
6	1.256	1.022	0.592	0.957	234.0	316.4	274.0	274.8	11.27	9.866	7.028	9.388	5.958	8.697	8.204	7.619
							Fuz	zy Logic	Controll	er						
1	309.5	309.5	309.5	309.5	308.5	308.6	308.3	308.5	8.418	8.410	8.414	8.414	8.545	8.552	8.549	8.549
2	307.4	307.9	308.0	307.8	309.0	309.3	308.9	309.1	31.64	25.47	29.34	28.82	22.56	34.18	34.59	30.44
3	309.5	309.5	309.5	309.5	313.2	313.7	314.1	313.7	8.519	8.531	8.531	8.527	8.713	8.714	8.718	8.715
4	154.4	154.4	154.4	154.4	308.0	308.1	307.7	307.9	8.557	8.539	8.561	8.552	8.528	8.541	8.525	8.531
5	464.6	464.7	464.7	464.7	309.2	309.3	309.2	309.2	8.391	8.385	8.388	8.388	8.565	8.570	8.567	8.567
6	0.357	0.396	0.397	0.383	303.7	300.0	315.3	306.4	3.358	3.464	3.542	3.420	8.557	8.418	8.731	8.569

Table 4. Voltage and Current of 3P3W System Using UPQC-BES System Supplied PV-Wind Hybrid

Son	So	Source Voltage $V_S(V)$ Load Voltage $V_L(V)$ Source Current $I_S(A)$								A)	I	load Curi	rent I _L (A	.)		
SCII	Ph A	Ph B	Ph C	Avg	Ph A	Ph B	Ph C	Avg	Ph A	Ph B	Ph C	Avg	Ph A	Ph B	Ph C	Avg
							PI	Controll	er							
1	309.6	309.6	309.6	309.6	307.8	308.0	307.7	307.8	7.790	7.802	7.770	7.787	8.527	8.537	8.533	8.533
2	307.4	308.0	308.0	307.8	308.4	308.8	308.4	308.6	31.02	24.87	28.74	28.21	22.52	34.13	34.53	31.40
3	309.6	309.5	309.6	309.6	314.0	315.5	316.9	315.5	7.942	7.939	7.918	7.933	8.739	8.750	8.783	8.757
4	154.5	154.5	154.5	154.5	307.3	307.4	307.2	307.3	7.289	7.309	7.251	7.283	8.513	8.516	8.515	8.515
5	464.7	464.7	464.7	464.7	308.7	308.9	308.7	308.8	7.985	7.985	7.975	7.982	8.552	8.558	8.558	8.556
6	1.048	0.825	0.845	0.906	247.5	300.7	303.7	283.9	5.119	5.927	9.271	6.773	7.016	7.893	8.793	7.867
							Fuzzy I	logic Con	ntroller							
1	309.5	309.5	309.5	309.5	307.8	308.0	307.7	307.8	8.419	8.418	8.409	8.413	8.529	8.539	8.533	8.534
2	307.4	307.9	308.0	307.8	308.7	308.7	308.9	308.8	31.66	25.47	29.32	28.82	22.54	34.13	34.56	30.41
3	309.5	309.5	309.5	309.5	314.4	315.5	316.6	315.5	8.581	8.593	8.568	8.581	8.761	8.722	8.761	8.748
4	154.4	154.4	154.4	154.4	307.3	307.5	307.3	307.4	8.566	8.572	8.563	8.567	8.511	8.520	8.519	8.517
5	464.6	464.6	464.6	464.6	308.8	308.8	308.7	308.8	8.391	8.394	8.396	8.394	22.33	22.35	22.36	22.35
6	0.412	0.403	0.402	0.418	311.6	295.7	310.4	305.9	3.774	3.544	3.593	3.640	8.855	8.321	8.288	8.488

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		Ta	ble 5.	Harm	onics	of 3P3	W Sys	stem U	sing UF	QC-BE	ES Syste	em Supp	olied b	y PV		
C	Sou	rce Volta	ge THD ((%)	Lo	ad Voltag	ge THD ((%)	Se	ource Curr	ent THD (%)		Load Cu	rrent (%)	
Scii	Ph A	Ph B	Ph C	Avg	Ph A	Ph B	Ph C	Avg	Ph A	Ph B	Ph C	Avg	Ph A	Ph B	Ph C	Avg
								PI Co	ntroller							
1	2.35	2.36	2.32	2.34	2.48	2.50	2.46	2.48	12.89	12.72	12.92	12.84	22.32	22.34	22.32	22.33
2	2.29	2.20	2.24	2.24	2.43	2.23	2.37	2.34	2.660	2.330	2.240	2.410	5.230	2.070	2.660	3.320
3	5.84	5.86	5.94	5.88	6.36	5.90	6.58	6.28	12.75	12.64	13.06	12.82	21.92	22.16	22.33	22.14
4	4.69	4.75	4.81	4.75	2.46	2.48	2.53	2.49	14.26	13.96	14.16	14.13	22.28	22.31	22.28	22.29
5	1.56	1.53	1.55	1.55	2.47	2.43	2.45	2.45	12.51	12.36	12.44	12.44	22.34	22.32	22.32	22.33
6	NA	NA	NA	NA	32.11	15.09	28.54	25.25	270.90	145.89	275.67	230.82	47.70	34.58	36.29	39.53
							F	uzzy Log	ic Controll	ler						
1	2.35	2.33	2.35	2.34	2.48	2.46	2.49	2.47	11.83	11.82	11.84	11.83	22.33	22.32	22.33	22.33
2	2.25	2.27	2.20	2.24	2.39	2.41	2.34	2.38	2.620	2.400	2.220	2.413	5.230	2.100	2.640	3.323
3	5.83	5.88	5.93	5.88	6.23	5.93	6.69	6.28	11.83	11.90	12.14	11.96	21.84	22.34	22.53	22.24
4	4.71	4.76	4.79	4.75	2.46	2.48	2.50	2.48	11.91	11.88	11.86	11.89	22.27	22.32	22.32	22.31
5	1.55	1.54	1.54	1.54	2.45	2.44	2.46	2.45	11.90	11.84	11.85	11.86	22.36	22.33	22.35	22.35
6	NA	NA	NA	NA	13.05	6.60	11.15	10.27	30.61	34.72	31.57	32.30	24.25	24.25	24.71	24.40

Table 6. Harmonics of 3P3W System Using UPQC-BES System Supplied by Wind

Con	Sour	ce Volta	ge THD	(%)	Lo	ad Volta	ge THD ((%)	Sc	ource Curr	ent THD (9	%)		Load Cu	rrent (%)	
SCII	Ph A	Ph B	Ph C	Avg	Ph A	Ph B	Ph C	Avg	Ph A	Ph B	Ph C	Avg	Ph A	Ph B	Ph C	Avg
								PI Cor	ntroller							
1	1.88	1.87	1.94	1.89	1.99	1.97	2.05	2.00	12.63	12.37	12.70	12.57	12.30	12.30	12.34	12.31
2	1.83	1.76	1.82	1.80	1.92	1.85	1.93	1.90	2.460	2.070	2.200	2.240	5.260	2.070	2.690	3.340
3	5.67	5.71	5.77	5.72	6.00	6.83	6.02	6.28	12.48	12.26	12.66	12.47	22.01	22.12	22.08	22.07
4	3.76	3.86	3.86	1.83	1.97	2.02	2.03	2.01	13.59	13.17	13.51	13.42	22.29	22.31	22.30	22.30
5	1.26	1.24	1.29	1.26	1.99	1.97	2.05	2.00	12.31	12.20	12.31	12.27	22.36	22.33	22.37	22.35
6	NA	NA	NA	NA	14.09	35.59	34.73	28.14	157.76	139.01	266.07	186.95	37.60	34.39	46.97	39.65
							Fι	ızzy Logi	c Controll	er						
1	1.89	1.88	1.93	1.90	1.99	1.98	2.04	2.00	11.71	11.72	11.77	11.73	22.34	22.31	22.32	22.32
2	1.85	1.79	1.78	1.81	1.95	1.87	1.88	1.90	2.43	2.11	2.12	2.220	5.240	2.070	2.700	3.240
3	5.67	5.71	5.78	5.72	5.99	6.39	6.13	6.17	11.72	11.62	11.90	11.75	22.08	21.94	22.47	22.16
4	3.79	3.81	3.86	3.82	1.97	1.99	2.03	1.99	11.72	11.69	11.74	11.72	22.28	22.30	22.35	22.31
5	1.27	1.24	1.28	1.26	2.00	1.96	2.04	2.00	11.66	11.76	11.76	11.73	22.31	22.33	22.35	22.33
6	NA	NA	NA	NA	7.59	6.44	10.95	8.33	27.33	28.27	26.39	27.33	25.39	23.65	24.31	24.45

Table 7. Harmonics of 3P3W System Using UPQC-BES System Supplied by PV-Wind Hybrid

								-	-		-					
Son	Sour	rce Voltag	ge THD	(%)	Loa	d Voltag	e THD (9	%)	Sc	ource Curre	ent THD (%)		Load Cu	rrent (%)	
Self	Ph A	Ph B	Ph C	Avg	Ph A	Ph B	Ph C	Avg	Ph A	Ph B	Ph C	Avg	Ph A	Ph B	Ph C	Avg
								PI Co	ntroller							
1	2.25	2.19	2.29	2.24	2.37	2.31	2.42	3.37	12.85	12.62	12.74	12.74	22.33	22.31	22.34	22.33
2	2.18	2.08	2.15	2.13	2.30	2.19	2.18	2.22	2.630	2.300	2.290	2.407	5.230	2.070	2.670	3.323
3	5.81	5.82	5.89	5.84	6.12	5.88	6.75	6.25	12.71	12.63	12.98	12.77	22.05	22.13	22.54	22.24
4	4.53	4.48	4.51	4.51	2.37	2.35	2.37	2.36	14.16	13.50	13.99	13.88	22.27	22.30	22.28	22.28
5	1.49	1.46	1.51	1.49	2.37	2.31	2.40	2.36	12.43	12.29	12.41	12.38	22.34	22.32	22.33	22.33
6	NA	NA	NA	NA	18.61	36.38	28.42	27.8	387.71	330.34	189.29	302.45	36.73	38.51	36.83	37.36
							Fuz	zy Log	ic Control	ler						
1	2.25	2.23	2.25	2.24	2.37	2.35	2.39	2.37	11.85	11.74	11.84	11.81	22.32	22.31	22.33	22.32
2	2.23	2.15	2.05	2.14	2.37	2.26	2.17	2.26	2.520	2.410	2.140	2.446	5.230	2.070	2.690	3.330
3	5.80	5.83	5.90	5.84	6.57	5.26	7.06	6.29	11.83	11.78	12.24	11.95	22.15	22.23	22.95	22.44
4	4.53	4.52	4.54	4.86	2.36	2.35	2.35	2.35	11.79	11.74	11.84	11.79	22.29	22.30	22.29	22.29
5	1.48	1.46	1.51	1.48	2.35	2.32	2.40	2.35	11.78	11.81	11.81	11.80	22.33	22.35	22.36	22.35
6	NA	NA	NA	NA	10.30	4.90	10.25	8.48	27.44	29.52	28.63	28.53	23.20	23.97	24.65	23.94

Table 5 shows that average THD of load voltage (V_L) of UPQC-BES system supplied by PV in 3P3W system for scenarios 1 to 5 using PI control is within limits in IEEE 519. The highest and lowest average THD load voltages are achieved under scenario 6 and 2 as 25.25% and 2.34% respectively. PI controller is also able to mitigation average THD source voltage in scenario 6 from not accessible (NA) to 25.25% on the load side. The highest and lowest average THD of source current are achieved in scenario 6 and 2 as 230.82% and 2.41%. Table 5 also indicates that average THD of load voltage of UPQC system supplied by PV with BES using FLC in scenarios 1 to 5, has fulfilled limits in IEEE 519. The highest and lowest average THD of load voltage are achieved under scenario 6 and 2 of 10.27% and 2.38%. The use of FLC method is also able to reduce average THD on source voltage in scenario 6 from NA to 10.27% on load side. The highest and lowest average THD of source current are achieved in scenario 6 and 2 of 32.30% and 2.413%.

Table 6 shows that average THD of load voltage of UPQC-BES system supplied by wind in 3P3W system for interference scenarios 1 to 5 using PI is within limits prescribed in IEEE 519. The highest and lowest average THD load voltages is achieved under scenario 6 and scenario 2 as 28.14% and 1.90% respectively. PI controller is also able to reduce average THD source voltage in scenario 6 from NA to 28.14% on the load side. The highest and lowest average THD of source current are achieved in scenario 6 and 2 as 186.95% and 2.24% respectively. Table 6 also shows that average THD of load voltage of UPQC-BES supplied by wind using FLC in scenarios 1 to 5, has fulfilled limits prescribed in IEEE 519. The highest and lowest average THD of load voltage are achieved under scenario 6 and 4 of 8.33% and 1.90%. FLC method is also able to reduce average THD on source voltage in scenario 6 from NA to 7.33% on load side. The highest and lowest average THD source current are achieved in scenario 6 and 2 of 27.33% and 2.22%.

Table 7 shows that average THD of load voltage (V_L) of UPQC-BES system supplied by PV-wind hybrid in 3P3W system for scenarios 1 to 5 using PI is within limits in IEEE 519. The highest and lowest average THD load voltages are achieved under scenario 6 and 2 as 27.8% and 2.22% respectively. PI is also able to mitigate average THD source voltage in scenario 6 from NA to 27.8% on load side. The highest and lowest average THD of source current are achieved in scenario 6and 2 as 302.45% and 2.407% respectively. Table 7 also indicates that average THD of load voltage of UPQC-BES system supplied by PV-wind hybrid using FLC for scenarios 1 to 5, has fulfilled limits in IEEE 519. The highest and lowest average THD of load voltage are achieved under scenario 6 and 2 of 8.48% and 2.26%. FLC method is also able to reduce average THD on source voltage in scenario 6 from NA to 8.48% on load side. The highest and lowest average THD of source current are achieved in scenario 5 and 2 of 28.53% and 2.446%. Overall for UPQC-BES systemsystem supplied by three RE sources in scenarios 1 to 5 using PI and FLC is able to improve average THD of source current better on average THD of load current. Figure 9 presents UPQC-BES system performance supplied by three RE sources using FLC in scenario 6.

Figure 9 a(i) shows that in scenario 6, UPQC-BES system supplied by PV at t=0.2 s to t=0.5 s, average source voltage (V_S) falls as 100% to 0.4062 V. During the disturbance, PV is able to generate power to UPQC DC link and injecting full average compensation voltage (V_c) in Figure 9 a(iii) through injection transformer on series active filter so that average load voltage (VL) in Figure 9 a(ii) remains stable at 304.1 V. As long as fault period, although nominal of average source current (I_s) in Figure 9 a(iv) drops to 3.804 A, combination of PV and BES is able to generate power, store excess energy of PV, and inject current into load through shunt active filter so that average load current (IL) in Figure 9 a(v) remains as 8.421 A. Figure 9 b(i) presents on UPQC-BES supplied by wind at t=0.2 s to t=0.5 s average source voltage (Vs) drops 100% to 0.3828 V. During the disturbance, wind is able to generate power to UPQC DC link and injecting full average compensation voltage (V_C) in Figure 9 b(iii) through injection transformer on series active filter so that average load voltage (V_L) in Figure 9 b(ii) remains stable at 306.4 V. During fault period, although nominal of average source current (Is) falls to 3.420 A, combination of wind and BES is able to generate power, store excess energy of wind, and inject current into load through shunt active filter so that average load current (I₁) in Figure 9 b(v) remains as 8.569 A. Figure 9 c(i) indicates on UPQC-BES supplied by PV-Wind Hybrid at t=0.2 s to t=0.5 s average source voltage (V_s) drops 100% to 0.4175 V. During the disturbance, PV-wind hybrid is able to generate power to UPQC DC link and injecting full average compensation voltage (V_c) in Figure 9 c(iii) through injection transformer on series active filter so that average load voltage (V_L) in Figure 9 b(ii) remains stable at 305.9 V. As long as disturbance period, although nominal of average source current (Is) falls to 3.640 A, combination of PV-wind hybrid and BES is able to generate power, store excess energy of wind, and inject current into load through shunt active filter so that average load current (I_L) in Figure 9 c(v) remains as 8.488 A.

Figure 10 shows spectra of load voltage harmonics on phase A of UPQC-BES system supplied by three RE sources using FLC in scenario 6. Figure 11 shows performance of average THD of load voltage and source current on UPQC-BES system supplied by three RE sources. Figure 11(a) shows that in scenario 1 to 5, the implementation of FLC on UPQC-BES system supplied by three RE sources is able to obtain average THD of load voltage slightly better than PI controller and both method have already met the limit in IEEE 519. Further under scenario 6, FLC applied on UPQC-BES system supplied by three RE sources gives significantly better result of average THD of load voltage than PI controller. In six disturbance scenarios, both PI controller and FLC applied on UPQC-BES system supplied by three RE sources, PV is able to obtain the highest average THD of load voltages. Figure 11(b) shows that in disturbance scenario 1 to 5, implementation of FLC on UPQC-BES system supplied by three RE sources is able to obtain average THD of source current slightly better than PI controller. Furthermore under scenario 6, FLC applied on UPQC-BES system supplied by three RE sources is able to obtain average THD of source current slightly better than PI controller. Furthermore under scenario 6, FLC applied on UPQC-BES system supplied by three RE sources is able to obtain average THD of source current slightly better than PI controller. Furthermore under scenario 6, FLC applied on UPQC-BES system supplied by three RE sources is able to obtain average THD of source current than PI controller. Both PI controller and FLC on UPQC-BES system supplied by three RE sources in six disturbance scenarios, PV is able to obtain the highest average THD of source current.



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Figure 9. UPQC-BES system performance using FLC in scenario 6 (Inter-NL): (a) UPQC-BES + PV; (b) UPQC-BES + Wind; (c) UPQC-BES + PV-Wind Hybrid







(a) Average load voltage harmonics



(b) Average source current harmonics

Figure 11. Performance of UPQC-BES supplied by three RE sources using PI and FLC

4. CONCLUSION

Comparative performance analysis of UPQC-BES system supplied by three RE sources i.e. PV, wind, and PV-wind hybrid respectively using PI controller and FLC have been discussed. In disturbance scenario 1 to 5, implementation of FLC on UPQC-BES system supplied by three RE sources is able to obtain average THD of load voltage slightly better than PI and both methods have already met the limit in IEEE 519. Under scenario 6, FLC applied on UPQC-BES system supplied by three RE sources gives significantly better result average THD of load voltage than PI. In six disturbance scenarios, both PI and FLC applied on UPQC-BES system supplied by three RE sources is able to obtain the highest average THD of load voltage. In interference scenario 1 to 5, FLC method on UPQC-BES system supplied by three RE sources is able to obtain average THD of source current slightly better than PI. Furthermore under scenario 6, FLC applied on UPQC-BES system supplied by three RE sources gives significantly better result of average THD of source current slightly better than PI. Furthermore under scenario 6, FLC applied on UPQC-BES system supplied by three RE sources gives significantly better result of average THD of source current slightly better than PI. Furthermore under scenario 6, FLC applied on UPQC-BES system supplied by three RE sources gives significantly better result of average THD of source current than PI. Both PI and FLC on UPQC-BES system supplied by three RE sources in six scenarios, PV is able to obtain the highest average THD of source current.

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APPENDIX

Three phase grid: RMS voltage 380 volt (L-L), 50 Hz, line impedance: $R_s=0.1$ Ohm $L_s=15$ mH; series and shunt active filter: series inductance $L_{se}=0.015$ mH; shunt inductance $L_{sh}=15$ mH; injection transformers: rating 10 kVA, 50 Hz, turn ratio $(N_1/N_2)=1:1$; non linear load: resistance $R_L=60$ ohm, inductance $L_L=0.15$ mH, load impedance $R_c=0.4$ ohm and $L_c=15$ mH; unbalance load: resistance $R_1=24$ ohm, $R_2=12$ ohm, and $R_3=6$ ohm, capacitance $C_1, C_2, C_3=2200 \ \mu\text{F}$; DC-link: voltage $V_{DC}=650$ volt and capacitance $C_{DC}=3000 \ \mu\text{F}$; battery energe storage: type=nickel metal hybrid, DC voltage=650 volt, rated capacity= 200 Ah, initial SOC=100%, inductance $L_1=6$ mH, capacitance $C_1=200 \ \mu\text{F}$; photovoltaic: active power= 0.6 kW temperature=25° C, irradiance=1000 W/m²; PMSG wind turbine active power=0.6 kW, voltage= 380 volt, 50 Hz, wind speed=5 m/s, picth angle=2; PI controller: $K_p=0.2$, $K_i=1.5$; fuzzy model: method= mamdani, composition=max-min; input membership function: error (V_{dc})=trapmf, trimf delta error (ΔV_{dc})= trapmf, trimf; output membership function: \overline{p}_{loss} =trapmf,trimf.

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Lampiran 2.8 Revisi keenam makalah

Matlab/simulink simulation of unified power quality conditioner-battery energy storage system supplied by PV-wind hybrid using fuzzy logic controller

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ABSTRACT

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Keywords: Battery energy storage Photovoltaic Power quality PV-Wind Hybrid Total harmonic distortion UPQC Wind turbine

This paper presents performance analysis of Unified Power Quality Conditioner-Battery Energy Storage (UPQC-BES) system supplied by Photovoltaic (PV)-Wind Hybrid connected to three phase three wire (3P3W) of 380 volt (L-L) and 50 hertz distribution system. The performance of supply system is compared with two renewable energy (RE) sources i.e. PV and Wind, respectively. Fuzzy Logic Controller (FLC) is implemented to maintain DC voltage across the capacitor under disturbance scenarios of source and load as well as to compare the results with Proportional Intergral (PI) controller. There are six scenarios of disturbance i.e. (1) non-linear load (NL), (2) unbalance and nonlinear load (Unba-NL), (3) distortion supply and non-linear load (Dis-NL), (4) sag and non-linear load (Sag-NL), (5) swell and non-linear load (Swell-NL), and (6) interruption and non-linear load (Inter-NL). In disturbance scenario 1 to 5, implementation of FLC on UPQC-BES system supplied by three RE sources is able to obtain average THD of load voltage/source current slightly better than PI. Furthermore under scenario 6, FLC applied on UPQC-BES system supplied by three RE sources gives significantly better result of average THD of load voltage/source current than PI. This research is simulated using Matlab/Simulink.

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1. INTRODUCTION

PV and wind are the most RE distributed generations (DGs) because they are able to convert sunlight and wind into power. PV and solar are the potential DGs sources since it only need sunlight to generate electricity, where the resources are available in abundance, free and relatively clean. Indonesia has enormous energy potential from the sun because it lies on the equator. Almost all areas of Indonesia get sunlight about 10 to 12 hours per day, with an average intensity of irradiation of 4.5 kWh/m² or equivalent to 112.000 GW. The potential of wind energy in Indonesia generally has a speed between 4 to 5 m/s and classified as medium scale with potential capacity of 10 to 100 kW. The weakness of PV and wind turbine besides able to generate power, they also produces a number voltage and current harmonics resulted by presence of several types of PV and wind turbine devices and power converters as well as to increase a number of non-linear loads connected to the grid, so finally resulting in the decrease in power quality.

In order to overcome and improve power quality due to presence of non-linear loads and integration of PV and wind turbine to grid, UPQC is a proposed. UPQC serves to compensate for source voltage quality problemsi.e. sag, swell unbalance, flicker, harmonics, and load current quality problems i.e. harmonics,

unbalance, reactive currents, and neutral current. B. Han et. al and Vinod Khadkikar have investigated UPQC as one part of active power filter consisting of shunt and series active filters connected in parallel and serves as superior controller to overcome a number of power quality problems simultaneously. Series component has been responsible for reducing a number of interference on source side i.e. voltage sag/swell, flicker, unbalanced voltage, and harmonics. Shunt component has been responsible for addressing a current quality problems i.e. low power factor, load current harmonics, and unbalanced load. [1, 2]. UPQC based on RE has been investigated by some researchers. There are two methods used to overcome this problem i.e. using conventional and artificial intelligence. Shafiuzzaman K.K., et.al have proposed system includes a series inverter, shunt inverter, and a DG connected to a DC link through a rectifier using PI. The system was capable of increase source voltage quality i.e. sag and interruption and load current quality, as well as transfer of active power on/off grid mode [3]. The influence of DG on UPQC performance in reducing sag under conditions of some phase to ground faults to using DSTATCOM has been implemented by Norshafinash S., et.al. The DG was effective enough to help UPQC to improve sag [4]. It was connected in series with load resulting better sag mitigation compared to system without DG. Implementation of UPQC using UVTG method with PI to reduce sag, swell, voltage/current harmonics has been doneby S. N. Gohil, et.al. Simulation of voltage distortion was made by adding 5th and 7th harmonics at fundamental source voltage, resulting in a reduction of THD source current and THD load voltage [5].

UPQC supplied by PV panels using boost converter, PI, MPPT P and O, and p-q theory has been proposed by Yahia Bouzelata at.al [6]. The system was capable of compensate reactive power and reduce source current/load voltage harmonics, but did not discuss migitation of sag and interuption caused by PV penetration. Power quality enhancement of sag and source voltage harmonics on grid using UPQC supplied by PV array connected to DC link using PI compared with FLC has been done by Ramalengswara Rao, et.al. Combination of UPQC and PV using FLC can improve source voltage THD better than PI [7]. Amirullah et.al have researched a method for balancing current and line voltage, as a result of DGs of a single phase PV generator unit in randomly installed at homes through on a three phase four wire 220 kV and 50 Hz distribution line using BES and three of single phase bidirectional inverter. Both devices was capable of reduce unbalanced line current/voltage, but both of them were also capable of increase current/voltage harmonics on PCC bus [8]. Power quality migitation of UPQC on microgrid supplied by PV and wind turbine has been implemented by K S Srikanth et. al. It resulted that PI and FLC was able to improve power quality and reduce distortion in output power [9]. The UPQC-wind turbine to provide active power to overcome low sag and interruption voltage to grid has been investigated by H.Toodeji, et.al. The model was used VSC as a rectifier on generator output and controlled so that maximum power desired can be generated by different speed wind turbines using PI [10]. The UPQC-wind turbine connected to UPQC DC link was implemented by M. Hosseinpour, et al. The proposed combination using PI was capable of compensate swell, interruption voltage, and reactive power both on on/off grid [11]. R.Bhavani, et, al have researched on UPOC controlled by FLC to improve power quality in a DFIG wind turbine connected grid. FLC can improve power quality i.e. sag voltage and load current harmonics better than PI [12]. Power quality enhancement on wind turbine and BES with PI connected grid on PCC bus using UPQC has been implemented by S.RajeshRajan, et al. BES was installed to maintain and stabilize active power supply under different wind speed [13].

This research will analyze UPQC-BES performance supplied by PV-wind hybrid connected to 3P3W of 380 volt (L-L) and 50 hertz distribution system. The performance of supply system is compared with two RE sources i.e. PV and Wind, respectively. BES serves to store excess energy produced by three RE sources and distribute it to load if necessary, to prevent interruption voltage, and to adjust charging and discharging of energy in battery. BES is also expected to store excess power produced by three RE combinations and use it as backup power. FLC is proposed and compared with PI to control variable of DC voltage and DC reference voltage input to generate reference current source in current hysteresis controller on shunt active filter. DC voltage controller in shunt active filter and series active filter is used to migitate power quality of load voltage and source current.Performance of two controllers are used to determine load voltage, source current, load voltage THD, and source current THD based on IEEE 519. This paper is presented as follow. Section 2 describes proposed method, model of UPQC-BES system supplied by three RE sources i.e. PV, wind, and PV-wind hybrid, simulation parameters, PV and PMSG wind turbine model, series and shunt active filter, as well as application of PI and FLC method for proposed model. Section 3 shows results and analysis about performance of THD analysis on the proposed model of three RE sources connected to DC link of UPQC-BES system using PI and FLC. In this section, six disturbance scenarios are presented and the results are verified with Matlab/Simulink. Finally, this paper in concluded in Section 4.

2. RESEARCH METHOD

2.1. Proposed method

Figure 1 shows proposed model in this research. The RE sources based DGs used i.e. PV, Wind Turbine, and PV-Wind Turbine Hybrid connected to 3P3W distribution system with 380 volt (L-L) and 50 Hz frequency, through UPQC-BES system. PV array produce power under fixed temperature and radiation as well as connect to UPQC-DC link through a DC/DC boost converter. The maximum power point tracking (MPPT) method with Pertub and Observer (P and O) algorithms helps PV produce maximum power and generate output voltage, as the input voltage for DC/DC boost converter. The converter serves to adjust dutycycle value and output voltage of PV as its input voltage to produce an output voltage corresponding to UPQC DC link voltage. Wind turbine type used is a permanent magnetic synchronous generator (PMSG) with variable speed and fixed voltage which generating power and is connected to UPQC DC link circuit through AC/DC bridge rectifier. The rectifier helps to change AC PSMG stator output voltage to DC voltage through LC circuit that serves to filter and smooth it before connected to UPQC-DC link.BES connected to the UPQC-DC link circuit serves as energy storage and is expected to overcome interruption voltage and overall help UPQC performance to improve voltage and current quality on source and load bus. Simulation parameters proposed in this study is shown in Appendix Section. Power quality analysis is performed on PV, Wind, PV-Wind Hybrid respectively, connected to 3P3W system through UPQC DC-link (on-grid) using BES circuit. Single phase circuit breakers (CBs) are used to connect and disconnect PV, Wind, and Hybrid PV-Wind respectively with UPOC DC-link.

There are six disturbance scenarios i.e. (1) NL, (2) Unba-NL, (3) Dis-NL, (4) Sag-NL, (5) Swell-NL, and (6) Inter-NL. In scenario 1, the model is connected a non-linear load with R_L and L_L of 60 Ohm and 0.15 mH respectively. In scenario 2, the model is connected to non-linear load and during 0.3 s since t=0.2 s to t=0.5 s connected to unbalance three phase load with R1, R2, R3 as 6 Ohm, 12 Ohm, 24 Ohm respectively, and value of C1, C2, C3 as 2200 µF. In scenario 3, the model is connected to non-linear load and source voltage generating 5th and 7th harmonic components with individual harmonic distortion values of 5% and 2% respectively. In scenario 4, the model is connected to non-linear load and source experiences a sag voltage disturbance of 50% for 0.3 s between t=0.2 s to t=0.5 s. In scenario 5, the model is connected to a non-linear load and source experiences a swell voltage disturbance of 50% for 0.3 s between t=0.2 s to t=0.5 s. In scenario 6, the model is connected to non-linear load and source experiences an interruption voltage interference of 100% for 0.3 s between t=0.2 s to t=0.5 s. FLC is used as a DC voltage control in a shunt active filter to improve the power quality of the load voltage and current source and compare it with PI controller. Each disturbance scenario uses a PI controller and FLC so that the total of 12 disturbances. The result analysis of research was carried out i.e. (1) voltage and current on source or poin common coupling (PCC) bus, (2) voltage and current on load bus, (3) harmonic voltage and harmonic current on source bus and (4) harmonic voltage and harmonic current on load bus. The final phase is to compare performance of UPQC-BES system on-grid supplied by PV, Wind, PV-Wind Hybrid respectively using two controllers to improve power quality of load voltage and source current under six disturbance conditions.



Figure 1. Proposed model of UPQC-BES system supplied by PV, Wind, and PV-Wind Hybrid

2.2. Photovoltaic model

Figure 2 shows the equivalent circuit and V-I characteristic of a solar panel. A solar panel is composed of several PV cells that have series, parallel, or series-parallel external connections [14].



Figure 2. Equivalent circuit and V-I characteristic of solar panel

The V-I characteristic of a solar panel is showed in (1):

$$I = I_{PV} - I_o \left[\exp\left(\frac{V + R_s I}{aV_t}\right) - 1 \right] - \frac{V + R_s I}{R_p}$$
(1)

where I_{PV} is the photovoltaic current, I_o is saturated reverse current, 'a' is the ideal diode constant, $V_t = N_S K T q^{-1}$ is the thermal voltage, N_S is the number of series cells, q is the electron charge, K is the Boltzmann constant, T is the temperature of p–n junction, R_S and R_P are series and parallel equivalent resistance of the solar panels. I_{PV} has a linear relation with light intensity and also varies with temperature variations. I_o is dependent on temperature variations. The values of I_{pv} and I_o are calculated as following (2) and (3):

$$I_{PV} = (I_{PV,n} + K_1 \Delta T) \frac{G}{G_n} I$$
⁽²⁾

$$I_o = \frac{I_{SC,n} + K_I \Delta T}{\exp(V_{OC,n} + K_V \Delta T) / aV_t - 1}$$
(3)

In which $I_{PV,n}$, $I_{SC,n}$ and $V_{OC,n}$ are photovoltaic current, short circuit current and open circuit voltage in standard conditions ($T_n=25$ C and $G_n=1000$ Wm⁻²) respectively. K_I is the coefficient of short circuit current to temperature, $\Delta T=T-T_n$ is the temperature deviation from standard temperature, G is the light intensity and K_I is the ratio coefficient of open circuit voltage to temperature. Open circuit voltage, short circuit current and voltage-current corresponding to the maximum power are three important points of I-V characteristic of solar panel. These points are changed by variations of atmospheric conditions. By using (4) and (5) which are derived from PV model equations, short circuit current and open circuit voltage can be calculated in different atmospheric conditions.

$$I_{SC} = (I_{SC} + K_1 \Delta T) \frac{G}{G_n}$$
⁽⁴⁾

$$V_{OC} = V_{OC} + K_V \Delta T \tag{5}$$

2.3. PMSG wind turbine

Wind turbine is one of part of an integrated system, which can be divided into two types i.e. fixed and variable speed wind turbines. In fixed speed type, rotating speed of turbine is fixed and hence, frequency of generated voltage remains constant, so it can be directly connected to the network. In this case, maximum power can not always be extracted by wind. On the other hand, on variable speed, turbine can rotate at different speeds, so maximum power can be generated in each wind speed by MPPT method [10]. The advantage of using a PMSG over a synchronous generator and DFIG machine because it has high efficiency and reliability. Due to the elimination of rotor external excitation, machine size, and cost also decreases, making PMSG to be more controlled easily with feedback control system. PMSG has become an attractive solution on wind generation systems with variable speed wind turbine applications [15]. Figure 3 and 4 shows model of PMSG wind turbine and wind turbin power characteristic curve.



Figure 3. Model of PMSG wind turbine



Figure 4. Wind turbin power characteristic curve

The output power of wind turbine can be expressed using (6), (7), and (8) [11].

$$\lambda = \frac{\omega_r R}{V_{wind}} \tag{6}$$

$$P_M = \frac{1}{2} \rho \pi R^2 C_p V_{wind}^3 \tag{7}$$

$$T_{M} = \frac{P_{M}}{\omega_{r}} = \frac{1}{2} \rho \pi R^{5} C_{p} \frac{\omega_{M}^{3}}{\lambda^{3}}$$

$$\tag{8}$$

Where λ is the speed-tip ratio, V_{wind} is wind speed, R is blade radius, ω_r is rotor speed (rad/sec), ρ is the air density, C_P is the power coefficient, P_M is the output mechanical power, and T_M is output torque of wind turbine. The C_P coefficient is dependent on the pitch angle value, at which rotor blade can rotate along axis and tip-speed ratio λ expressed in (9).

$$C_p = (0.44 - 0.167\beta)\sin\frac{\pi(\lambda - 2)}{(13 - 0.3\beta)}$$
(9)

Where β is a pitch angle blade. In a fixed pitch type, the value of β is set to a fixed value.

2.4. Control of series active filter

The main function of series active filter is as a sensitive load protection against a number of voltage interference at PCC bus. The control strategy algorithm of the source and load voltage in series active filter circuit is shown in Figure 5. It extracts the unit vector templates from the distorted input supply. Furthermore, the templates are expected to be ideal sinusoidal signal with unity amplitude. The distorted supply voltages are measured and divided by peak amplitude of fundamental input voltage V_m give in (10) [6].

$$V_m = \sqrt{\frac{2}{3} \left(V_{sa}^2 + V_{sb}^2 + V_{sc}^2 \right)}$$
(10)

A three phase locked loop (PLL) is used in order to generate a sinusoidal unit vector templates with a phase lagging by the use of sinus function. The reference load voltage signal is determined by multiplying the unit vector templates with the peak amplitude of the fundamental input voltage V_m . The load reference voltage (V_{La}^* , V_{Lb}^* , V_c^*) is then compared against to sensed load voltage (V_{La} , V_{Lb} , V_{Lc}) by a pulse width modulation (PWM) controller used to generate the desired trigger signal on series active filter.



Figure 5. Control strategy of series active filter

2.5. Control of shunt active filter

The main function of shunt active filter is mitigation of power quality problems on the load side. The control methodology in shunt active filter is that the absorbed current from the PCC bus is a balanced positive sequence current including unbalanced sag voltage conditions in the PCC bus or unbalanced conditions or non-linear loads. In order to obtain satisfactory compensation caesed by disturbance due to non-linear load, many algorithms have been used in the literature. This research used instantaneous reactive power theory method "p-q theory". The voltages and currents in Cartesian *abc* coordinates can be transformed to Cartesian $\alpha\beta$ coordinates as expressed in (11) and (12) [16].

$$\begin{bmatrix} v_{\alpha} \\ v_{\beta} \end{bmatrix} = \begin{bmatrix} 1 & -1/2 & -1/2 \\ 1 & \sqrt{3}/2 & -\sqrt{3}/2 \end{bmatrix} \begin{bmatrix} V_{\alpha} \\ V_{b} \\ V_{c} \end{bmatrix}$$
(11)

$$\begin{bmatrix} i_{\alpha} \\ i_{\beta} \end{bmatrix} = \begin{bmatrix} 1 & -1/2 & -1/2 \\ 1 & \sqrt{3}/2 & -\sqrt{3}/2 \end{bmatrix} \begin{bmatrix} i_{La} \\ i_{Lb} \\ i_{Lc} \end{bmatrix}$$
(12)

The computation of the real power (p) and imaginary power (q) is showed in (13). The real power and imaginary are measured instantaneously power and in matrix it is form is given as. The presence of oscillating and average components in instantaneous power is presented in (14) [17].

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$$\begin{bmatrix} p \\ q \end{bmatrix} = \begin{bmatrix} v_{\alpha} & v_{\beta} \\ -v_{\beta} & v_{\alpha} \end{bmatrix} \begin{bmatrix} i_{\alpha} \\ i_{\beta} \end{bmatrix}$$
(13)

$$p = \overline{p} + \widetilde{p} \quad ; q = \overline{q} + \widetilde{q} \tag{14}$$

Where \overline{p} = direct component of real power, \widetilde{p} = fluctuating component of real power, \overline{q} = direct component of imaginary power, \widetilde{q} = fluctuating component of imaginary power. The total imaginary power (q) and the fluctuating component of real power are selected as power references and current references and are utilized through the use of (15) for compensating harmonic and reactive power [18].

$$\begin{bmatrix} i_{c\alpha}^{*} \\ i_{c\beta}^{*} \end{bmatrix} = \frac{1}{v_{\alpha}^{2} + v_{\beta}^{2}} \begin{bmatrix} v_{\alpha} & v_{\beta} \\ v_{\beta} & -v_{\alpha} \end{bmatrix} \begin{bmatrix} -\widetilde{p} + \overline{p}_{loss} \\ -q \end{bmatrix}$$
(15)

The signal \overline{p}_{loss} , is obtained from voltage regulator and is utilized as average real power. It can also be specified as the instantaneous active power which corresponds to the resistive loss and switching loss of the UPQC. The error obtained on comparing the actual DC-link capacitor voltage with the reference value is processed in FLC, engaged by voltage control loop as it minimizes the steady state error of the voltage across the DC link to zero. The compensating currents ($i_{c\alpha}^*$, $i_{c\beta}^*$) as required to meet the power demand of load are shown in (15). These currents are represented in α - β coordinates. The phase current is required to acquire using (16) for compensation. These source phase currents (i_{sa}^* , i_{sb}^* , i_{sc}^*) are represented in a-b-c axis obtained from the compensating current in the α - β coordinates presented in (16) [18]. Figure 6 shows a control of shunt active filter.

$$\begin{bmatrix} i_{s_{\alpha}}^{*} \\ i_{s_{b}}^{*} \\ i_{s_{c}}^{*} \end{bmatrix} = \sqrt{\frac{2}{3}} \begin{bmatrix} 1 & 0 \\ -1/2 & \sqrt{3}/2 \\ -1/2 & -\sqrt{3}/2 \end{bmatrix} \begin{bmatrix} i_{c\alpha}^{*} \\ i_{c\beta}^{*} \end{bmatrix}$$
(16)



Figure 6. Control strategy of shunt active filter

The proposed model of UPQC-BES system supplied by three RE sources is shown in Figure 1. From the figure, we can see that PV is connected to the DC link through a DC-DC boost converter circuit. The PV partially distributes power to the load and the remains is transfered to three phase grid. The load consists of non linear and unbalanced load. The non-linear load is a diode rectifier circuit with the RL load type, while the unbalanced load is a three phase RC load with different R value on each phase. In order to economically efficient, PV must always work in MPP condition. In this research, MPPT method used is P and O algorithm. The model is also applied for UPQC-BES system which is supplied by wind and PV-wind hybrid respectively. In order to operate properly, UPQC-BES system device must have a minimum DC link voltage (V_{dc}). The value of common DC link voltage depends on the nstantaneous energy avialable to UPQC is defined by in (17) [16]:

$$V_{dc} = \frac{2\sqrt{2}V_{LL}}{\sqrt{3}m} \tag{17}$$

where m is modulation index and V_{LL} is the AC grid line voltage of UPQC. Considering that modulation index as 1 and for line to line grid voltage (V_{LL} =380 volt), the V_{dc} is obtained 620, 54 volt and selected as 650 volt.

The input of shunt active filter showed in Figure 5 is DC voltage (V_{dc}) and reference DC voltage (V_{dc}^*), while the output is \bar{p}_{loss} by using PI controller. Then, the \bar{p}_{loss} is as one of input variable to generate the reference source current (I_{sa}^* , I_{sb}^* , and I_{sc}^*). The reference source current output is then compared to source current (I_{sa} , I_{sb} , and I_{sc}) by the current hysteresis control to generate trigger signal in IGBT circuit of shunt active filter. In this research, FLC as DC voltage control algorithm on shunt active filter is proposed and compared with PI controller. The FLC is capable of reduce oscilation and generate quick convergence calculation during disturbances. This method is also used to overcome the weakness of PI controller in determining proportional gain (K_p) and integral gain constant (K_i) which still use trial and error method.

2.6. Fuzzy logic controller

The research is started by determine \overline{p}_{loss} as the input variable to result the reference source current on current hysteresis controller to generate trigger signal on the IGBT shunt active filter of UPQC using PI controller (K_p=0.2 and K_i=1.5). By using the same procedure, \overline{p}_{loss} is also determined by using FLC. The FLC has been widely used in recent industrial process because it has heuristic, simpler, more effective and has multi rule based variables in both linear and non-linear system variations. The main components of FLC are fuzzification, decision making (rulebase, database, reason mechanism) and defuzzification in Figure 7. The output membership function is generated using inference blocks and the basic rules of FLC as shown in Table 1.



The fuzzy rule algorithm collects a number of fuzzy control rules in a particular order. This rule is used to control the system to meet the desired performance requirements and they are designed from a number of intelligent system control knowledge. The fuzzy inference of FLC using Mamdani method related to max-min composition. The fuzzy inference system in FLC consists of three parts: rule base, database, and reasoning mechanism [19]. The FLC method is performed by determining input variables V_{dc} (V_{dc-error}) and delta Vdc ($\Delta V_{dc-error}$), seven linguistic fuzzy sets, operation fuzzy block system (fuzzyfication, fuzzy rule base and defuzzification), $V_{dc-error}$ and $\Delta V_{dc-error}$ during fuzzification process, fuzzy rule base table, crisp value to determine \bar{p}_{loss} in defuzzification phase. The \bar{p}_{loss} is one of input variable to obtain compensating currents (i_{ca}^*, i_{cb}^*) in (16). During fuzzification process, a number of input variables are calculated and converted into linguistic variables based on a subset called membership function. The error Vdc (V_{dc-error}) and delta error Vdc ($\Delta V_{dc-error}$) are proposed input variable system and output variable is \overline{p}_{loss} . To translate these variables, each input and output variable is designed using seven membership functions: Negative Big (NB), Negative Medium (NM), Negative Small (NS), Zero (Z), Positive Small (PS), Positive Medium (PM) and Positive Big (PB). The membership functions of crisp input and output are presented with triangular and trapezoidal membership functions. The value of V_{dc-error} range from -650 to 650, $\Delta V_{dc-error}$ from -650 to 650, and \bar{p}_{lass} from -100 to 100. The input and output MFs are shown in Figure 8.



Figure 8. Membership functions (a) $V_{dc-error}$, (b) $\Delta V_{dc-error}$, and (c) \overline{p}_{lass}

After the V_{dc-error} and Δ V_{dc-error} are obtained, then two input membership functions are converted to linguistic variables and uses them as input functions for FLC. The output membership function is generated using inference blocks and the basic rules of FLC as shown in Table 1. Finally the defuzzification block operates to convert generated \overline{p}_{loss} output from linguistic to numerical variable again. Then it becomes input variable for current hysteresis controller to produce trigger signal on the IGBT circuit of UPQC shunt active filter to reduce source current and load voltage harmonics. While simultaneously, it also improve power quality of 3P3W system under six scenarios due to the integration of three RE sources to UPQC-BES system.

3. RESULTS AND ANALYSIS

The analysis of proposed model is investigated through determination of six disturbance scenarios i.e. (1) NL, (2) Unba-NL, (3) Dis-NL, (4) Sag-NL, (5) Swell-NL, and (6) Inter-NL. Each scenario of UPQC uses PI controller and FLC so total number of disturbance are 12 scenarios.By using Matlab/Simulink, the model is then executed according to the desired scenario to obtain curve of source voltage (V_s), load voltage (V_L), compensation voltage (V_c), source current (V_s), load current (I_L), and DC voltage DC link (V_{dc}). Then, THD value of source voltage, source current, load voltage, and load current in each phase as well as average THD value (Avg THD) are obtained base on the curves. THD in each phase is determined in one cycle started at t = 0.35 s. The results of average of source voltage, source current, load voltage, source current of 3P3W system using UPQC-BES system supplied by three RE sources i.e. PV, wind, and PV-wind hybrid are presented in Table 2, 3, and 4. Next THD in each phase and average THD are showed in Table 5, 6 and 7.

Table 2 shows UPQC-BES system supplied PV connected 3P3W system using PI and FLC, disturbance scenarios 1 to 5 produce an average load voltage above 307 V. While in scenario 6, FLC produces a higher average load voltage of 304.1 V than if using a PIof 286.7 V. If reviewed from average source current with PI, the highest and lowest average source currents are generated by disturbance scenarios

2 and 4 of 28.15 A and 7,246 A. Whereas if using FLC the highest and lowest average source currents are achieved in scenario 2 and 6 of 28.84 A and 3.804 A. Table 3 shows UPQC-BES supplied by wind connected to 3P3W with PI and FLC, scenarios 1 to 5 is able to obtain a stable load voltage above 308 V. The difference is that in scenario 6, PI generates a load voltage of 274.8 V, otherwise if using FLC, load voltage increases to 306.4 V. If reviewed from source current using PI, the highest and lowest average source currents are resulted by scenarios 2 and 4 of 28.28 A and 7.417 A. Rather, if using FLC, the highest and lowest average source currents are achieved in scenario 2 and 6 of 28.82 A and 3,420 A. Table 4 shows UPQC-BES supplied PV-wind hybrid connected 3P3W using PI and FLC, scenarios 1 to 5 produce an average load voltage above 307 V. While in scenario 6, FLC generates an average load voltage 305.9 V higher than if using PI control of 283.9 V. If reviewed from average source current with PI, the highest and lowest average source currents are resulted by scenarios 2 and 4 of 28.21 A and 6,773 A. Otherwise if using FLC the highest and lowest average source currents are achieved in scenario 2 and 6 of 28.82 A and 3.640 A respectively.

Table 2. Voltage and Current of 3P3W System Using UPQC-BES System Supplied by PV

Con	So	urce Vol	tage V _S ((V)		Load Vo	ltage V _L (V)	Se	ource Cu	rrent I _S (.	A)	I	Load Cu	rent I _L (A	<i>I</i>)
Self	Ph A	Ph B	Ph C	Avg	Ph A	Ph B	Ph C	Avg	Ph A	Ph B	Ph C	Avg	Ph A	Ph B	Ph C	Avg
							PI	Controlle	er							
1	309.6	309.6	309.6	309.6	307.6	307.8	307.7	307.7	7.766	7.793	7.759	7.773	8.528	8.529	8.533	8.530
2	307.4	308.0	308.0	307.8	308.3	308.7	308.3	308.4	31.00	24.84	28.73	28.15	22.50	34.12	34.52	30.38
3	309.6	309.6	309.6	309.6	313,8	314.3	317.4	317.4	7.897	7.919	7.867	7.895	8.748	8.704	8.785	8.746
4	154.5	154.5	154.5	154.5	307.1	307.3	307.3	307.2	7.235	7.276	7.226	7.246	8.509	8.514	8.510	8.511
5	464.7	464.7	464.7	464.7	308.6	308.7	308.6	308.6	7.979	7.980	7.964	7.975	8.550	8.553	8.554	8.553
6	0.536	1.385	0.850	0.924	310.2	259.8	290.2	286.7	7.392	12.67	6.045	8.703	8.707	7.747	7.637	8.031
							Fuzzy l	Logic Cor	troller							
1	309.5	309.5	309.5	309.5	307.7	307.9	307.7	307.8	8.420	8.426	8.416	8.421	8.527	8.532	8.531	8.530
2	307.4	307.9	308.0	307.8	308.5	308.7	308.4	308.5	31.66	25.50	29.36	28.84	22.52	34.11	35.52	30.72
3	309.6	309.5	309.5	309.5	313.4	312.9	315.9	314.1	8.516	8.565	8.496	8.526	8.741	8.677	8.736	8.718
4	154.4	154.4	154.4	154.4	307.3	307.3	307.2	307.3	8.563	8.560	8.561	8.561	8.514	8.517	8.512	8.515
5	464.6	464.6	464.6	464.6	308.6	308.8	308.6	308.7	8.396	8.389	8.389	8.392	8.552	8.556	8.554	8.554
6	0.447	0.392	0.380	0.407	314.0	293.4	304.9	304.1	4.024	3.778	3.608	3.804	8.874	8.195	8.193	8.421

Table 3. Voltage and Current of 3P3W System Using UPQC-BES System Supplied by Wind

C	So	urce Vol	tage Vs (V)	L	oad Volt	age V _L (V	V)	Se	ource Cu	rrent Is (A	A)		Load Curr	ent I _L (A)	
SCII	Ph A	Ph B	Ph C	Avg	Ph A	Ph B	Ph C	Avg	Ph A	Ph B	Ph C	Avg	Ph A	Ph B	Ph C	Avg
								PI Cont	roller							
1	309.5	309.6	309.6	309.6	308.6	308.6	308.2	308.5	7.863	7.875	7.840	7.869	8.554	8.553	8.546	8.551
2	307.4	308.0	308.0	308.0	308.9	309.2	308.7	308.9	31.07	24.97	28.81	28.28	22.55	34.17	34.57	30.43
3	309.6	309.5	309.6	309.6	312.9	312.9	315.4	313.8	7.993	8.015	7.947	7.985	8.817	8.682	8.741	8.747
4	154.5	154.5	154.5	154.5	308.0	308.1	307.8	307.9	7.428	7.455	7.368	7.417	8.527	8.535	8.532	8.531
5	464.7	464.7	464.7	464.7	309.3	309.3	309.0	309.2	8.015	8.020	8.002	8.012	8.564	8.573	8.568	8.568
6	1.256	1.022	0.592	0.957	234.0	316.4	274.0	274.8	11.27	9.866	7.028	9.388	5.958	8.697	8.204	7.619
							Fuz	zy Logic	Controll	er						
1	309.5	309.5	309.5	309.5	308.5	308.6	308.3	308.5	8.418	8.410	8.414	8.414	8.545	8.552	8.549	8.549
2	307.4	307.9	308.0	307.8	309.0	309.3	308.9	309.1	31.64	25.47	29.34	28.82	22.56	34.18	34.59	30.44
3	309.5	309.5	309.5	309.5	313.2	313.7	314.1	313.7	8.519	8.531	8.531	8.527	8.713	8.714	8.718	8.715
4	154.4	154.4	154.4	154.4	308.0	308.1	307.7	307.9	8.557	8.539	8.561	8.552	8.528	8.541	8.525	8.531
5	464.6	464.7	464.7	464.7	309.2	309.3	309.2	309.2	8.391	8.385	8.388	8.388	8.565	8.570	8.567	8.567
6	0.357	0.396	0.397	0.383	303.7	300.0	315.3	306.4	3.358	3.464	3.542	3.420	8.557	8.418	8.731	8.569

Table 4. Voltage and Current of 3P3W System Using UPQC-BES System Supplied PV-Wind Hybrid

Son	So	Source Voltage $V_S(V)$ Load Voltage $V_L(V)$ Source Current $I_S(A)$								A)	I	load Curi	rent I _L (A	.)		
SCII	Ph A	Ph B	Ph C	Avg	Ph A	Ph B	Ph C	Avg	Ph A	Ph B	Ph C	Avg	Ph A	Ph B	Ph C	Avg
							PI	Controll	er							
1	309.6	309.6	309.6	309.6	307.8	308.0	307.7	307.8	7.790	7.802	7.770	7.787	8.527	8.537	8.533	8.533
2	307.4	308.0	308.0	307.8	308.4	308.8	308.4	308.6	31.02	24.87	28.74	28.21	22.52	34.13	34.53	31.40
3	309.6	309.5	309.6	309.6	314.0	315.5	316.9	315.5	7.942	7.939	7.918	7.933	8.739	8.750	8.783	8.757
4	154.5	154.5	154.5	154.5	307.3	307.4	307.2	307.3	7.289	7.309	7.251	7.283	8.513	8.516	8.515	8.515
5	464.7	464.7	464.7	464.7	308.7	308.9	308.7	308.8	7.985	7.985	7.975	7.982	8.552	8.558	8.558	8.556
6	1.048	0.825	0.845	0.906	247.5	300.7	303.7	283.9	5.119	5.927	9.271	6.773	7.016	7.893	8.793	7.867
							Fuzzy I	logic Con	ntroller							
1	309.5	309.5	309.5	309.5	307.8	308.0	307.7	307.8	8.419	8.418	8.409	8.413	8.529	8.539	8.533	8.534
2	307.4	307.9	308.0	307.8	308.7	308.7	308.9	308.8	31.66	25.47	29.32	28.82	22.54	34.13	34.56	30.41
3	309.5	309.5	309.5	309.5	314.4	315.5	316.6	315.5	8.581	8.593	8.568	8.581	8.761	8.722	8.761	8.748
4	154.4	154.4	154.4	154.4	307.3	307.5	307.3	307.4	8.566	8.572	8.563	8.567	8.511	8.520	8.519	8.517
5	464.6	464.6	464.6	464.6	308.8	308.8	308.7	308.8	8.391	8.394	8.396	8.394	22.33	22.35	22.36	22.35
6	0.412	0.403	0.402	0.418	311.6	295.7	310.4	305.9	3.774	3.544	3.593	3.640	8.855	8.321	8.288	8.488

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		Ta	ble 5.	Harm	onics	of 3P3	W Sys	stem U	sing UF	QC-BE	ES Syste	em Supp	olied b	y PV		
C	Sou	rce Volta	ge THD ((%)	Lo	ad Voltag	ge THD ((%)	Se	ource Curr	ent THD (%)		Load Cu	rrent (%)	
Scii	Ph A	Ph B	Ph C	Avg	Ph A	Ph B	Ph C	Avg	Ph A	Ph B	Ph C	Avg	Ph A	Ph B	Ph C	Avg
								PI Co	ntroller							
1	2.35	2.36	2.32	2.34	2.48	2.50	2.46	2.48	12.89	12.72	12.92	12.84	22.32	22.34	22.32	22.33
2	2.29	2.20	2.24	2.24	2.43	2.23	2.37	2.34	2.660	2.330	2.240	2.410	5.230	2.070	2.660	3.320
3	5.84	5.86	5.94	5.88	6.36	5.90	6.58	6.28	12.75	12.64	13.06	12.82	21.92	22.16	22.33	22.14
4	4.69	4.75	4.81	4.75	2.46	2.48	2.53	2.49	14.26	13.96	14.16	14.13	22.28	22.31	22.28	22.29
5	1.56	1.53	1.55	1.55	2.47	2.43	2.45	2.45	12.51	12.36	12.44	12.44	22.34	22.32	22.32	22.33
6	NA	NA	NA	NA	32.11	15.09	28.54	25.25	270.90	145.89	275.67	230.82	47.70	34.58	36.29	39.53
							F	uzzy Log	ic Controll	ler						
1	2.35	2.33	2.35	2.34	2.48	2.46	2.49	2.47	11.83	11.82	11.84	11.83	22.33	22.32	22.33	22.33
2	2.25	2.27	2.20	2.24	2.39	2.41	2.34	2.38	2.620	2.400	2.220	2.413	5.230	2.100	2.640	3.323
3	5.83	5.88	5.93	5.88	6.23	5.93	6.69	6.28	11.83	11.90	12.14	11.96	21.84	22.34	22.53	22.24
4	4.71	4.76	4.79	4.75	2.46	2.48	2.50	2.48	11.91	11.88	11.86	11.89	22.27	22.32	22.32	22.31
5	1.55	1.54	1.54	1.54	2.45	2.44	2.46	2.45	11.90	11.84	11.85	11.86	22.36	22.33	22.35	22.35
6	NA	NA	NA	NA	13.05	6.60	11.15	10.27	30.61	34.72	31.57	32.30	24.25	24.25	24.71	24.40

Table 6. Harmonics of 3P3W System Using UPQC-BES System Supplied by Wind

Con	Sour	ce Volta	ge THD	(%)	Lo	ad Volta	ge THD ((%)	Sc	ource Curr	ent THD (9	%)		Load Cu	rrent (%)	
SCII	Ph A	Ph B	Ph C	Avg	Ph A	Ph B	Ph C	Avg	Ph A	Ph B	Ph C	Avg	Ph A	Ph B	Ph C	Avg
								PI Cor	ntroller							
1	1.88	1.87	1.94	1.89	1.99	1.97	2.05	2.00	12.63	12.37	12.70	12.57	12.30	12.30	12.34	12.31
2	1.83	1.76	1.82	1.80	1.92	1.85	1.93	1.90	2.460	2.070	2.200	2.240	5.260	2.070	2.690	3.340
3	5.67	5.71	5.77	5.72	6.00	6.83	6.02	6.28	12.48	12.26	12.66	12.47	22.01	22.12	22.08	22.07
4	3.76	3.86	3.86	1.83	1.97	2.02	2.03	2.01	13.59	13.17	13.51	13.42	22.29	22.31	22.30	22.30
5	1.26	1.24	1.29	1.26	1.99	1.97	2.05	2.00	12.31	12.20	12.31	12.27	22.36	22.33	22.37	22.35
6	NA	NA	NA	NA	14.09	35.59	34.73	28.14	157.76	139.01	266.07	186.95	37.60	34.39	46.97	39.65
							Fι	ızzy Logi	c Controll	er						
1	1.89	1.88	1.93	1.90	1.99	1.98	2.04	2.00	11.71	11.72	11.77	11.73	22.34	22.31	22.32	22.32
2	1.85	1.79	1.78	1.81	1.95	1.87	1.88	1.90	2.43	2.11	2.12	2.220	5.240	2.070	2.700	3.240
3	5.67	5.71	5.78	5.72	5.99	6.39	6.13	6.17	11.72	11.62	11.90	11.75	22.08	21.94	22.47	22.16
4	3.79	3.81	3.86	3.82	1.97	1.99	2.03	1.99	11.72	11.69	11.74	11.72	22.28	22.30	22.35	22.31
5	1.27	1.24	1.28	1.26	2.00	1.96	2.04	2.00	11.66	11.76	11.76	11.73	22.31	22.33	22.35	22.33
6	NA	NA	NA	NA	7.59	6.44	10.95	8.33	27.33	28.27	26.39	27.33	25.39	23.65	24.31	24.45

Table 7. Harmonics of 3P3W System Using UPQC-BES System Supplied by PV-Wind Hybrid

								-	-		-					
Son	Sour	rce Voltag	ge THD	(%)	Loa	d Voltag	e THD (9	%)	Sc	ource Curre	ent THD (%)		Load Cu	rrent (%)	
Self	Ph A	Ph B	Ph C	Avg	Ph A	Ph B	Ph C	Avg	Ph A	Ph B	Ph C	Avg	Ph A	Ph B	Ph C	Avg
								PI Co	ntroller							
1	2.25	2.19	2.29	2.24	2.37	2.31	2.42	3.37	12.85	12.62	12.74	12.74	22.33	22.31	22.34	22.33
2	2.18	2.08	2.15	2.13	2.30	2.19	2.18	2.22	2.630	2.300	2.290	2.407	5.230	2.070	2.670	3.323
3	5.81	5.82	5.89	5.84	6.12	5.88	6.75	6.25	12.71	12.63	12.98	12.77	22.05	22.13	22.54	22.24
4	4.53	4.48	4.51	4.51	2.37	2.35	2.37	2.36	14.16	13.50	13.99	13.88	22.27	22.30	22.28	22.28
5	1.49	1.46	1.51	1.49	2.37	2.31	2.40	2.36	12.43	12.29	12.41	12.38	22.34	22.32	22.33	22.33
6	NA	NA	NA	NA	18.61	36.38	28.42	27.8	387.71	330.34	189.29	302.45	36.73	38.51	36.83	37.36
							Fuz	zy Log	ic Control	ler						
1	2.25	2.23	2.25	2.24	2.37	2.35	2.39	2.37	11.85	11.74	11.84	11.81	22.32	22.31	22.33	22.32
2	2.23	2.15	2.05	2.14	2.37	2.26	2.17	2.26	2.520	2.410	2.140	2.446	5.230	2.070	2.690	3.330
3	5.80	5.83	5.90	5.84	6.57	5.26	7.06	6.29	11.83	11.78	12.24	11.95	22.15	22.23	22.95	22.44
4	4.53	4.52	4.54	4.86	2.36	2.35	2.35	2.35	11.79	11.74	11.84	11.79	22.29	22.30	22.29	22.29
5	1.48	1.46	1.51	1.48	2.35	2.32	2.40	2.35	11.78	11.81	11.81	11.80	22.33	22.35	22.36	22.35
6	NA	NA	NA	NA	10.30	4.90	10.25	8.48	27.44	29.52	28.63	28.53	23.20	23.97	24.65	23.94

Table 5 shows that average THD of load voltage (V_L) of UPQC-BES system supplied by PV in 3P3W system for scenarios 1 to 5 using PI control is within limits in IEEE 519. The highest and lowest average THD load voltages are achieved under scenario 6 and 2 as 25.25% and 2.34% respectively. PI controller is also able to mitigation average THD source voltage in scenario 6 from not accessible (NA) to 25.25% on the load side. The highest and lowest average THD of source current are achieved in scenario 6 and 2 as 230.82% and 2.41%. Table 5 also indicates that average THD of load voltage of UPQC system supplied by PV with BES using FLC in scenarios 1 to 5, has fulfilled limits in IEEE 519. The highest and lowest average THD of load voltage are achieved under scenario 6 and 2 of 10.27% and 2.38%. The use of FLC method is also able to reduce average THD on source voltage in scenario 6 from NA to 10.27% on load side. The highest and lowest average THD of source current are achieved in scenario 6 and 2 of 32.30% and 2.413%.

Table 6 shows that average THD of load voltage of UPQC-BES system supplied by wind in 3P3W system for interference scenarios 1 to 5 using PI is within limits prescribed in IEEE 519. The highest and lowest average THD load voltages is achieved under scenario 6 and scenario 2 as 28.14% and 1.90% respectively. PI controller is also able to reduce average THD source voltage in scenario 6 from NA to 28.14% on the load side. The highest and lowest average THD of source current are achieved in scenario 6 and 2 as 186.95% and 2.24% respectively. Table 6 also shows that average THD of load voltage of UPQC-BES supplied by wind using FLC in scenarios 1 to 5, has fulfilled limits prescribed in IEEE 519. The highest and lowest average THD of load voltage are achieved under scenario 6 and 4 of 8.33% and 1.90%. FLC method is also able to reduce average THD on source voltage in scenario 6 from NA to 7.33% on load side. The highest and lowest average THD source current are achieved in scenario 6 and 2 of 27.33% and 2.22%.

Table 7 shows that average THD of load voltage (V_L) of UPQC-BES system supplied by PV-wind hybrid in 3P3W system for scenarios 1 to 5 using PI is within limits in IEEE 519. The highest and lowest average THD load voltages are achieved under scenario 6 and 2 as 27.8% and 2.22% respectively. PI is also able to mitigate average THD source voltage in scenario 6 from NA to 27.8% on load side. The highest and lowest average THD of source current are achieved in scenario 6and 2 as 302.45% and 2.407% respectively. Table 7 also indicates that average THD of load voltage of UPQC-BES system supplied by PV-wind hybrid using FLC for scenarios 1 to 5, has fulfilled limits in IEEE 519. The highest and lowest average THD of load voltage are achieved under scenario 6 and 2 of 8.48% and 2.26%. FLC method is also able to reduce average THD on source voltage in scenario 6 from NA to 8.48% on load side. The highest and lowest average THD of source current are achieved in scenario 5 and 2 of 28.53% and 2.446%. Overall for UPQC-BES systemsystem supplied by three RE sources in scenarios 1 to 5 using PI and FLC is able to improve average THD of source current better on average THD of load current. Figure 9 presents UPQC-BES system performance supplied by three RE sources using FLC in scenario 6.

Figure 9 a(i) shows that in scenario 6, UPQC-BES system supplied by PV at t=0.2 s to t=0.5 s, average source voltage (V_S) falls as 100% to 0.4062 V. During the disturbance, PV is able to generate power to UPQC DC link and injecting full average compensation voltage (V_c) in Figure 9 a(iii) through injection transformer on series active filter so that average load voltage (VL) in Figure 9 a(ii) remains stable at 304.1 V. As long as fault period, although nominal of average source current (I_s) in Figure 9 a(iv) drops to 3.804 A, combination of PV and BES is able to generate power, store excess energy of PV, and inject current into load through shunt active filter so that average load current (IL) in Figure 9 a(v) remains as 8.421 A. Figure 9 b(i) presents on UPQC-BES supplied by wind at t=0.2 s to t=0.5 s average source voltage (Vs) drops 100% to 0.3828 V. During the disturbance, wind is able to generate power to UPQC DC link and injecting full average compensation voltage (V_C) in Figure 9 b(iii) through injection transformer on series active filter so that average load voltage (V_L) in Figure 9 b(ii) remains stable at 306.4 V. During fault period, although nominal of average source current (Is) falls to 3.420 A, combination of wind and BES is able to generate power, store excess energy of wind, and inject current into load through shunt active filter so that average load current (I₁) in Figure 9 b(v) remains as 8.569 A. Figure 9 c(i) indicates on UPQC-BES supplied by PV-Wind Hybrid at t=0.2 s to t=0.5 s average source voltage (V_s) drops 100% to 0.4175 V. During the disturbance, PV-wind hybrid is able to generate power to UPQC DC link and injecting full average compensation voltage (V_c) in Figure 9 c(iii) through injection transformer on series active filter so that average load voltage (V_L) in Figure 9 b(ii) remains stable at 305.9 V. As long as disturbance period, although nominal of average source current (Is) falls to 3.640 A, combination of PV-wind hybrid and BES is able to generate power, store excess energy of wind, and inject current into load through shunt active filter so that average load current (I_L) in Figure 9 c(v) remains as 8.488 A.

Figure 10 shows spectra of load voltage harmonics on phase A of UPQC-BES system supplied by three RE sources using FLC in scenario 6. Figure 11 shows performance of average THD of load voltage and source current on UPQC-BES system supplied by three RE sources. Figure 11(a) shows that in scenario 1 to 5, the implementation of FLC on UPQC-BES system supplied by three RE sources is able to obtain average THD of load voltage slightly better than PI controller and both method have already met the limit in IEEE 519. Further under scenario 6, FLC applied on UPQC-BES system supplied by three RE sources gives significantly better result of average THD of load voltage than PI controller. In six disturbance scenarios, both PI controller and FLC applied on UPQC-BES system supplied by three RE sources, PV is able to obtain the highest average THD of load voltages. Figure 11(b) shows that in disturbance scenario 1 to 5, implementation of FLC on UPQC-BES system supplied by three RE sources is able to obtain average THD of source current slightly better than PI controller. Furthermore under scenario 6, FLC applied on UPQC-BES system supplied by three RE sources is able to obtain average THD of source current slightly better than PI controller. Furthermore under scenario 6, FLC applied on UPQC-BES system supplied by three RE sources is able to obtain average THD of source current slightly better than PI controller. Furthermore under scenario 6, FLC applied on UPQC-BES system supplied by three RE sources is able to obtain average THD of source current than PI controller. Both PI controller and FLC on UPQC-BES system supplied by three RE sources in six disturbance scenarios, PV is able to obtain the highest average THD of source current.



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Figure 9. UPQC-BES system performance using FLC in scenario 6 (Inter-NL): (a) UPQC-BES + PV; (b) UPQC-BES + Wind; (c) UPQC-BES + PV-Wind Hybrid







(a) Average load voltage harmonics



(b) Average source current harmonics

Figure 11. Performance of UPQC-BES supplied by three RE sources using PI and FLC

4. CONCLUSION

Comparative performance analysis of UPQC-BES system supplied by three RE sources i.e. PV, wind, and PV-wind hybrid respectively using PI controller and FLC have been discussed. In disturbance scenario 1 to 5, implementation of FLC on UPQC-BES system supplied by three RE sources is able to obtain average THD of load voltage slightly better than PI and both methods have already met the limit in IEEE 519. Under scenario 6, FLC applied on UPQC-BES system supplied by three RE sources gives significantly better result average THD of load voltage than PI. In six disturbance scenarios, both PI and FLC applied on UPQC-BES system supplied by three RE sources is able to obtain the highest average THD of load voltage. In interference scenario 1 to 5, FLC method on UPQC-BES system supplied by three RE sources is able to obtain average THD of source current slightly better than PI. Furthermore under scenario 6, FLC applied on UPQC-BES system supplied by three RE sources gives significantly better result of average THD of source current slightly better than PI. Furthermore under scenario 6, FLC applied on UPQC-BES system supplied by three RE sources gives significantly better result of average THD of source current slightly better than PI. Furthermore under scenario 6, FLC applied on UPQC-BES system supplied by three RE sources gives significantly better result of average THD of source current than PI. Both PI and FLC on UPQC-BES system supplied by three RE sources in six scenarios, PV is able to obtain the highest average THD of source current.

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APPENDIX

Three phase grid: RMS voltage 380 volt (L-L), 50 Hz, line impedance: $R_s=0.1$ Ohm $L_s=15$ mH; series and shunt active filter: series inductance $L_{se}=0.015$ mH; shunt inductance $L_{sh}=15$ mH; injection transformers: rating 10 kVA, 50 Hz, turn ratio $(N_1/N_2)=1:1$; non linear load: resistance $R_L=60$ ohm, inductance $L_L=0.15$ mH, load impedance $R_c=0.4$ ohm and $L_c=15$ mH; unbalance load: resistance $R_1=24$ ohm, $R_2=12$ ohm, and $R_3=6$ ohm, capacitance $C_1, C_2, C_3=2200 \ \mu\text{F}$; DC-link: voltage $V_{DC}=650$ volt and capacitance $C_{DC}=3000 \ \mu\text{F}$; battery energe storage: type=nickel metal hybrid, DC voltage=650 volt, rated capacity= 200 Ah, initial SOC=100%, inductance $L_1=6$ mH, capacitance $C_1=200 \ \mu\text{F}$; photovoltaic: active power= 0.6 kW temperature=25° C, irradiance=1000 W/m²; PMSG wind turbine active power=0.6 kW, voltage= 380 volt, 50 Hz, wind speed=5 m/s, picth angle=2; PI controller: $K_p=0.2$, $K_i=1.5$; fuzzy model: method= mamdani, composition=max-min; input membership function: error (V_{dc})=trapmf, trimf delta error (ΔV_{dc})= trapmf, trimf; output membership function: \overline{p}_{loss} =trapmf,trimf.

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Amirullah was born in Sampang East Java Indonesia, in 1977. He received bachelor and master degree in electrical engineering from University of Brawijaya Malang and ITS Surabaya, in 2000 and 2008, respectively. He also worked as a lecturer in University of Bhayangkara Surabaya. He is currently working toward the doctoral degree, in electrical engineering in Power System and Simulation Laboratory (PSSL) ITS Surabaya. His research interest includes power distribution modeling and simulation, power quality, harmonics migitation, design of filter/PFC, and RE.



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Matlab/simulink simulation of unified power quality conditioner-battery energy storage system supplied by PV-wind hybrid using fuzzy logic controller

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ABSTRACT

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This paper presents performance analysis of Unified Power Quality Conditioner-Battery Energy Storage (UPQC-BES) system supplied by Photovoltaic (PV)-Wind Hybrid connected to three phase three wire (3P3W) of 380 volt (L-L) and 50 hertz distribution system. The performance of supply system is compared with two renewable energy (RE) sources i.e. PV and Wind, respectively. Fuzzy Logic Controller (FLC) is implemented to maintain DC voltage across the capacitor under disturbance scenarios of source and load as well as to compare the results with Proportional Intergral (PI) controller. There are six scenarios of disturbance i.e. (1) non-linear load (NL), (2) unbalance and nonlinear load (Unba-NL), (3) distortion supply and non-linear load (Dis-NL), (4) sag and non-linear load (Sag-NL), (5) swell and non-linear load (Swell-NL), and (6) interruption and non-linear load (Inter-NL). In disturbance scenario 1 to 5, implementation of FLC on UPQC-BES system supplied by three RE sources is able to obtain average THD of load voltage/source current slightly better than PI. Furthermore under scenario 6, FLC applied on UPQC-BES system supplied by three RE sources gives significantly better result of average THD of load voltage/source current than PI. This research is simulated using Matlab/Simulink.

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1. INTRODUCTION

PV and wind are the most RE distributed generations (DGs) because they are able to convert sunlight and wind into power. PV and solar are the potential DGs sources since it only need sunlight to generate electricity, where the resources are available in abundance, free and relatively clean. Indonesia has enormous energy potential from the sun because it lies on the equator. Almost all areas of Indonesia get sunlight about 10 to 12 hours per day, with an average intensity of irradiation of 4.5 kWh/m² or equivalent to 112.000 GW. The potential of wind energy in Indonesia generally has a speed between 4 to 5 m/s and classified as medium scale with potential capacity of 10 to 100 kW. The weakness of PV and wind turbine besides able to generate power, they also produces a number voltage and current harmonics resulted by presence of several types of PV and wind turbine devices and power converters as well as to increase a number of non-linear loads connected to the grid, so finally resulting in the decrease in power quality.

In order to overcome and improve power quality due to presence of non-linear loads and integration of PV and wind turbine to grid, UPQC is a proposed. UPQC serves to compensate for source voltage quality problemsi.e. sag, swell unbalance, flicker, harmonics, and load current quality problems i.e. harmonics,

unbalance, reactive currents, and neutral current. B. Han et. al and Vinod Khadkikar have investigated UPQC as one part of active power filter consisting of shunt and series active filters connected in parallel and serves as superior controller to overcome a number of power quality problems simultaneously. Series component has been responsible for reducing a number of interference on source side i.e. voltage sag/swell, flicker, unbalanced voltage, and harmonics. Shunt component has been responsible for addressing a current quality problems i.e. low power factor, load current harmonics, and unbalanced load. [1, 2]. UPQC based on RE has been investigated by some researchers. There are two methods used to overcome this problem i.e. using conventional and artificial intelligence. Shafiuzzaman K.K., et.al have proposed system includes a series inverter, shunt inverter, and a DG connected to a DC link through a rectifier using PI. The system was capable of increase source voltage quality i.e. sag and interruption and load current quality, as well as transfer of active power on/off grid mode [3]. The influence of DG on UPQC performance in reducing sag under conditions of some phase to ground faults to using DSTATCOM has been implemented by Norshafinash S., et.al. The DG was effective enough to help UPQC to improve sag [4]. It was connected in series with load resulting better sag mitigation compared to system without DG. Implementation of UPQC using UVTG method with PI to reduce sag, swell, voltage/current harmonics has been doneby S. N. Gohil, et.al. Simulation of voltage distortion was made by adding 5th and 7th harmonics at fundamental source voltage, resulting in a reduction of THD source current and THD load voltage [5].

UPQC supplied by PV panels using boost converter, PI, MPPT P and O, and p-q theory has been proposed by Yahia Bouzelata at.al [6]. The system was capable of compensate reactive power and reduce source current/load voltage harmonics, but did not discuss migitation of sag and interuption caused by PV penetration. Power quality enhancement of sag and source voltage harmonics on grid using UPQC supplied by PV array connected to DC link using PI compared with FLC has been done by Ramalengswara Rao, et.al. Combination of UPQC and PV using FLC can improve source voltage THD better than PI [7]. Amirullah et.al have researched a method for balancing current and line voltage, as a result of DGs of a single phase PV generator unit in randomly installed at homes through on a three phase four wire 220 kV and 50 Hz distribution line using BES and three of single phase bidirectional inverter. Both devices was capable of reduce unbalanced line current/voltage, but both of them were also capable of increase current/voltage harmonics on PCC bus [8]. Power quality migitation of UPQC on microgrid supplied by PV and wind turbine has been implemented by K S Srikanth et. al. It resulted that PI and FLC was able to improve power quality and reduce distortion in output power [9]. The UPQC-wind turbine to provide active power to overcome low sag and interruption voltage to grid has been investigated by H.Toodeji, et.al. The model was used VSC as a rectifier on generator output and controlled so that maximum power desired can be generated by different speed wind turbines using PI [10]. The UPQC-wind turbine connected to UPQC DC link was implemented by M. Hosseinpour, et al. The proposed combination using PI was capable of compensate swell, interruption voltage, and reactive power both on on/off grid [11]. R.Bhavani, et, al have researched on UPOC controlled by FLC to improve power quality in a DFIG wind turbine connected grid. FLC can improve power quality i.e. sag voltage and load current harmonics better than PI [12]. Power quality enhancement on wind turbine and BES with PI connected grid on PCC bus using UPQC has been implemented by S.RajeshRajan, et al. BES was installed to maintain and stabilize active power supply under different wind speed [13].

This research will analyze UPQC-BES performance supplied by PV-wind hybrid connected to 3P3W of 380 volt (L-L) and 50 hertz distribution system. The performance of supply system is compared with two RE sources i.e. PV and Wind, respectively. BES serves to store excess energy produced by three RE sources and distribute it to load if necessary, to prevent interruption voltage, and to adjust charging and discharging of energy in battery. BES is also expected to store excess power produced by three RE combinations and use it as backup power. FLC is proposed and compared with PI to control variable of DC voltage and DC reference voltage input to generate reference current source in current hysteresis controller on shunt active filter. DC voltage controller in shunt active filter and series active filter is used to migitate power quality of load voltage and source current.Performance of two controllers are used to determine load voltage, source current, load voltage THD, and source current THD based on IEEE 519. This paper is presented as follow. Section 2 describes proposed method, model of UPQC-BES system supplied by three RE sources i.e. PV, wind, and PV-wind hybrid, simulation parameters, PV and PMSG wind turbine model, series and shunt active filter, as well as application of PI and FLC method for proposed model. Section 3 shows results and analysis about performance of THD analysis on the proposed model of three RE sources connected to DC link of UPQC-BES system using PI and FLC. In this section, six disturbance scenarios are presented and the results are verified with Matlab/Simulink. Finally, this paper in concluded in Section 4.

2. RESEARCH METHOD

2.1. Proposed method

Figure 1 shows proposed model in this research. The RE sources based DGs used i.e. PV, Wind Turbine, and PV-Wind Turbine Hybrid connected to 3P3W distribution system with 380 volt (L-L) and 50 Hz frequency, through UPQC-BES system. PV array produce power under fixed temperature and radiation as well as connect to UPQC-DC link through a DC/DC boost converter. The maximum power point tracking (MPPT) method with Pertub and Observer (P and O) algorithms helps PV produce maximum power and generate output voltage, as the input voltage for DC/DC boost converter. The converter serves to adjust dutycycle value and output voltage of PV as its input voltage to produce an output voltage corresponding to UPQC DC link voltage. Wind turbine type used is a permanent magnetic synchronous generator (PMSG) with variable speed and fixed voltage which generating power and is connected to UPQC DC link circuit through AC/DC bridge rectifier. The rectifier helps to change AC PSMG stator output voltage to DC voltage through LC circuit that serves to filter and smooth it before connected to UPQC-DC link.BES connected to the UPQC-DC link circuit serves as energy storage and is expected to overcome interruption voltage and overall help UPQC performance to improve voltage and current quality on source and load bus. Simulation parameters proposed in this study is shown in Appendix Section. Power quality analysis is performed on PV, Wind, PV-Wind Hybrid respectively, connected to 3P3W system through UPQC DC-link (on-grid) using BES circuit. Single phase circuit breakers (CBs) are used to connect and disconnect PV, Wind, and Hybrid PV-Wind respectively with UPOC DC-link.

There are six disturbance scenarios i.e. (1) NL, (2) Unba-NL, (3) Dis-NL, (4) Sag-NL, (5) Swell-NL, and (6) Inter-NL. In scenario 1, the model is connected a non-linear load with R_L and L_L of 60 Ohm and 0.15 mH respectively. In scenario 2, the model is connected to non-linear load and during 0.3 s since t=0.2 s to t=0.5 s connected to unbalance three phase load with R1, R2, R3 as 6 Ohm, 12 Ohm, 24 Ohm respectively, and value of C1, C2, C3 as 2200 µF. In scenario 3, the model is connected to non-linear load and source voltage generating 5th and 7th harmonic components with individual harmonic distortion values of 5% and 2% respectively. In scenario 4, the model is connected to non-linear load and source experiences a sag voltage disturbance of 50% for 0.3 s between t=0.2 s to t=0.5 s. In scenario 5, the model is connected to a non-linear load and source experiences a swell voltage disturbance of 50% for 0.3 s between t=0.2 s to t=0.5 s. In scenario 6, the model is connected to non-linear load and source experiences an interruption voltage interference of 100% for 0.3 s between t=0.2 s to t=0.5 s. FLC is used as a DC voltage control in a shunt active filter to improve the power quality of the load voltage and current source and compare it with PI controller. Each disturbance scenario uses a PI controller and FLC so that the total of 12 disturbances. The result analysis of research was carried out i.e. (1) voltage and current on source or poin common coupling (PCC) bus, (2) voltage and current on load bus, (3) harmonic voltage and harmonic current on source bus and (4) harmonic voltage and harmonic current on load bus. The final phase is to compare performance of UPQC-BES system on-grid supplied by PV, Wind, PV-Wind Hybrid respectively using two controllers to improve power quality of load voltage and source current under six disturbance conditions.



Figure 1. Proposed model of UPQC-BES system supplied by PV, Wind, and PV-Wind Hybrid

2.2. Photovoltaic model

Figure 2 shows the equivalent circuit and V-I characteristic of a solar panel. A solar panel is composed of several PV cells that have series, parallel, or series-parallel external connections [14].



Figure 2. Equivalent circuit and V-I characteristic of solar panel

The V-I characteristic of a solar panel is showed in (1):

$$I = I_{PV} - I_o \left[\exp\left(\frac{V + R_s I}{aV_t}\right) - 1 \right] - \frac{V + R_s I}{R_p}$$
(1)

where I_{PV} is the photovoltaic current, I_o is saturated reverse current, 'a' is the ideal diode constant, $V_t = N_S K T q^{-1}$ is the thermal voltage, N_S is the number of series cells, q is the electron charge, K is the Boltzmann constant, T is the temperature of p–n junction, R_S and R_P are series and parallel equivalent resistance of the solar panels. I_{PV} has a linear relation with light intensity and also varies with temperature variations. I_o is dependent on temperature variations. The values of I_{pv} and I_o are calculated as following (2) and (3):

$$I_{PV} = (I_{PV,n} + K_1 \Delta T) \frac{G}{G_n} I$$
⁽²⁾

$$I_o = \frac{I_{SC,n} + K_I \Delta T}{\exp(V_{OC,n} + K_V \Delta T) / aV_t - 1}$$
(3)

In which $I_{PV,n}$, $I_{SC,n}$ and $V_{OC,n}$ are photovoltaic current, short circuit current and open circuit voltage in standard conditions ($T_n=25$ C and $G_n=1000$ Wm⁻²) respectively. K_I is the coefficient of short circuit current to temperature, $\Delta T=T-T_n$ is the temperature deviation from standard temperature, G is the light intensity and K_I is the ratio coefficient of open circuit voltage to temperature. Open circuit voltage, short circuit current and voltage-current corresponding to the maximum power are three important points of I-V characteristic of solar panel. These points are changed by variations of atmospheric conditions. By using (4) and (5) which are derived from PV model equations, short circuit current and open circuit voltage can be calculated in different atmospheric conditions.

$$I_{SC} = (I_{SC} + K_1 \Delta T) \frac{G}{G_n}$$
⁽⁴⁾

$$V_{OC} = V_{OC} + K_V \Delta T \tag{5}$$

2.3. PMSG wind turbine

Wind turbine is one of part of an integrated system, which can be divided into two types i.e. fixed and variable speed wind turbines. In fixed speed type, rotating speed of turbine is fixed and hence, frequency of generated voltage remains constant, so it can be directly connected to the network. In this case, maximum power can not always be extracted by wind. On the other hand, on variable speed, turbine can rotate at different speeds, so maximum power can be generated in each wind speed by MPPT method [10]. The advantage of using a PMSG over a synchronous generator and DFIG machine because it has high efficiency and reliability. Due to the elimination of rotor external excitation, machine size, and cost also decreases, making PMSG to be more controlled easily with feedback control system. PMSG has become an attractive solution on wind generation systems with variable speed wind turbine applications [15]. Figure 3 and 4 shows model of PMSG wind turbine and wind turbin power characteristic curve.



Figure 3. Model of PMSG wind turbine



Figure 4. Wind turbin power characteristic curve

The output power of wind turbine can be expressed using (6), (7), and (8) [11].

$$\lambda = \frac{\omega_r R}{V_{wind}} \tag{6}$$

$$P_M = \frac{1}{2} \rho \pi R^2 C_p V_{wind}^3 \tag{7}$$

$$T_{M} = \frac{P_{M}}{\omega_{r}} = \frac{1}{2} \rho \pi R^{5} C_{p} \frac{\omega_{M}^{3}}{\lambda^{3}}$$

$$\tag{8}$$

Where λ is the speed-tip ratio, V_{wind} is wind speed, R is blade radius, ω_r is rotor speed (rad/sec), ρ is the air density, C_P is the power coefficient, P_M is the output mechanical power, and T_M is output torque of wind turbine. The C_P coefficient is dependent on the pitch angle value, at which rotor blade can rotate along axis and tip-speed ratio λ expressed in (9).

$$C_p = (0.44 - 0.167\beta)\sin\frac{\pi(\lambda - 2)}{(13 - 0.3\beta)}$$
(9)

Where β is a pitch angle blade. In a fixed pitch type, the value of β is set to a fixed value.

2.4. Control of series active filter

The main function of series active filter is as a sensitive load protection against a number of voltage interference at PCC bus. The control strategy algorithm of the source and load voltage in series active filter circuit is shown in Figure 5. It extracts the unit vector templates from the distorted input supply. Furthermore, the templates are expected to be ideal sinusoidal signal with unity amplitude. The distorted supply voltages are measured and divided by peak amplitude of fundamental input voltage V_m give in (10) [6].

$$V_m = \sqrt{\frac{2}{3} \left(V_{sa}^2 + V_{sb}^2 + V_{sc}^2 \right)}$$
(10)

A three phase locked loop (PLL) is used in order to generate a sinusoidal unit vector templates with a phase lagging by the use of sinus function. The reference load voltage signal is determined by multiplying the unit vector templates with the peak amplitude of the fundamental input voltage V_m . The load reference voltage (V_{La}^* , V_{Lb}^* , V_c^*) is then compared against to sensed load voltage (V_{La} , V_{Lb} , V_{Lc}) by a pulse width modulation (PWM) controller used to generate the desired trigger signal on series active filter.



Figure 5. Control strategy of series active filter

2.5. Control of shunt active filter

The main function of shunt active filter is mitigation of power quality problems on the load side. The control methodology in shunt active filter is that the absorbed current from the PCC bus is a balanced positive sequence current including unbalanced sag voltage conditions in the PCC bus or unbalanced conditions or non-linear loads. In order to obtain satisfactory compensation caesed by disturbance due to non-linear load, many algorithms have been used in the literature. This research used instantaneous reactive power theory method "p-q theory". The voltages and currents in Cartesian *abc* coordinates can be transformed to Cartesian $\alpha\beta$ coordinates as expressed in (11) and (12) [16].

$$\begin{bmatrix} v_{\alpha} \\ v_{\beta} \end{bmatrix} = \begin{bmatrix} 1 & -1/2 & -1/2 \\ 1 & \sqrt{3}/2 & -\sqrt{3}/2 \end{bmatrix} \begin{bmatrix} V_{\alpha} \\ V_{b} \\ V_{c} \end{bmatrix}$$
(11)

$$\begin{bmatrix} i_{\alpha} \\ i_{\beta} \end{bmatrix} = \begin{bmatrix} 1 & -1/2 & -1/2 \\ 1 & \sqrt{3}/2 & -\sqrt{3}/2 \end{bmatrix} \begin{bmatrix} i_{La} \\ i_{Lb} \\ i_{Lc} \end{bmatrix}$$
(12)

The computation of the real power (p) and imaginary power (q) is showed in (13). The real power and imaginary are measured instantaneously power and in matrix it is form is given as. The presence of oscillating and average components in instantaneous power is presented in (14) [17].

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$$\begin{bmatrix} p \\ q \end{bmatrix} = \begin{bmatrix} v_{\alpha} & v_{\beta} \\ -v_{\beta} & v_{\alpha} \end{bmatrix} \begin{bmatrix} i_{\alpha} \\ i_{\beta} \end{bmatrix}$$
(13)

$$p = \overline{p} + \widetilde{p} \quad ; q = \overline{q} + \widetilde{q} \tag{14}$$

Where \overline{p} = direct component of real power, \widetilde{p} = fluctuating component of real power, \overline{q} = direct component of imaginary power, \widetilde{q} = fluctuating component of imaginary power. The total imaginary power (q) and the fluctuating component of real power are selected as power references and current references and are utilized through the use of (15) for compensating harmonic and reactive power [18].

$$\begin{bmatrix} i_{c\alpha}^{*} \\ i_{c\beta}^{*} \end{bmatrix} = \frac{1}{v_{\alpha}^{2} + v_{\beta}^{2}} \begin{bmatrix} v_{\alpha} & v_{\beta} \\ v_{\beta} & -v_{\alpha} \end{bmatrix} \begin{bmatrix} -\widetilde{p} + \overline{p}_{loss} \\ -q \end{bmatrix}$$
(15)

The signal \overline{p}_{loss} , is obtained from voltage regulator and is utilized as average real power. It can also be specified as the instantaneous active power which corresponds to the resistive loss and switching loss of the UPQC. The error obtained on comparing the actual DC-link capacitor voltage with the reference value is processed in FLC, engaged by voltage control loop as it minimizes the steady state error of the voltage across the DC link to zero. The compensating currents ($i_{c\alpha}^*$, $i_{c\beta}^*$) as required to meet the power demand of load are shown in (15). These currents are represented in α - β coordinates. The phase current is required to acquire using (16) for compensation. These source phase currents (i_{sa}^* , i_{sb}^* , i_{sc}^*) are represented in a-b-c axis obtained from the compensating current in the α - β coordinates presented in (16) [18]. Figure 6 shows a control of shunt active filter.

$$\begin{bmatrix} i_{s_{\alpha}}^{*} \\ i_{s_{b}}^{*} \\ i_{s_{c}}^{*} \end{bmatrix} = \sqrt{\frac{2}{3}} \begin{bmatrix} 1 & 0 \\ -1/2 & \sqrt{3}/2 \\ -1/2 & -\sqrt{3}/2 \end{bmatrix} \begin{bmatrix} i_{c\alpha}^{*} \\ i_{c\beta}^{*} \end{bmatrix}$$
(16)



Figure 6. Control strategy of shunt active filter

The proposed model of UPQC-BES system supplied by three RE sources is shown in Figure 1. From the figure, we can see that PV is connected to the DC link through a DC-DC boost converter circuit. The PV partially distributes power to the load and the remains is transfered to three phase grid. The load consists of non linear and unbalanced load. The non-linear load is a diode rectifier circuit with the RL load type, while the unbalanced load is a three phase RC load with different R value on each phase. In order to economically efficient, PV must always work in MPP condition. In this research, MPPT method used is P and O algorithm. The model is also applied for UPQC-BES system which is supplied by wind and PV-wind hybrid respectively. In order to operate properly, UPQC-BES system device must have a minimum DC link voltage (V_{dc}). The value of common DC link voltage depends on the nstantaneous energy avialable to UPQC is defined by in (17) [16]:

$$V_{dc} = \frac{2\sqrt{2}V_{LL}}{\sqrt{3}m} \tag{17}$$

where m is modulation index and V_{LL} is the AC grid line voltage of UPQC. Considering that modulation index as 1 and for line to line grid voltage (V_{LL} =380 volt), the V_{dc} is obtained 620, 54 volt and selected as 650 volt.

The input of shunt active filter showed in Figure 5 is DC voltage (V_{dc}) and reference DC voltage (V_{dc}^*), while the output is \bar{p}_{loss} by using PI controller. Then, the \bar{p}_{loss} is as one of input variable to generate the reference source current (I_{sa}^* , I_{sb}^* , and I_{sc}^*). The reference source current output is then compared to source current (I_{sa} , I_{sb} , and I_{sc}) by the current hysteresis control to generate trigger signal in IGBT circuit of shunt active filter. In this research, FLC as DC voltage control algorithm on shunt active filter is proposed and compared with PI controller. The FLC is capable of reduce oscilation and generate quick convergence calculation during disturbances. This method is also used to overcome the weakness of PI controller in determining proportional gain (K_p) and integral gain constant (K_i) which still use trial and error method.

2.6. Fuzzy logic controller

The research is started by determine \overline{p}_{loss} as the input variable to result the reference source current on current hysteresis controller to generate trigger signal on the IGBT shunt active filter of UPQC using PI controller (K_p=0.2 and K_i=1.5). By using the same procedure, \overline{p}_{loss} is also determined by using FLC. The FLC has been widely used in recent industrial process because it has heuristic, simpler, more effective and has multi rule based variables in both linear and non-linear system variations. The main components of FLC are fuzzification, decision making (rulebase, database, reason mechanism) and defuzzification in Figure 7. The output membership function is generated using inference blocks and the basic rules of FLC as shown in Table 1.



The fuzzy rule algorithm collects a number of fuzzy control rules in a particular order. This rule is used to control the system to meet the desired performance requirements and they are designed from a number of intelligent system control knowledge. The fuzzy inference of FLC using Mamdani method related to max-min composition. The fuzzy inference system in FLC consists of three parts: rule base, database, and reasoning mechanism [19]. The FLC method is performed by determining input variables V_{dc} (V_{dc-error}) and delta Vdc ($\Delta V_{dc-error}$), seven linguistic fuzzy sets, operation fuzzy block system (fuzzyfication, fuzzy rule base and defuzzification), $V_{dc-error}$ and $\Delta V_{dc-error}$ during fuzzification process, fuzzy rule base table, crisp value to determine \bar{p}_{loss} in defuzzification phase. The \bar{p}_{loss} is one of input variable to obtain compensating currents (i_{ca}^*, i_{cb}^*) in (16). During fuzzification process, a number of input variables are calculated and converted into linguistic variables based on a subset called membership function. The error Vdc (V_{dc-error}) and delta error Vdc ($\Delta V_{dc-error}$) are proposed input variable system and output variable is \overline{p}_{loss} . To translate these variables, each input and output variable is designed using seven membership functions: Negative Big (NB), Negative Medium (NM), Negative Small (NS), Zero (Z), Positive Small (PS), Positive Medium (PM) and Positive Big (PB). The membership functions of crisp input and output are presented with triangular and trapezoidal membership functions. The value of V_{dc-error} range from -650 to 650, $\Delta V_{dc-error}$ from -650 to 650, and \bar{p}_{lass} from -100 to 100. The input and output MFs are shown in Figure 8.


Figure 8. Membership functions (a) $V_{dc-error}$, (b) $\Delta V_{dc-error}$, and (c) \overline{p}_{lass}

After the V_{dc-error} and Δ V_{dc-error} are obtained, then two input membership functions are converted to linguistic variables and uses them as input functions for FLC. The output membership function is generated using inference blocks and the basic rules of FLC as shown in Table 1. Finally the defuzzification block operates to convert generated \overline{p}_{loss} output from linguistic to numerical variable again. Then it becomes input variable for current hysteresis controller to produce trigger signal on the IGBT circuit of UPQC shunt active filter to reduce source current and load voltage harmonics. While simultaneously, it also improve power quality of 3P3W system under six scenarios due to the integration of three RE sources to UPQC-BES system.

3. RESULTS AND ANALYSIS

The analysis of proposed model is investigated through determination of six disturbance scenarios i.e. (1) NL, (2) Unba-NL, (3) Dis-NL, (4) Sag-NL, (5) Swell-NL, and (6) Inter-NL. Each scenario of UPQC uses PI controller and FLC so total number of disturbance are 12 scenarios.By using Matlab/Simulink, the model is then executed according to the desired scenario to obtain curve of source voltage (V_s), load voltage (V_L), compensation voltage (V_c), source current (V_s), load current (I_L), and DC voltage DC link (V_{dc}). Then, THD value of source voltage, source current, load voltage, and load current in each phase as well as average THD value (Avg THD) are obtained base on the curves. THD in each phase is determined in one cycle started at t = 0.35 s. The results of average of source voltage, source current, load voltage, source current of 3P3W system using UPQC-BES system supplied by three RE sources i.e. PV, wind, and PV-wind hybrid are presented in Table 2, 3, and 4. Next THD in each phase and average THD are showed in Table 5, 6 and 7.

Table 2 shows UPQC-BES system supplied PV connected 3P3W system using PI and FLC, disturbance scenarios 1 to 5 produce an average load voltage above 307 V. While in scenario 6, FLC produces a higher average load voltage of 304.1 V than if using a PIof 286.7 V. If reviewed from average source current with PI, the highest and lowest average source currents are generated by disturbance scenarios

Matlab/simulink simulation of unified power quality conditioner-battery energy storage... (Amirullah)

2 and 4 of 28.15 A and 7,246 A. Whereas if using FLC the highest and lowest average source currents are achieved in scenario 2 and 6 of 28.84 A and 3.804 A. Table 3 shows UPQC-BES supplied by wind connected to 3P3W with PI and FLC, scenarios 1 to 5 is able to obtain a stable load voltage above 308 V. The difference is that in scenario 6, PI generates a load voltage of 274.8 V, otherwise if using FLC, load voltage increases to 306.4 V. If reviewed from source current using PI, the highest and lowest average source currents are resulted by scenarios 2 and 4 of 28.28 A and 7.417 A. Rather, if using FLC, the highest and lowest average source currents are achieved in scenario 2 and 6 of 28.82 A and 3,420 A. Table 4 shows UPQC-BES supplied PV-wind hybrid connected 3P3W using PI and FLC, scenarios 1 to 5 produce an average load voltage above 307 V. While in scenario 6, FLC generates an average load voltage 305.9 V higher than if using PI control of 283.9 V. If reviewed from average source current with PI, the highest and lowest average source currents are resulted by scenarios 2 and 4 of 28.21 A and 6,773 A. Otherwise if using FLC the highest and lowest average source currents are achieved in scenario 2 and 6 of 28.82 A and 3.640 A respectively.

Table 2. Voltage and Current of 3P3W System Using UPQC-BES System Supplied by PV

Con	So	urce Vol	tage V _S ((V)		Load Vo	ltage V _L (V)	Se	ource Cu	rrent I _S (.	A)	I	Load Cu	rent I _L (A	<i>I</i>)
Self	Ph A	Ph B	Ph C	Avg	Ph A	Ph B	Ph C	Avg	Ph A	Ph B	Ph C	Avg	Ph A	Ph B	Ph C	Avg
							PI	Controlle	er							
1	309.6	309.6	309.6	309.6	307.6	307.8	307.7	307.7	7.766	7.793	7.759	7.773	8.528	8.529	8.533	8.530
2	307.4	308.0	308.0	307.8	308.3	308.7	308.3	308.4	31.00	24.84	28.73	28.15	22.50	34.12	34.52	30.38
3	309.6	309.6	309.6	309.6	313,8	314.3	317.4	317.4	7.897	7.919	7.867	7.895	8.748	8.704	8.785	8.746
4	154.5	154.5	154.5	154.5	307.1	307.3	307.3	307.2	7.235	7.276	7.226	7.246	8.509	8.514	8.510	8.511
5	464.7	464.7	464.7	464.7	308.6	308.7	308.6	308.6	7.979	7.980	7.964	7.975	8.550	8.553	8.554	8.553
6	0.536	1.385	0.850	0.924	310.2	259.8	290.2	286.7	7.392	12.67	6.045	8.703	8.707	7.747	7.637	8.031
							Fuzzy l	Logic Cor	troller							
1	309.5	309.5	309.5	309.5	307.7	307.9	307.7	307.8	8.420	8.426	8.416	8.421	8.527	8.532	8.531	8.530
2	307.4	307.9	308.0	307.8	308.5	308.7	308.4	308.5	31.66	25.50	29.36	28.84	22.52	34.11	35.52	30.72
3	309.6	309.5	309.5	309.5	313.4	312.9	315.9	314.1	8.516	8.565	8.496	8.526	8.741	8.677	8.736	8.718
4	154.4	154.4	154.4	154.4	307.3	307.3	307.2	307.3	8.563	8.560	8.561	8.561	8.514	8.517	8.512	8.515
5	464.6	464.6	464.6	464.6	308.6	308.8	308.6	308.7	8.396	8.389	8.389	8.392	8.552	8.556	8.554	8.554
6	0.447	0.392	0.380	0.407	314.0	293.4	304.9	304.1	4.024	3.778	3.608	3.804	8.874	8.195	8.193	8.421

Table 3. Voltage and Current of 3P3W System Using UPQC-BES System Supplied by Wind

C	So	urce Vol	tage Vs (V)	L	oad Volt	age V _L (V	V)	Se	ource Cu	rrent Is (A	A)		Load Curr	ent I _L (A)	
SCII	Ph A	Ph B	Ph C	Avg	Ph A	Ph B	Ph C	Avg	Ph A	Ph B	Ph C	Avg	Ph A	Ph B	Ph C	Avg
								PI Cont	roller							
1	309.5	309.6	309.6	309.6	308.6	308.6	308.2	308.5	7.863	7.875	7.840	7.869	8.554	8.553	8.546	8.551
2	307.4	308.0	308.0	308.0	308.9	309.2	308.7	308.9	31.07	24.97	28.81	28.28	22.55	34.17	34.57	30.43
3	309.6	309.5	309.6	309.6	312.9	312.9	315.4	313.8	7.993	8.015	7.947	7.985	8.817	8.682	8.741	8.747
4	154.5	154.5	154.5	154.5	308.0	308.1	307.8	307.9	7.428	7.455	7.368	7.417	8.527	8.535	8.532	8.531
5	464.7	464.7	464.7	464.7	309.3	309.3	309.0	309.2	8.015	8.020	8.002	8.012	8.564	8.573	8.568	8.568
6	1.256	1.022	0.592	0.957	234.0	316.4	274.0	274.8	11.27	9.866	7.028	9.388	5.958	8.697	8.204	7.619
							Fuz	zy Logic	Controll	er						
1	309.5	309.5	309.5	309.5	308.5	308.6	308.3	308.5	8.418	8.410	8.414	8.414	8.545	8.552	8.549	8.549
2	307.4	307.9	308.0	307.8	309.0	309.3	308.9	309.1	31.64	25.47	29.34	28.82	22.56	34.18	34.59	30.44
3	309.5	309.5	309.5	309.5	313.2	313.7	314.1	313.7	8.519	8.531	8.531	8.527	8.713	8.714	8.718	8.715
4	154.4	154.4	154.4	154.4	308.0	308.1	307.7	307.9	8.557	8.539	8.561	8.552	8.528	8.541	8.525	8.531
5	464.6	464.7	464.7	464.7	309.2	309.3	309.2	309.2	8.391	8.385	8.388	8.388	8.565	8.570	8.567	8.567
6	0.357	0.396	0.397	0.383	303.7	300.0	315.3	306.4	3.358	3.464	3.542	3.420	8.557	8.418	8.731	8.569

Table 4. Voltage and Current of 3P3W System Using UPQC-BES System Supplied PV-Wind Hybrid

Son	So	urce Vol	tage V _S (V)	Lo	oad Volta	ge V _L (V)	Se	ource Cu	rrent I _S (A	A)	I	load Curi	rent I _L (A	.)
SCII	Ph A	Ph B	Ph C	Avg	Ph A	Ph B	Ph C	Avg	Ph A	Ph B	Ph C	Avg	Ph A	Ph B	Ph C	Avg
							PI	Controll	er							
1	309.6	309.6	309.6	309.6	307.8	308.0	307.7	307.8	7.790	7.802	7.770	7.787	8.527	8.537	8.533	8.533
2	307.4	308.0	308.0	307.8	308.4	308.8	308.4	308.6	31.02	24.87	28.74	28.21	22.52	34.13	34.53	31.40
3	309.6	309.5	309.6	309.6	314.0	315.5	316.9	315.5	7.942	7.939	7.918	7.933	8.739	8.750	8.783	8.757
4	154.5	154.5	154.5	154.5	307.3	307.4	307.2	307.3	7.289	7.309	7.251	7.283	8.513	8.516	8.515	8.515
5	464.7	464.7	464.7	464.7	308.7	308.9	308.7	308.8	7.985	7.985	7.975	7.982	8.552	8.558	8.558	8.556
6	1.048	0.825	0.845	0.906	247.5	300.7	303.7	283.9	5.119	5.927	9.271	6.773	7.016	7.893	8.793	7.867
							Fuzzy I	logic Con	ntroller							
1	309.5	309.5	309.5	309.5	307.8	308.0	307.7	307.8	8.419	8.418	8.409	8.413	8.529	8.539	8.533	8.534
2	307.4	307.9	308.0	307.8	308.7	308.7	308.9	308.8	31.66	25.47	29.32	28.82	22.54	34.13	34.56	30.41
3	309.5	309.5	309.5	309.5	314.4	315.5	316.6	315.5	8.581	8.593	8.568	8.581	8.761	8.722	8.761	8.748
4	154.4	154.4	154.4	154.4	307.3	307.5	307.3	307.4	8.566	8.572	8.563	8.567	8.511	8.520	8.519	8.517
5	464.6	464.6	464.6	464.6	308.8	308.8	308.7	308.8	8.391	8.394	8.396	8.394	22.33	22.35	22.36	22.35
6	0.412	0.403	0.402	0.418	311.6	295.7	310.4	305.9	3.774	3.544	3.593	3.640	8.855	8.321	8.288	8.488

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		Ta	ble 5.	Harm	onics	of 3P3	W Sys	stem U	sing UF	QC-BE	ES Syste	em Supp	olied b	y PV		
C	Sou	rce Volta	ge THD ((%)	Lo	ad Voltag	ge THD ((%)	Se	ource Curr	ent THD (%)		Load Cu	rrent (%)	
Scii	Ph A	Ph B	Ph C	Avg	Ph A	Ph B	Ph C	Avg	Ph A	Ph B	Ph C	Avg	Ph A	Ph B	Ph C	Avg
								PI Co	ntroller							
1	2.35	2.36	2.32	2.34	2.48	2.50	2.46	2.48	12.89	12.72	12.92	12.84	22.32	22.34	22.32	22.33
2	2.29	2.20	2.24	2.24	2.43	2.23	2.37	2.34	2.660	2.330	2.240	2.410	5.230	2.070	2.660	3.320
3	5.84	5.86	5.94	5.88	6.36	5.90	6.58	6.28	12.75	12.64	13.06	12.82	21.92	22.16	22.33	22.14
4	4.69	4.75	4.81	4.75	2.46	2.48	2.53	2.49	14.26	13.96	14.16	14.13	22.28	22.31	22.28	22.29
5	1.56	1.53	1.55	1.55	2.47	2.43	2.45	2.45	12.51	12.36	12.44	12.44	22.34	22.32	22.32	22.33
6	NA	NA	NA	NA	32.11	15.09	28.54	25.25	270.90	145.89	275.67	230.82	47.70	34.58	36.29	39.53
							F	uzzy Log	ic Controll	ler						
1	2.35	2.33	2.35	2.34	2.48	2.46	2.49	2.47	11.83	11.82	11.84	11.83	22.33	22.32	22.33	22.33
2	2.25	2.27	2.20	2.24	2.39	2.41	2.34	2.38	2.620	2.400	2.220	2.413	5.230	2.100	2.640	3.323
3	5.83	5.88	5.93	5.88	6.23	5.93	6.69	6.28	11.83	11.90	12.14	11.96	21.84	22.34	22.53	22.24
4	4.71	4.76	4.79	4.75	2.46	2.48	2.50	2.48	11.91	11.88	11.86	11.89	22.27	22.32	22.32	22.31
5	1.55	1.54	1.54	1.54	2.45	2.44	2.46	2.45	11.90	11.84	11.85	11.86	22.36	22.33	22.35	22.35
6	NA	NA	NA	NA	13.05	6.60	11.15	10.27	30.61	34.72	31.57	32.30	24.25	24.25	24.71	24.40

Table 6. Harmonics of 3P3W System Using UPQC-BES System Supplied by Wind

Con	Sour	ce Volta	ge THD	(%)	Lo	ad Volta	ge THD ((%)	Sc	ource Curr	ent THD (9	%)		Load Cu	rrent (%)	
SCII	Ph A	Ph B	Ph C	Avg	Ph A	Ph B	Ph C	Avg	Ph A	Ph B	Ph C	Avg	Ph A	Ph B	Ph C	Avg
								PI Cor	ntroller							
1	1.88	1.87	1.94	1.89	1.99	1.97	2.05	2.00	12.63	12.37	12.70	12.57	12.30	12.30	12.34	12.31
2	1.83	1.76	1.82	1.80	1.92	1.85	1.93	1.90	2.460	2.070	2.200	2.240	5.260	2.070	2.690	3.340
3	5.67	5.71	5.77	5.72	6.00	6.83	6.02	6.28	12.48	12.26	12.66	12.47	22.01	22.12	22.08	22.07
4	3.76	3.86	3.86	1.83	1.97	2.02	2.03	2.01	13.59	13.17	13.51	13.42	22.29	22.31	22.30	22.30
5	1.26	1.24	1.29	1.26	1.99	1.97	2.05	2.00	12.31	12.20	12.31	12.27	22.36	22.33	22.37	22.35
6	NA	NA	NA	NA	14.09	35.59	34.73	28.14	157.76	139.01	266.07	186.95	37.60	34.39	46.97	39.65
							Fι	ızzy Logi	c Controll	er						
1	1.89	1.88	1.93	1.90	1.99	1.98	2.04	2.00	11.71	11.72	11.77	11.73	22.34	22.31	22.32	22.32
2	1.85	1.79	1.78	1.81	1.95	1.87	1.88	1.90	2.43	2.11	2.12	2.220	5.240	2.070	2.700	3.240
3	5.67	5.71	5.78	5.72	5.99	6.39	6.13	6.17	11.72	11.62	11.90	11.75	22.08	21.94	22.47	22.16
4	3.79	3.81	3.86	3.82	1.97	1.99	2.03	1.99	11.72	11.69	11.74	11.72	22.28	22.30	22.35	22.31
5	1.27	1.24	1.28	1.26	2.00	1.96	2.04	2.00	11.66	11.76	11.76	11.73	22.31	22.33	22.35	22.33
6	NA	NA	NA	NA	7.59	6.44	10.95	8.33	27.33	28.27	26.39	27.33	25.39	23.65	24.31	24.45

Table 7. Harmonics of 3P3W System Using UPQC-BES System Supplied by PV-Wind Hybrid

								-	-		-					
Son	Sour	rce Voltag	ge THD	(%)	Loa	d Voltag	e THD (9	%)	Sc	ource Curre	ent THD (%)		Load Cu	rrent (%)	
Self	Ph A	Ph B	Ph C	Avg	Ph A	Ph B	Ph C	Avg	Ph A	Ph B	Ph C	Avg	Ph A	Ph B	Ph C	Avg
								PI Co	ntroller							
1	2.25	2.19	2.29	2.24	2.37	2.31	2.42	3.37	12.85	12.62	12.74	12.74	22.33	22.31	22.34	22.33
2	2.18	2.08	2.15	2.13	2.30	2.19	2.18	2.22	2.630	2.300	2.290	2.407	5.230	2.070	2.670	3.323
3	5.81	5.82	5.89	5.84	6.12	5.88	6.75	6.25	12.71	12.63	12.98	12.77	22.05	22.13	22.54	22.24
4	4.53	4.48	4.51	4.51	2.37	2.35	2.37	2.36	14.16	13.50	13.99	13.88	22.27	22.30	22.28	22.28
5	1.49	1.46	1.51	1.49	2.37	2.31	2.40	2.36	12.43	12.29	12.41	12.38	22.34	22.32	22.33	22.33
6	NA	NA	NA	NA	18.61	36.38	28.42	27.8	387.71	330.34	189.29	302.45	36.73	38.51	36.83	37.36
							Fuz	zy Log	ic Control	ler						
1	2.25	2.23	2.25	2.24	2.37	2.35	2.39	2.37	11.85	11.74	11.84	11.81	22.32	22.31	22.33	22.32
2	2.23	2.15	2.05	2.14	2.37	2.26	2.17	2.26	2.520	2.410	2.140	2.446	5.230	2.070	2.690	3.330
3	5.80	5.83	5.90	5.84	6.57	5.26	7.06	6.29	11.83	11.78	12.24	11.95	22.15	22.23	22.95	22.44
4	4.53	4.52	4.54	4.86	2.36	2.35	2.35	2.35	11.79	11.74	11.84	11.79	22.29	22.30	22.29	22.29
5	1.48	1.46	1.51	1.48	2.35	2.32	2.40	2.35	11.78	11.81	11.81	11.80	22.33	22.35	22.36	22.35
6	NA	NA	NA	NA	10.30	4.90	10.25	8.48	27.44	29.52	28.63	28.53	23.20	23.97	24.65	23.94

Table 5 shows that average THD of load voltage (V_L) of UPQC-BES system supplied by PV in 3P3W system for scenarios 1 to 5 using PI control is within limits in IEEE 519. The highest and lowest average THD load voltages are achieved under scenario 6 and 2 as 25.25% and 2.34% respectively. PI controller is also able to mitigation average THD source voltage in scenario 6 from not accessible (NA) to 25.25% on the load side. The highest and lowest average THD of source current are achieved in scenario 6 and 2 as 230.82% and 2.41%. Table 5 also indicates that average THD of load voltage of UPQC system supplied by PV with BES using FLC in scenarios 1 to 5, has fulfilled limits in IEEE 519. The highest and lowest average THD of load voltage are achieved under scenario 6 and 2 of 10.27% and 2.38%. The use of FLC method is also able to reduce average THD on source voltage in scenario 6 from NA to 10.27% on load side. The highest and lowest average THD of source current are achieved in scenario 6 and 2 of 32.30% and 2.413%.

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Table 6 shows that average THD of load voltage of UPQC-BES system supplied by wind in 3P3W system for interference scenarios 1 to 5 using PI is within limits prescribed in IEEE 519. The highest and lowest average THD load voltages is achieved under scenario 6 and scenario 2 as 28.14% and 1.90% respectively. PI controller is also able to reduce average THD source voltage in scenario 6 from NA to 28.14% on the load side. The highest and lowest average THD of source current are achieved in scenario 6 and 2 as 186.95% and 2.24% respectively. Table 6 also shows that average THD of load voltage of UPQC-BES supplied by wind using FLC in scenarios 1 to 5, has fulfilled limits prescribed in IEEE 519. The highest and lowest average THD of load voltage are achieved under scenario 6 and 4 of 8.33% and 1.90%. FLC method is also able to reduce average THD on source voltage in scenario 6 from NA to 7.33% on load side. The highest and lowest average THD source current are achieved in scenario 6 and 2 of 27.33% and 2.22%.

Table 7 shows that average THD of load voltage (V_L) of UPQC-BES system supplied by PV-wind hybrid in 3P3W system for scenarios 1 to 5 using PI is within limits in IEEE 519. The highest and lowest average THD load voltages are achieved under scenario 6 and 2 as 27.8% and 2.22% respectively. PI is also able to mitigate average THD source voltage in scenario 6 from NA to 27.8% on load side. The highest and lowest average THD of source current are achieved in scenario 6and 2 as 302.45% and 2.407% respectively. Table 7 also indicates that average THD of load voltage of UPQC-BES system supplied by PV-wind hybrid using FLC for scenarios 1 to 5, has fulfilled limits in IEEE 519. The highest and lowest average THD of load voltage are achieved under scenario 6 and 2 of 8.48% and 2.26%. FLC method is also able to reduce average THD on source voltage in scenario 6 from NA to 8.48% on load side. The highest and lowest average THD of source current are achieved in scenario 5 and 2 of 28.53% and 2.446%. Overall for UPQC-BES systemsystem supplied by three RE sources in scenarios 1 to 5 using PI and FLC is able to improve average THD of source current better on average THD of load current. Figure 9 presents UPQC-BES system performance supplied by three RE sources using FLC in scenario 6.

Figure 9 a(i) shows that in scenario 6, UPQC-BES system supplied by PV at t=0.2 s to t=0.5 s, average source voltage (V_S) falls as 100% to 0.4062 V. During the disturbance, PV is able to generate power to UPQC DC link and injecting full average compensation voltage (V_c) in Figure 9 a(iii) through injection transformer on series active filter so that average load voltage (VL) in Figure 9 a(ii) remains stable at 304.1 V. As long as fault period, although nominal of average source current (I_s) in Figure 9 a(iv) drops to 3.804 A, combination of PV and BES is able to generate power, store excess energy of PV, and inject current into load through shunt active filter so that average load current (IL) in Figure 9 a(v) remains as 8.421 A. Figure 9 b(i) presents on UPQC-BES supplied by wind at t=0.2 s to t=0.5 s average source voltage (Vs) drops 100% to 0.3828 V. During the disturbance, wind is able to generate power to UPQC DC link and injecting full average compensation voltage (V_C) in Figure 9 b(iii) through injection transformer on series active filter so that average load voltage (V_L) in Figure 9 b(ii) remains stable at 306.4 V. During fault period, although nominal of average source current (Is) falls to 3.420 A, combination of wind and BES is able to generate power, store excess energy of wind, and inject current into load through shunt active filter so that average load current (I₁) in Figure 9 b(v) remains as 8.569 A. Figure 9 c(i) indicates on UPQC-BES supplied by PV-Wind Hybrid at t=0.2 s to t=0.5 s average source voltage (V_s) drops 100% to 0.4175 V. During the disturbance, PV-wind hybrid is able to generate power to UPQC DC link and injecting full average compensation voltage (V_c) in Figure 9 c(iii) through injection transformer on series active filter so that average load voltage (V_L) in Figure 9 b(ii) remains stable at 305.9 V. As long as disturbance period, although nominal of average source current (Is) falls to 3.640 A, combination of PV-wind hybrid and BES is able to generate power, store excess energy of wind, and inject current into load through shunt active filter so that average load current (I_L) in Figure 9 c(v) remains as 8.488 A.

Figure 10 shows spectra of load voltage harmonics on phase A of UPQC-BES system supplied by three RE sources using FLC in scenario 6. Figure 11 shows performance of average THD of load voltage and source current on UPQC-BES system supplied by three RE sources. Figure 11(a) shows that in scenario 1 to 5, the implementation of FLC on UPQC-BES system supplied by three RE sources is able to obtain average THD of load voltage slightly better than PI controller and both method have already met the limit in IEEE 519. Further under scenario 6, FLC applied on UPQC-BES system supplied by three RE sources gives significantly better result of average THD of load voltage than PI controller. In six disturbance scenarios, both PI controller and FLC applied on UPQC-BES system supplied by three RE sources, PV is able to obtain the highest average THD of load voltages. Figure 11(b) shows that in disturbance scenario 1 to 5, implementation of FLC on UPQC-BES system supplied by three RE sources is able to obtain average THD of source current slightly better than PI controller. Furthermore under scenario 6, FLC applied on UPQC-BES system supplied by three RE sources is able to obtain average THD of source current slightly better than PI controller. Furthermore under scenario 6, FLC applied on UPQC-BES system supplied by three RE sources is able to obtain average THD of source current slightly better than PI controller. Furthermore under scenario 6, FLC applied on UPQC-BES system supplied by three RE sources is able to obtain average THD of source current than PI controller. Both PI controller and FLC on UPQC-BES system supplied by three RE sources in six disturbance scenarios, PV is able to obtain the highest average THD of source current.



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Figure 9. UPQC-BES system performance using FLC in scenario 6 (Inter-NL): (a) UPQC-BES + PV; (b) UPQC-BES + Wind; (c) UPQC-BES + PV-Wind Hybrid







(a) Average load voltage harmonics



(b) Average source current harmonics

Figure 11. Performance of UPQC-BES supplied by three RE sources using PI and FLC

4. CONCLUSION

Comparative performance analysis of UPQC-BES system supplied by three RE sources i.e. PV, wind, and PV-wind hybrid respectively using PI controller and FLC have been discussed. In disturbance scenario 1 to 5, implementation of FLC on UPQC-BES system supplied by three RE sources is able to obtain average THD of load voltage slightly better than PI and both methods have already met the limit in IEEE 519. Under scenario 6, FLC applied on UPQC-BES system supplied by three RE sources gives significantly better result average THD of load voltage than PI. In six disturbance scenarios, both PI and FLC applied on UPQC-BES system supplied by three RE sources is able to obtain the highest average THD of load voltage. In interference scenario 1 to 5, FLC method on UPQC-BES system supplied by three RE sources is able to obtain average THD of source current slightly better than PI. Furthermore under scenario 6, FLC applied on UPQC-BES system supplied by three RE sources gives significantly better result of average THD of source current slightly better than PI. Furthermore under scenario 6, FLC applied on UPQC-BES system supplied by three RE sources gives significantly better result of average THD of source current slightly better than PI. Furthermore under scenario 6, FLC applied on UPQC-BES system supplied by three RE sources gives significantly better result of average THD of source current than PI. Both PI and FLC on UPQC-BES system supplied by three RE sources in six scenarios, PV is able to obtain the highest average THD of source current.

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APPENDIX

Three phase grid: RMS voltage 380 volt (L-L), 50 Hz, line impedance: $R_s=0.1$ Ohm $L_s=15$ mH; series and shunt active filter: series inductance $L_{se}=0.015$ mH; shunt inductance $L_{sh}=15$ mH; injection transformers: rating 10 kVA, 50 Hz, turn ratio $(N_1/N_2)=1:1$; non linear load: resistance $R_L=60$ ohm, inductance $L_L=0.15$ mH, load impedance $R_c=0.4$ ohm and $L_c=15$ mH; unbalance load: resistance $R_1=24$ ohm, $R_2=12$ ohm, and $R_3=6$ ohm, capacitance $C_1, C_2, C_3=2200 \ \mu\text{F}$; DC-link: voltage $V_{DC}=650$ volt and capacitance $C_{DC}=3000 \ \mu\text{F}$; battery energe storage: type=nickel metal hybrid, DC voltage=650 volt, rated capacity= 200 Ah, initial SOC=100%, inductance $L_1=6$ mH, capacitance $C_1=200 \ \mu\text{F}$; photovoltaic: active power= 0.6 kW temperature=25° C, irradiance=1000 W/m²; PMSG wind turbine active power=0.6 kW, voltage= 380 volt, 50 Hz, wind speed=5 m/s, picth angle=2; PI controller: $K_p=0.2$, $K_i=1.5$; fuzzy model: method= mamdani, composition=max-min; input membership function: error (V_{dc})=trapmf, trimf delta error (ΔV_{dc})= trapmf, trimf; output membership function: \overline{p}_{loss} =trapmf,trimf.

BIOGRAPHIES OF AUTHORS



Amirullah was born in Sampang East Java Indonesia, in 1977. He received bachelor and master degree in electrical engineering from University of Brawijaya Malang and ITS Surabaya, in 2000 and 2008, respectively. He also worked as a lecturer in University of Bhayangkara Surabaya. He is currently working toward the doctoral degree, in electrical engineering in Power System and Simulation Laboratory (PSSL) ITS Surabaya. His research interest includes power distribution modeling and simulation, power quality, harmonics migitation, design of filter/PFC, and RE.



Ontoseno Penangsang was born in Madiun East Java Indonesia, in 1949. He received bachelor degree in electrical engineering from ITS Surabaya, in 1974. He received M.Sc and Ph.D degree in Power System Analysis from University of Wisconsin, Madison, USA, in 1979 and 1983, respectively. He is currently a professor at Department of Electrical Engineering and the head of PSSL ITS Surabaya. He has a long experience and main interest in power system analysis (with renewable energy sources), design of power distribution, power quality, and harmonic mitigation in industry.



Adi Soeprijanto was born in Lumajang East Java Indonesia, in 1964. He received bachelor in electrical engineering from ITB Bandung, in 1988. He received master of electrical engineering in control automatic from ITB Bandung. He continued his study to Doctoral Program in Power System Control in Hiroshima University Japan and was finished it's in 2001. He is currently a professor at Department of Electrical Engineering and member of PSSL in ITS Surabaya. His main interest includes power system analysis, power system stability control, and power system dynamic stability. He had already achieved a patent in optimum operation of power system.

Lampiran 2.10 Makalah Camera Ready

Matlab/simulink simulation of unified power quality conditioner-battery energy storage system supplied by PV-wind hybrid using fuzzy logic controller

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Article Info

ABSTRACT

Article history:	This paper presents performance analysis of Unified Power Quality
Received May 2, 2018 Revised Nov 11, 2018 Accepted Dec 2, 2018	Photovoltaic (PV)-Wind Hybrid connected to three phase three wire (3P3W) of 380 volt (L-L) and 50 hertz distribution system. The performance of supply system is compared with two renewable energy (RE) sources i.e. PV and Wind, respectively. Fuzzy Logic Controller (FLC) is implemented to maintain
Keywords:	DC voltage across the capacitor under disturbance scenarios of source and load as well as to compare the results with Proportional Integral (PI) controller.
Battery energy storage Photovoltaic Power quality PV-Wind Hybrid Total harmonic distortion UPQC Wind turbine	There are six scenarios of disturbance i.e. (1) non-linear load (NL), (2) unbalance and nonlinear load (Unba-NL), (3) distortion supply and non-linear load (Dis-NL), (4) sag and non-linear load (Sag-NL), (5) swell and non-linear load (Swell-NL), and (6) interruption and non-linear load (Inter-NL). In disturbance scenario 1 to 5, implementation of FLC on UPQC-BES system supplied by three RE sources is able to obtain average THD of load voltage/source current slightly better than PI. Furthermore under scenario 6, FLC applied on UPQC-BES system supplied by three RE sources gives significantly better result of average THD of load voltage/source current than PI. This research is simulated using Matlab/Simulink.
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1. INTRODUCTION

PV and wind are the most RE distributed generations (DGs) because they are able to convert sunlight and wind into power. PV and solar are the potential DGs sources since it only need sunlight to generate electricity, where the resources are available in abundance, free and relatively clean. Indonesia has enormous energy potential from the sun because it lies on the equator. Almost all areas of Indonesia get sunlight about 10 to 12 hours per day, with an average intensity of irradiation of 4.5 kWh/m² or equivalent to 112.000 GW. The potential of wind energy in Indonesia generally has a speed between 4 to 5 m/s and classified as medium scale with potential capacity of 10 to 100 kW. The weakness of PV and wind turbine besides able to generate power, they also produces a number voltage and current harmonics resulted by presence of several types of PV and wind turbine devices and power converters as well as to increase a number of non-linear loads connected to the grid, so finally resulting in the decrease in power quality.

In order to overcome and improve power quality due to presence of non-linear loads and integration of PV and wind turbine to grid, UPQC is a proposed. UPQC serves to compensate for source voltage quality problemsi.e. sag, swell unbalance, flicker, harmonics, and load current quality problems i.e. harmonics,

unbalance, reactive currents, and neutral current. B. Han et. al and Vinod Khadkikar have investigated UPQC as one part of active power filter consisting of shunt and series active filters connected in parallel and serves as superior controller to overcome a number of power quality problems simultaneously. Series component has been responsible for reducing a number of interference on source side i.e. voltage sag/swell, flicker, unbalanced voltage, and harmonics. Shunt component has been responsible for addressing a current quality problems i.e. low power factor, load current harmonics, and unbalanced load. [1, 2]. UPQC based on RE has been investigated by some researchers. There are two methods used to overcome this problem i.e. using conventional and artificial intelligence. Shafiuzzaman K.K., et.al have proposed system includes a series inverter, shunt inverter, and a DG connected to a DC link through a rectifier using PI. The system was capable of increase source voltage quality i.e. sag and interruption and load current quality, as well as transfer of active power on/off grid mode [3]. The influence of DG on UPQC performance in reducing sag under conditions of some phase to ground faults to using DSTATCOM has been implemented by Norshafinash S., et.al. The DG was effective enough to help UPQC to improve sag [4]. It was connected in series with load resulting better sag mitigation compared to system without DG. Implementation of UPQC using UVTG method with PI to reduce sag, swell, voltage/current harmonics has been doneby S. N. Gohil, et.al. Simulation of voltage distortion was made by adding 5th and 7th harmonics at fundamental source voltage, resulting in a reduction of THD source current and THD load voltage [5].

UPQC supplied by PV panels using boost converter, PI, MPPT P and O, and p-q theory has been proposed by Yahia Bouzelata at.al [6]. The system was capable of compensate reactive power and reduce source current/load voltage harmonics, but did not discuss migitation of sag and interuption caused by PV penetration. Power quality enhancement of sag and source voltage harmonics on grid using UPQC supplied by PV array connected to DC link using PI compared with FLC has been done by Ramalengswara Rao, et.al. Combination of UPQC and PV using FLC can improve source voltage THD better than PI [7]. Amirullah et.al have researched a method for balancing current and line voltage, as a result of DGs of a single phase PV generator unit in randomly installed at homes through on a three phase four wire 220 kV and 50 Hz distribution line using BES and three of single phase bidirectional inverter. Both devices was capable of reduce unbalanced line current/voltage, but both of them were also capable of increase current/voltage harmonics on PCC bus [8]. Power quality migitation of UPQC on microgrid supplied by PV and wind turbine has been implemented by K S Srikanth et. al. It resulted that PI and FLC was able to improve power quality and reduce distortion in output power [9]. The UPQC-wind turbine to provide active power to overcome low sag and interruption voltage to grid has been investigated by H.Toodeji, et.al. The model was used VSC as a rectifier on generator output and controlled so that maximum power desired can be generated by different speed wind turbines using PI [10]. The UPQC-wind turbine connected to UPQC DC link was implemented by M. Hosseinpour, et al. The proposed combination using PI was capable of compensate swell, interruption voltage, and reactive power both on on/off grid [11]. R.Bhavani, et, al have researched on UPOC controlled by FLC to improve power quality in a DFIG wind turbine connected grid. FLC can improve power quality i.e. sag voltage and load current harmonics better than PI [12]. Power quality enhancement on wind turbine and BES with PI connected grid on PCC bus using UPQC has been implemented by S.RajeshRajan, et al. BES was installed to maintain and stabilize active power supply under different wind speed [13].

This research will analyze UPQC-BES performance supplied by PV-wind hybrid connected to 3P3W of 380 volt (L-L) and 50 hertz distribution system. The performance of supply system is compared with two RE sources i.e. PV and Wind, respectively. BES serves to store excess energy produced by three RE sources and distribute it to load if necessary, to prevent interruption voltage, and to adjust charging and discharging of energy in battery. BES is also expected to store excess power produced by three RE combinations and use it as backup power. FLC is proposed and compared with PI to control variable of DC voltage and DC reference voltage input to generate reference current source in current hysteresis controller on shunt active filter. DC voltage controller in shunt active filter and series active filter is used to migitate power quality of load voltage and source current.Performance of two controllers are used to determine load voltage, source current, load voltage THD, and source current THD based on IEEE 519. This paper is presented as follow. Section 2 describes proposed method, model of UPQC-BES system supplied by three RE sources i.e. PV, wind, and PV-wind hybrid, simulation parameters, PV and PMSG wind turbine model, series and shunt active filter, as well as application of PI and FLC method for proposed model. Section 3 shows results and analysis about performance of THD analysis on the proposed model of three RE sources connected to DC link of UPQC-BES system using PI and FLC. In this section, six disturbance scenarios are presented and the results are verified with Matlab/Simulink. Finally, this paper in concluded in Section 4.

2. RESEARCH METHOD

2.1. Proposed method

Figure 1 shows proposed model in this research. The RE sources based DGs used i.e. PV, Wind Turbine, and PV-Wind Turbine Hybrid connected to 3P3W distribution system with 380 volt (L-L) and 50 Hz frequency, through UPQC-BES system. PV array produce power under fixed temperature and radiation as well as connect to UPQC-DC link through a DC/DC boost converter. The maximum power point tracking (MPPT) method with Pertub and Observer (P and O) algorithms helps PV produce maximum power and generate output voltage, as the input voltage for DC/DC boost converter. The converter serves to adjust duty-cycle value and output voltage of PV as its input voltage to produce an output voltage corresponding to UPQC DC link voltage. Wind turbine type used is a permanent magnetic synchronous generator (PMSG) with variable speed and fixed voltage which generating power and is connected to UPQC DC link circuit through AC/DC bridge rectifier. The rectifier helps to change AC PSMG stator output voltage to DC voltage through LC circuit that serves to filter and smooth it before connected to UPQC-DC link.BES connected to the UPQC-DC link circuit serves as energy storage and is expected to overcome interruption voltage and overall help UPQC performance to improve voltage and current quality on source and load bus. Simulation parameters proposed in this study is shown in Appendix Section. Power quality analysis is performed on PV, Wind, PV-Wind Hybrid respectively, connected to 3P3W system through UPQC DC-link (on-grid) using BES circuit. Single phase circuit breakers (CBs) are used to connect and disconnect PV, Wind, and Hybrid PV-Wind respectively with UPOC DC-link.

There are six disturbance scenarios i.e. (1) NL, (2) Unba-NL, (3) Dis-NL, (4) Sag-NL, (5) Swell-NL, and (6) Inter-NL. In scenario 1, the model is connected a non-linear load with $R_{\rm L}$ and $L_{\rm L}$ of 60 Ohm and 0.15 mH respectively. In scenario 2, the model is connected to non-linear load and during 0.3 s since t=0.2 s to t=0.5s connected to unbalance three phase load with R₁, R₂, R₃ as 6 Ohm, 12 Ohm, 24 Ohm respectively, and value of C_1 , C_2 , C_3 as 2200 μ F. In scenario 3, the model is connected to non-linear load and source voltage generating 5th and 7th harmonic components with individual harmonic distortion values of 5% and 2% respectively. In scenario 4, the model is connected to non-linear load and source experiences a sag voltage disturbance of 50% for 0.3 s between t=0.2 s to t=0.5 s. In scenario 5, the model is connected to a non-linear load and source experiences a swell voltage disturbance of 50% for 0.3 s between t=0.2 s to t=0.5 s. In scenario 6, the model is connected to non-linear load and source experiences an interruption voltage interference of 100% for 0.3 s between t=0.2 s to t=0.5 s. FLC is used as a DC voltage control in a shunt active filter to improve the power quality of the load voltage and current source and compare it with PI controller. Each disturbance scenario uses a PI controller and FLC so that the total of 12 disturbances. The result analysis of research was carried out i.e. (1) voltage and current on source or poin common coupling (PCC) bus, (2) voltage and current on load bus, (3) harmonic voltage and harmonic current on source bus and (4) harmonic voltage and harmonic current on load bus. The final phase is to compare performance of UPQC-BES system on-grid supplied by PV, Wind, PV-Wind Hybrid respectively using two controllers to improve power quality of load voltage and source current under six disturbance conditions.



Figure 1. Proposed model of UPQC-BES system supplied by PV, Wind, and PV-Wind Hybrid Matlab/simulink simulation of unified power quality conditioner-battery energy storage... (Amirullah)

2.2. Photovoltaic model

Figure 2 shows the equivalent circuit and V-I characteristic of a solar panel. A solar panel is composed of several PV cells that have series, parallel, or series-parallel external connections [14].



Figure 2. Equivalent circuit and V-I characteristic of solar panel

The V-I characteristic of a solar panel is showed in (1):

$$I = I_{PV} - I_o \left[\exp\left(\frac{V + R_s I}{aV_t}\right) - 1 \right] - \frac{V + R_s I}{R_p}$$
(1)

where I_{PV} is the photovoltaic current, I_o is saturated reverse current, 'a' is the ideal diode constant, $V_t = N_S K T q^{-1}$ is the thermal voltage, N_S is the number of series cells, q is the electron charge, K is the Boltzmann constant, T is the temperature of p–n junction, R_S and R_P are series and parallel equivalent resistance of the solar panels. I_{PV} has a linear relation with light intensity and also varies with temperature variations. I_o is dependent on temperature variations. The values of I_{pv} and I_o are calculated as following (2) and (3):

$$I_{PV} = (I_{PV,n} + K_1 \Delta T) \frac{G}{G_n} I$$
⁽²⁾

$$I_o = \frac{I_{SC,n} + K_I \Delta T}{\exp(V_{OC,n} + K_V \Delta T) / aV_I - 1}$$
(3)

In which $I_{PV,n}$, $I_{SC,n}$ and $V_{OC,n}$ are photovoltaic current, short circuit current and open circuit voltage in standard conditions ($T_n=25$ C and $G_n=1000$ Wm⁻²) respectively. K_I is the coefficient of short circuit current to temperature, $\Delta T=T-T_n$ is the temperature deviation from standard temperature, G is the light intensity and K_V is the ratio coefficient of open circuit voltage to temperature. Open circuit voltage, short circuit current and voltage-current corresponding to the maximum power are three important points of I-V characteristic of solar panel. These points are changed by variations of atmospheric conditions. By using (4) and (5) which are derived from PV model equations, short circuit current and open circuit voltage can be calculated in different atmospheric conditions.

$$I_{SC} = (I_{SC} + K_1 \Delta T) \frac{G}{G_n}$$
(4)

$$V_{OC} = V_{OC} + K_V \Delta T \tag{5}$$

2.3. PMSG wind turbine

Wind turbine is one of part of an integrated system, which can be divided into two types i.e. fixed and variable speed wind turbines. In fixed speed type, rotating speed of turbine is fixed and hence, frequency of generated voltage remains constant, so it can be directly connected to the network. In this case, maximum power can not always be extracted by wind. On the other hand, on variable speed, turbine can rotate at different speeds, so maximum power can be generated in each wind speed by MPPT method [10]. The advantage of

using a PMSG over a synchronous generator and DFIG machine because it has high efficiency and reliability. Due to the elimination of rotor external excitation, machine size, and cost also decreases, making PMSG to be more controlled easily with feedback control system. PMSG has become an attractive solution on wind generation systems with variable speed wind turbine applications [15]. Figure 3 and 4 shows model of PMSG wind turbine and wind turbin power characteristic curve.



Figure 3. Model of PMSG wind turbine



Figure 4. Wind turbin power characteristic curve

The output power of wind turbine can be expressed using (6), (7), and (8) [11].

$$\lambda = \frac{\omega_r R}{V_{wind}} \tag{6}$$

$$P_{M} = \frac{1}{2} \rho \pi R^{2} C_{p} V_{wind}^{3}$$

$$\tag{7}$$

$$T_{M} = \frac{P_{M}}{\omega_{r}} = \frac{1}{2} \rho \pi R^{5} C_{p} \frac{\omega_{M}^{3}}{\lambda^{3}}$$

$$\tag{8}$$

Where λ is the speed-tip ratio, V_{wind} is wind speed, R is blade radius, ω_r is rotor speed (rad/sec), ρ is the air density, C_P is the power coefficient, P_M is the output mechanical power, and T_M is output torque of wind turbine. The C_P coefficient is dependent on the pitch angle value, at which rotor blade can rotate along axis and tip-speed ratio λ expressed in (9).

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$$C_{p} = (0.44 - 0.167\beta)\sin\frac{\pi(\lambda - 2)}{(13 - 0.3\beta)}$$
(9)

Where β is a pitch angle blade. In a fixed pitch type, the value of β is set to a fixed value.

2.4. Control of series active filter

The main function of series active filter is as a sensitive load protection against a number of voltage interference at PCC bus. The control strategy algorithm of the source and load voltage in series active filter circuit is shown in Figure 5. It extracts the unit vector templates from the distorted input supply. Furthermore, the templates are expected to be ideal sinusoidal signal with unity amplitude. The distorted supply voltages are measured and divided by peak amplitude of fundamental input voltage V_m give in (10) [6].

$$V_m = \sqrt{\frac{2}{3} \left(V_{sa}^2 + V_{sb}^2 + V_{sc}^2 \right)}$$
(10)

A three phase locked loop (PLL) is used in order to generate a sinusoidal unit vector templates with a phase lagging by the use of sinus function. The reference load voltage signal is determined by multiplying the unit vector templates with the peak amplitude of the fundamental input voltage V_m . The load reference voltage $(V_{La}^*, V_{Lb}^*, V_c^*)$ is then compared against to sensed load voltage (V_{La}, V_{Lb}, V_{Lc}) by a pulse width modulation (PWM) controller used to generate the desired trigger signal on series active filter.



Figure 5. Control strategy of series active filter

2.5. Control of shunt active filter

The main function of shunt active filter is mitigation of power quality problems on the load side. The control methodology in shunt active filter is that the absorbed current from the PCC bus is a balanced positive sequence current including unbalanced sag voltage conditions in the PCC bus or unbalanced conditions or non-linear loads. In order to obtain satisfactory compensation caesed by disturbance due to non-linear load, many algorithms have been used in the literature. This research used instantaneous reactive power theory method "p-q theory". The voltages and currents in Cartesian *abc* coordinates can be transformed to Cartesian $\alpha\beta$ coordinates as expressed in (11) and (12) [16].

$$\begin{bmatrix} v_{\alpha} \\ v_{\beta} \end{bmatrix} = \begin{bmatrix} 1 & -1/2 & -1/2 \\ 1 & \sqrt{3}/2 & -\sqrt{3}/2 \end{bmatrix} \begin{bmatrix} V_{a} \\ V_{b} \\ V_{c} \end{bmatrix}$$
(11)

$$\begin{bmatrix} i_{\alpha} \\ i_{\beta} \end{bmatrix} = \begin{bmatrix} 1 & -1/2 & -1/2 \\ 1 & \sqrt{3}/2 & -\sqrt{3}/2 \end{bmatrix} \begin{bmatrix} i_{La} \\ i_{Lb} \\ i_{Lc} \end{bmatrix}$$
(12)

The computation of the real power (p) and imaginary power (q) is showed in (13). The real power and imaginary are measured instantaneously power and in matrix it is form is given as. The presence of oscillating and average components in instantaneous power is presented in (14) [17].

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$$\begin{bmatrix} p \\ q \end{bmatrix} = \begin{bmatrix} v_{\alpha} & v_{\beta} \\ -v_{\beta} & v_{\alpha} \end{bmatrix} \begin{bmatrix} i_{\alpha} \\ i_{\beta} \end{bmatrix}$$
(13)

$$p = \overline{p} + \widetilde{p} \quad ; q = \overline{q} + \widetilde{q} \tag{14}$$

Where \bar{p} = direct component of real power, \tilde{p} = fluctuating component of real power, \bar{q} = direct component of imaginary power, \tilde{q} = fluctuating component of imaginary power. The total imaginary power (q) and the fluctuating component of real power are selected as power references and current references and are utilized through the use of (15) for compensating harmonic and reactive power [18].

$$\begin{bmatrix} i_{c\alpha}^{*} \\ i_{c\beta}^{*} \end{bmatrix} = \frac{1}{v_{\alpha}^{2} + v_{\beta}^{2}} \begin{bmatrix} v_{\alpha} & v_{\beta} \\ v_{\beta} & -v_{\alpha} \end{bmatrix} \begin{bmatrix} -\widetilde{p} + \overline{p}_{loss} \\ -q \end{bmatrix}$$
(15)

The signal \overline{p}_{loss} , is obtained from voltage regulator and is utilized as average real power. It can also be specified as the instantaneous active power which corresponds to the resistive loss and switching loss of the UPQC. The error obtained on comparing the actual DC-link capacitor voltage with the reference value is processed in FLC, engaged by voltage control loop as it minimizes the steady state error of the voltage across the DC link to zero. The compensating currents ($i_{c\alpha}^*$, $i_{c\beta}^*$) as required to meet the power demand of load are shown in (15). These currents are represented in α - β coordinates. The phase current is required to acquire using (16) for compensation. These source phase currents (i_{sa}^* , i_{sb}^* , i_{sc}^*) are represented in a-b-c axis obtained from the compensating current in the α - β coordinates presented in (16) [18]. Figure 6 shows a control of shunt active filter.

$$\begin{bmatrix} i_{sa}^{*} \\ i_{sb}^{*} \\ i_{sc}^{*} \end{bmatrix} = \sqrt{\frac{2}{3}} \begin{bmatrix} 1 & 0 \\ -1/2 & \sqrt{3}/2 \\ -1/2 & -\sqrt{3}/2 \end{bmatrix} \begin{bmatrix} i_{c\alpha}^{*} \\ i_{c\beta}^{*} \end{bmatrix}$$
(16)



Figure 6. Control strategy of shunt active filter

The proposed model of UPQC-BES system supplied by three RE sources is shown in Figure 1. From the figure, we can see that PV is connected to the DC link through a DC-DC boost converter circuit. The PV partially distributes power to the load and the remains is transfered to three phase grid. The load consists of non linear and unbalanced load. The non-linear load is a diode rectifier circuit with the RL load type, while the unbalanced load is a three phase RC load with different R value on each phase. In order to economically efficient, PV must always work in MPP condition. In this research, MPPT method used is P and O algorithm. The model is also applied for UPQC-BES system which is supplied by wind and PV-wind hybrid respectively. In order to operate properly, UPQC-BES system device must have a minimum DC link voltage (V_{dc}). The value of common DC link voltage depends on the nstantaneous energy avialable to UPQC is defined by in (17) [16]:

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$$V_{dc} = \frac{2\sqrt{2}V_{LL}}{\sqrt{3}m} \tag{17}$$

where m is modulation index and V_{LL} is the AC grid line voltage of UPQC. Considering that modulation index as 1 and for line to line grid voltage (V_{LL} =380 volt), the V_{dc} is obtained 620, 54 volt and selected as 650 volt.

The input of shunt active filter showed in Figure 5 is DC voltage (V_{dc}) and reference DC voltage (V_{dc}^*), while the output is \bar{p}_{loss} by using PI controller. Then, the \bar{p}_{loss} is as one of input variable to generate the reference source current (I_{sa}^* , I_{sb}^* , and I_{sc}^*). The reference source current output is then compared to source current (I_{sa} , I_{sb} , and I_{sc}) by the current hysteresis control to generate trigger signal in IGBT circuit of shunt active filter. In this research, FLC as DC voltage control algorithm on shunt active filter is proposed and compared with PI controller. The FLC is capable of reduce oscilation and generate quick convergence calculation during disturbances. This method is also used to overcome the weakness of PI controller in determining proportional gain (K_p) and integral gain constant (K_i) which still use trial and error method.

2.6. Fuzzy logic controller

The research is started by determine \overline{p}_{loss} as the input variable to result the reference source current on current hysteresis controller to generate trigger signal on the IGBT shunt active filter of UPQC using PI controller (K_p=0.2 and K_i=1.5). By using the same procedure, \overline{p}_{loss} is also determined by using FLC. The FLC has been widely used in recent industrial process because it has heuristic, simpler, more effective and has multi rule based variables in both linear and non-linear system variations. The main components of FLC are fuzzification, decision making (rulebase, database, reason mechanism) and defuzzification in Figure 7. The output membership function is generated using inference blocks and the basic rules of FLC as shown in Table 1.



The fuzzy rule algorithm collects a number of fuzzy control rules in a particular order. This rule is used to control the system to meet the desired performance requirements and they are designed from a number of intelligent system control knowledge. The fuzzy inference of FLC using Mamdani method related to max-min composition. The fuzzy inference system in FLC consists of three parts: rule base, database, and reasoning mechanism [19]. The FLC method is performed by determining input variables V_{dc} (V_{dc-error}) and delta Vdc $(\Delta V_{dc-error})$, seven linguistic fuzzy sets, operation fuzzy block system (fuzzyfication, fuzzy rule base and defuzzification), $V_{dc-error}$ and $\Delta V_{dc-error}$ during fuzzification process, fuzzy rule base table, crisp value to determine \overline{p}_{loss} in defuzzification phase. The \overline{p}_{loss} is one of input variable to obtain compensating currents $(i_{ca}^*, i_{c\beta}^*)$ in (16). During fuzzification process, a number of input variables are calculated and converted into linguistic variables based on a subset called membership function. The error Vdc (V_{dc-error}) and delta error Vdc $(\Delta V_{dc-error})$ are proposed input variable system and output variable is \bar{p}_{loss} . To translate these variables, each input and output variable is designed using seven membership functions: Negative Big (NB), Negative Medium (NM), Negative Small (NS), Zero (Z), Positive Small (PS), Positive Medium (PM) and Positive Big (PB). The membership functions of crisp input and output are presented with triangular and trapezoidal membership functions. The value of V_{dc-error} range from -650 to 650, $\Delta V_{dc-error}$ from -650 to 650, and \overline{p}_{loss} from -100 to 100. The input and output MFs are shown in Figure 8.



Figure 8. Membership functions (a) $V_{dc-error}$, (b) $\Delta V_{dc-error}$, and (c) \overline{p}_{lass}

After the V_{dc-error} and Δ V_{dc-error} are obtained, then two input membership functions are converted to linguistic variables and uses them as input functions for FLC. The output membership function is generated using inference blocks and the basic rules of FLC as shown in Table 1. Finally the defuzzification block operates to convert generated \bar{p}_{loss} output from linguistic to numerical variable again. Then it becomes input variable for current hysteresis controller to produce trigger signal on the IGBT circuit of UPQC shunt active filter to reduce source current and load voltage harmonics. While simultaneously, it also improve power quality of 3P3W system under six scenarios due to the integration of three RE sources to UPQC-BES system.

3. RESULTS AND ANALYSIS

The analysis of proposed model is investigated through determination of six disturbance scenarios i.e. (1) NL, (2) Unba-NL, (3) Dis-NL, (4) Sag-NL, (5) Swell-NL, and (6) Inter-NL. Each scenario of UPQC uses PI controller and FLC so total number of disturbance are 12 scenarios. By using Matlab/Simulink, the model is then executed according to the desired scenario to obtain curve of source voltage (V_s), load voltage (V_L), compensation voltage (V_c), source current (V_s), load current (I_L), and DC voltage DC link (V_{dc}). Then, THD value of source voltage, source current, load voltage, and load current in each phase as well as average THD value (Avg THD) are obtained base on the curves. THD in each phase is determined in one cycle started at t = 0.35 s. The results of average of source voltage, source current, load voltage, and load current of 3P3W system using UPQC-BES system supplied by three RE sources i.e. PV, wind, and PV-wind hybrid are presented in Table 2, 3, and 4. Next THD in each phase and average THD are showed in Table 5, 6 and 7.

Table 2 shows UPQC-BES system supplied PV connected 3P3W system using PI and FLC, disturbance scenarios 1 to 5 produce an average load voltage above 307 V. While in scenario 6, FLC produces a higher average load voltage of 304.1 V than if using a PIof 286.7 V. If reviewed from average source current with PI, the highest and lowest average source currents are generated by disturbance scenarios 2 and 4 of 28.15

A and 7,246 A. Whereas if using FLC the highest and lowest average source currents are achieved in scenario 2 and 6 of 28.84 A and 3.804 A. Table 3 shows UPQC-BES supplied by wind connected to 3P3W with PI and FLC, scenarios 1 to 5 is able to obtain a stable load voltage above 308 V. The difference is that in scenario 6, PI generates a load voltage of 274.8 V, otherwise if using FLC, load voltage increases to 306.4 V. If reviewed from source current using PI, the highest and lowest average source currents are resulted by scenarios 2 and 4 of 28.28 A and 7.417 A. Rather, if using FLC, the highest and lowest average source currents are achieved in scenario 2 and 6 of 28.82 A and 3,420 A. Table 4 shows UPQC-BES supplied PV-wind hybrid connected 3P3W using PI and FLC, scenarios 1 to 5 produce an average load voltage above 307 V. While in scenario 6, FLC generates an average load voltage 305.9 V higher than if using PI control of 283.9 V. If reviewed from average source current with PI, the highest and lowest average source currents are resulted by scenarios 2 and 4 of 28.21 A and 6,773 A. Otherwise if using FLC the highest and lowest average source currents are achieved in scenario 2 and 6 of 28.82 A and 3.640 A respectively.

Table 2. Voltage and Current of 3P3W System Using UPQC-BES System Supplied by PV

							2		U	· ·		2	11	2		
Can	So	urce Vol	tage V _S ((V)		Load Vo	ltage V _L (V)	Se	ource Cu	rrent I _S (.	A)	1	Load Cu	rent I _L (A	A)
Sch	Ph A	Ph B	Ph C	Avg	Ph A	Ph B	Ph C	Avg	Ph A	Ph B	Ph C	Avg	Ph A	Ph B	Ph C	Avg
							PI	Controlle	er							
1	309.6	309.6	309.6	309.6	307.6	307.8	307.7	307.7	7.766	7.793	7.759	7.773	8.528	8.529	8.533	8.530
2	307.4	308.0	308.0	307.8	308.3	308.7	308.3	308.4	31.00	24.84	28.73	28.15	22.50	34.12	34.52	30.38
3	309.6	309.6	309.6	309.6	313,8	314.3	317.4	317.4	7.897	7.919	7.867	7.895	8.748	8.704	8.785	8.746
4	154.5	154.5	154.5	154.5	307.1	307.3	307.3	307.2	7.235	7.276	7.226	7.246	8.509	8.514	8.510	8.511
5	464.7	464.7	464.7	464.7	308.6	308.7	308.6	308.6	7.979	7.980	7.964	7.975	8.550	8.553	8.554	8.553
6	0.536	1.385	0.850	0.924	310.2	259.8	290.2	286.7	7.392	12.67	6.045	8.703	8.707	7.747	7.637	8.031
							Fuzzy l	Logic Con	troller							
1	309.5	309.5	309.5	309.5	307.7	307.9	307.7	307.8	8.420	8.426	8.416	8.421	8.527	8.532	8.531	8.530
2	307.4	307.9	308.0	307.8	308.5	308.7	308.4	308.5	31.66	25.50	29.36	28.84	22.52	34.11	35.52	30.72
3	309.6	309.5	309.5	309.5	313.4	312.9	315.9	314.1	8.516	8.565	8.496	8.526	8.741	8.677	8.736	8.718
4	154.4	154.4	154.4	154.4	307.3	307.3	307.2	307.3	8.563	8.560	8.561	8.561	8.514	8.517	8.512	8.515
5	464.6	464.6	464.6	464.6	308.6	308.8	308.6	308.7	8.396	8.389	8.389	8.392	8.552	8.556	8.554	8.554
6	0.447	0.392	0.380	0.407	314.0	293.4	304.9	304.1	4.024	3.778	3.608	3.804	8.874	8.195	8.193	8.421

Table 3. Voltage and Current of 3P3W System Using UPQC-BES System Supplied by Wind

San	So	urce Vol	tage Vs (V)	L	oad Volt	age V _L (V	/)	Se	ource Cu	rrent Is (A	A)		Load Curr	ent I _L (A)	
SCII	Ph A	Ph B	Ph C	Avg	Ph A	Ph B	Ph C	Avg	Ph A	Ph B	Ph C	Avg	Ph A	Ph B	Ph C	Avg
								PI Cont	roller							
1	309.5	309.6	309.6	309.6	308.6	308.6	308.2	308.5	7.863	7.875	7.840	7.869	8.554	8.553	8.546	8.551
2	307.4	308.0	308.0	308.0	308.9	309.2	308.7	308.9	31.07	24.97	28.81	28.28	22.55	34.17	34.57	30.43
3	309.6	309.5	309.6	309.6	312.9	312.9	315.4	313.8	7.993	8.015	7.947	7.985	8.817	8.682	8.741	8.747
4	154.5	154.5	154.5	154.5	308.0	308.1	307.8	307.9	7.428	7.455	7.368	7.417	8.527	8.535	8.532	8.531
5	464.7	464.7	464.7	464.7	309.3	309.3	309.0	309.2	8.015	8.020	8.002	8.012	8.564	8.573	8.568	8.568
6	1.256	1.022	0.592	0.957	234.0	316.4	274.0	274.8	11.27	9.866	7.028	9.388	5.958	8.697	8.204	7.619
							Fuz	zy Logic	Controll	er						
1	309.5	309.5	309.5	309.5	308.5	308.6	308.3	308.5	8.418	8.410	8.414	8.414	8.545	8.552	8.549	8.549
2	307.4	307.9	308.0	307.8	309.0	309.3	308.9	309.1	31.64	25.47	29.34	28.82	22.56	34.18	34.59	30.44
3	309.5	309.5	309.5	309.5	313.2	313.7	314.1	313.7	8.519	8.531	8.531	8.527	8.713	8.714	8.718	8.715
4	154.4	154.4	154.4	154.4	308.0	308.1	307.7	307.9	8.557	8.539	8.561	8.552	8.528	8.541	8.525	8.531
5	464.6	464.7	464.7	464.7	309.2	309.3	309.2	309.2	8.391	8.385	8.388	8.388	8.565	8.570	8.567	8.567
6	0.357	0.396	0.397	0.383	303.7	300.0	315.3	306.4	3.358	3.464	3.542	3.420	8.557	8.418	8.731	8.569

Table 4. Voltage and Current of 3P3W System Using UPQC-BES System Supplied PV-Wind Hybrid

Con	So	urce Vol	tage V _S (V)	Lo	oad Volta	ge V _L (V)	Sc	ource Cu	rrent I _S (A	A)	Ι	.oad Cur	rent I _L (A	.)
SCII	Ph A	Ph B	Ph C	Avg	Ph A	Ph B	Ph C	Avg	Ph A	Ph B	Ph C	Avg	Ph A	Ph B	Ph C	Avg
							PI	Controll	er							
1	309.6	309.6	309.6	309.6	307.8	308.0	307.7	307.8	7.790	7.802	7.770	7.787	8.527	8.537	8.533	8.533
2	307.4	308.0	308.0	307.8	308.4	308.8	308.4	308.6	31.02	24.87	28.74	28.21	22.52	34.13	34.53	31.40
3	309.6	309.5	309.6	309.6	314.0	315.5	316.9	315.5	7.942	7.939	7.918	7.933	8.739	8.750	8.783	8.757
4	154.5	154.5	154.5	154.5	307.3	307.4	307.2	307.3	7.289	7.309	7.251	7.283	8.513	8.516	8.515	8.515
5	464.7	464.7	464.7	464.7	308.7	308.9	308.7	308.8	7.985	7.985	7.975	7.982	8.552	8.558	8.558	8.556
6	1.048	0.825	0.845	0.906	247.5	300.7	303.7	283.9	5.119	5.927	9.271	6.773	7.016	7.893	8.793	7.867
							Fuzzy I	logic Co	ntroller							
1	309.5	309.5	309.5	309.5	307.8	308.0	307.7	307.8	8.419	8.418	8.409	8.413	8.529	8.539	8.533	8.534
2	307.4	307.9	308.0	307.8	308.7	308.7	308.9	308.8	31.66	25.47	29.32	28.82	22.54	34.13	34.56	30.41
3	309.5	309.5	309.5	309.5	314.4	315.5	316.6	315.5	8.581	8.593	8.568	8.581	8.761	8.722	8.761	8.748
4	154.4	154.4	154.4	154.4	307.3	307.5	307.3	307.4	8.566	8.572	8.563	8.567	8.511	8.520	8.519	8.517
5	464.6	464.6	464.6	464.6	308.8	308.8	308.7	308.8	8.391	8.394	8.396	8.394	22.33	22.35	22.36	22.35
6	0.412	0.403	0.402	0.418	311.6	295.7	310.4	305.9	3.774	3.544	3.593	3.640	8.855	8.321	8.288	8.488

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		Ta	ble 5. I	Harm	onics	of 3P3	W Sys	stem U	sing UF	PQC-BE	ES Syste	em Supp	olied b	y PV		
G	Sou	ce Volta	ge THD ((%)	Loa	ad Voltag	ge THD ((%)	Se	ource Curr	ent THD (9	%)		Load Cu	rrent (%)	
Scii	Ph A	Ph B	Ph C	Avg	Ph A	Ph B	Ph C	Avg	Ph A	Ph B	Ph C	Avg	Ph A	Ph B	Ph C	Avg
								PI Co	ntroller							
1	2.35	2.36	2.32	2.34	2.48	2.50	2.46	2.48	12.89	12.72	12.92	12.84	22.32	22.34	22.32	22.33
2	2.29	2.20	2.24	2.24	2.43	2.23	2.37	2.34	2.660	2.330	2.240	2.410	5.230	2.070	2.660	3.320
3	5.84	5.86	5.94	5.88	6.36	5.90	6.58	6.28	12.75	12.64	13.06	12.82	21.92	22.16	22.33	22.14
4	4.69	4.75	4.81	4.75	2.46	2.48	2.53	2.49	14.26	13.96	14.16	14.13	22.28	22.31	22.28	22.29
5	1.56	1.53	1.55	1.55	2.47	2.43	2.45	2.45	12.51	12.36	12.44	12.44	22.34	22.32	22.32	22.33
6	NA	NA	NA	NA	32.11	15.09	28.54	25.25	270.90	145.89	275.67	230.82	47.70	34.58	36.29	39.53
							F	uzzy Log	ic Controll	er						
1	2.35	2.33	2.35	2.34	2.48	2.46	2.49	2.47	11.83	11.82	11.84	11.83	22.33	22.32	22.33	22.33
2	2.25	2.27	2.20	2.24	2.39	2.41	2.34	2.38	2.620	2.400	2.220	2.413	5.230	2.100	2.640	3.323
3	5.83	5.88	5.93	5.88	6.23	5.93	6.69	6.28	11.83	11.90	12.14	11.96	21.84	22.34	22.53	22.24
4	4.71	4.76	4.79	4.75	2.46	2.48	2.50	2.48	11.91	11.88	11.86	11.89	22.27	22.32	22.32	22.31
5	1.55	1.54	1.54	1.54	2.45	2.44	2.46	2.45	11.90	11.84	11.85	11.86	22.36	22.33	22.35	22.35
6	NA	NA	NA	NA	13.05	6.60	11.15	10.27	30.61	34.72	31.57	32.30	24.25	24.25	24.71	24.40

Table 6. Harmonics of 3P3W System Using UPQC-BES System Supplied by Wind

Son	Sour	ce Volta	ge THD	(%)	Lo	ad Voltag	ge THD ((%)	Sc	ource Curr	ent THD (9	%)		Load Cu	rrent (%)	
SCII	Ph A	Ph B	Ph C	Avg	Ph A	Ph B	Ph C	Avg	Ph A	Ph B	Ph C	Avg	Ph A	Ph B	Ph C	Avg
								PI Co	ntroller							
1	1.88	1.87	1.94	1.89	1.99	1.97	2.05	2.00	12.63	12.37	12.70	12.57	12.30	12.30	12.34	12.31
2	1.83	1.76	1.82	1.80	1.92	1.85	1.93	1.90	2.460	2.070	2.200	2.240	5.260	2.070	2.690	3.340
3	5.67	5.71	5.77	5.72	6.00	6.83	6.02	6.28	12.48	12.26	12.66	12.47	22.01	22.12	22.08	22.07
4	3.76	3.86	3.86	1.83	1.97	2.02	2.03	2.01	13.59	13.17	13.51	13.42	22.29	22.31	22.30	22.30
5	1.26	1.24	1.29	1.26	1.99	1.97	2.05	2.00	12.31	12.20	12.31	12.27	22.36	22.33	22.37	22.35
6	NA	NA	NA	NA	14.09	35.59	34.73	28.14	157.76	139.01	266.07	186.95	37.60	34.39	46.97	39.65
							Fι	ızzy Logi	c Controll	er						
1	1.89	1.88	1.93	1.90	1.99	1.98	2.04	2.00	11.71	11.72	11.77	11.73	22.34	22.31	22.32	22.32
2	1.85	1.79	1.78	1.81	1.95	1.87	1.88	1.90	2.43	2.11	2.12	2.220	5.240	2.070	2.700	3.240
3	5.67	5.71	5.78	5.72	5.99	6.39	6.13	6.17	11.72	11.62	11.90	11.75	22.08	21.94	22.47	22.16
4	3.79	3.81	3.86	3.82	1.97	1.99	2.03	1.99	11.72	11.69	11.74	11.72	22.28	22.30	22.35	22.31
5	1.27	1.24	1.28	1.26	2.00	1.96	2.04	2.00	11.66	11.76	11.76	11.73	22.31	22.33	22.35	22.33
6	NA	NA	NA	NA	7.59	6.44	10.95	8.33	27.33	28.27	26.39	27.33	25.39	23.65	24.31	24.45

Table 7. Harmonics of 3P3W System Using UPQC-BES System Supplied by PV-Wind Hybrid

Scn	Source Voltage THD (%)				Load Voltage THD (%)				Source Current THD (%)				Load Current (%)			
	Ph A	Ph B	Ph C	Avg	Ph A	Ph B	Ph C	Avg	Ph A	Ph B	Ph C	Avg	Ph A	Ph B	Ph C	Avg
PI Controller																
1	2.25	2.19	2.29	2.24	2.37	2.31	2.42	3.37	12.85	12.62	12.74	12.74	22.33	22.31	22.34	22.33
2	2.18	2.08	2.15	2.13	2.30	2.19	2.18	2.22	2.630	2.300	2.290	2.407	5.230	2.070	2.670	3.323
3	5.81	5.82	5.89	5.84	6.12	5.88	6.75	6.25	12.71	12.63	12.98	12.77	22.05	22.13	22.54	22.24
4	4.53	4.48	4.51	4.51	2.37	2.35	2.37	2.36	14.16	13.50	13.99	13.88	22.27	22.30	22.28	22.28
5	1.49	1.46	1.51	1.49	2.37	2.31	2.40	2.36	12.43	12.29	12.41	12.38	22.34	22.32	22.33	22.33
6	NA	NA	NA	NA	18.61	36.38	28.42	27.8	387.71	330.34	189.29	302.45	36.73	38.51	36.83	37.36
Fuzzy Logic Controller																
1	2.25	2.23	2.25	2.24	2.37	2.35	2.39	2.37	11.85	11.74	11.84	11.81	22.32	22.31	22.33	22.32
2	2.23	2.15	2.05	2.14	2.37	2.26	2.17	2.26	2.520	2.410	2.140	2.446	5.230	2.070	2.690	3.330
3	5.80	5.83	5.90	5.84	6.57	5.26	7.06	6.29	11.83	11.78	12.24	11.95	22.15	22.23	22.95	22.44
4	4.53	4.52	4.54	4.86	2.36	2.35	2.35	2.35	11.79	11.74	11.84	11.79	22.29	22.30	22.29	22.29
5	1.48	1.46	1.51	1.48	2.35	2.32	2.40	2.35	11.78	11.81	11.81	11.80	22.33	22.35	22.36	22.35
6	NA	NA	NA	NA	10.30	4.90	10.25	8.48	27.44	29.52	28.63	28.53	23.20	23.97	24.65	23.94

Table 5 shows that average THD of load voltage (V_L) of UPQC-BES system supplied by PV in 3P3W system for scenarios 1 to 5 using PI control is within limits in IEEE 519. The highest and lowest average THD load voltages are achieved under scenario 6 and 2 as 25.25% and 2.34% respectively. PI controller is also able to mitigate average THD source voltage in scenario 6 from not accessible (NA) to 25.25% on the load side. The highest and lowest average THD of source current are achieved in scenario 6 and 2 as 230.82% and 2.41%. Table 5 also indicates that average THD of load voltage of UPQC system supplied by PV with BES using FLC in scenarios 1 to 5, has fulfilled limits in IEEE 519. The highest and lowest average THD of load voltage are achieved under scenario 6 and 2 of 10.27% and 2.38%. The use of FLC method is also able to reduce average THD of source current are achieved in the highest and lowest average THD of source of 32.30% and 2.413%.

Table 6 shows that average THD of load voltage of UPQC-BES system supplied by wind in 3P3W system for interference scenarios 1 to 5 using PI is within limits prescribed in IEEE 519. The highest and lowest

average THD load voltages is achieved under scenario 6 and scenario 2 as 28.14% and 1.90% respectively. PI controller is also able to reduce average THD source voltage in scenario 6 from NA to 28.14% on the load side. The highest and lowest average THD of source current are achieved in scenario 6 and 2 as 186.95% and 2.24% respectively. Table 6 also shows that average THD of load voltage of UPQC-BES supplied by wind using FLC in scenarios 1 to 5, has fulfilled limits prescribed in IEEE 519. The highest and lowest average THD of load voltage are achieved under scenario 6 and 4of 8.33% and 1.90%. FLC method is also able to reduce average THD on source voltage in scenario 6 from NA to 7.33% on load side. The highest and lowest average THD source current are achieved in scenario 6 and 2 of 27.33% and 2.22%.

Table 7 shows that average THD of load voltage (V_L) of UPQC-BES system supplied by PV-wind hybrid in 3P3W system for scenarios 1 to 5 using PI is within limits in IEEE 519. The highest and lowest average THD load voltages are achieved under scenario 6 and 2 as 27.8% and 2.22% respectively. PI is also able to mitigate average THD source voltage in scenario 6 from NA to 27.8% on load side. The highest and lowest average THD of source current are achieved in scenario 6and 2 as 302.45% and 2.407% respectively. Table 7 also indicates that average THD of load voltage of UPQC-BES system supplied by PV-wind hybrid using FLC for scenarios 1 to 5, has fulfilled limits in IEEE 519. The highest and lowest average THD of load voltage are achieved under scenario 6 and 2 of 8.48% and 2.26%. FLC method is also able to reduce average THD on source voltage in scenario 6 from NA to 8.48% on load side. The highest and lowest average THD of source current are achieved in scenario 6 and 2 of 28.53% and 2.446%. Overall for UPQC-BES systemsystem supplied by three RE sources in scenarios 1 to 5 using PI and FLC is able to improve average THD of source current better on average THD of load current. Figure 9 presents UPQC-BES system performance supplied by three RE sources using FLC in scenario 6.

Figure 9 a(i) shows that in scenario 6, UPQC-BES system supplied by PV at t=0.2 s to t=0.5 s, average source voltage (V_s) falls as 100% to 0.4062 V. During the disturbance, PV is able to generate power to UPQC DC link and injecting full average compensation voltage (V_c) in Figure 9 a(iii) through injection transformer on series active filter so that average load voltage (VL) in Figure 9 a(ii) remains stable at 304.1 V. As long as fault period, although nominal of average source current (I_S) in Figure 9 a(iv) drops to 3.804 A, combination of PV and BES is able to generate power, store excess energy of PV, and inject current into load through shunt active filter so that average load current (I_L) in Figure 9 a(v) remains as 8.421 A. Figure 9 b(i) presents on UPQC-BES supplied by wind at t=0.2 s to t=0.5 s average source voltage (V_s) drops 100% to 0.3828 V. During the disturbance, wind is able to generate power to UPQC DC link and injecting full average compensation voltage (V_C) in Figure 9 b(iii) through injection transformer on series active filter so that average load voltage (V_L) in Figure 9 b(ii) remains stable at 306.4 V. During fault period, although nominal of average source current (Is) falls to 3.420 A, combination of wind and BES is able to generate power, store excess energy of wind, and inject current into load through shunt active filter so that average load current (I₁) in Figure 9 b(y) remains as 8.569 A. Figure 9 c(i) indicates on UPOC-BES supplied by PV-Wind Hybrid at t=0.2 s to t=0.5 s average source voltage (V_s) drops 100% to 0.4175 V. During the disturbance, PV-wind hybrid is able to generate power to UPQC DC link and injecting full average compensation voltage (V_c) in Figure 9 c(iii) through injection transformer on series active filter so that average load voltage (V_L) in Figure 9 b(ii) remains stable at 305.9 V. As long as disturbance period, although nominal of average source current (I_s) falls to 3.640 A, combination of PV-wind hybrid and BES is able to generate power, store excess energy of wind, and inject current into load through shunt active filter so that average load current (I_L) in Figure 9 c(v) remains as 8.488 A.

Figure 10 shows spectra of load voltage harmonics on phase A of UPQC-BES system supplied by three RE sources using FLC in scenario 6. Figure 11 shows performance of average THD of load voltage and source current on UPQC-BES system supplied by three RE sources. Figure 11(a) shows that in scenario 1 to 5, the implementation of FLC on UPQC-BES system supplied by three RE sources is able to obtain average THD of load voltage slightly better than PI controller and both method have already met the limit in IEEE 519. Further under scenario 6, FLC applied on UPQC-BES system supplied by three RE sources gives significantly better result of average THD of load voltage than PI controller. In six disturbance scenarios, both PI controller and FLC applied on UPQC-BES system supplied by three RE sources, PV is able to obtain the highest average THD of load voltages. Figure 11(b) shows that in disturbance scenario 1 to 5, implementation of FLC on UPQC-BES system supplied by three RE sources is able to obtain the highest average THD of load voltages. Figure 11(b) shows that in disturbance scenario 1 to 5, implementation of FLC on UPQC-BES system supplied by three RE sources is able to obtain the highest average THD of source current slightly better than PI controller. Furthermore under scenario 6, FLC applied on UPQC-BES system supplied by three RE sources gives significantly better result of average THD of source current slightly better than PI controller. Furthermore under scenario 6, FLC applied on UPQC-BES system supplied by three RE sources gives significantly better result of average THD of source current than PI controller. Both PI controller and FLC on UPQC-BES system supplied by three RE sources in six disturbance scenarios, PV is able to obtain the highest average THD of source current.



Matlab/simulink simulation of unified power quality conditioner-battery energy storage... (Amirullah)



Figure 9. UPQC-BES system performance using FLC in scenario 6 (Inter-NL): (a) UPQC-BES + PV; (b) UPQC-BES + Wind; (c) UPQC-BES + PV-Wind Hybrid



Figure 10. Spectra of load voltage harmonics on phase A of UPQC-BES using FLC in scenario 6 (Inter-NL)





(b) Average source current harmonics

Figure 11. Performance of UPQC-BES supplied by three RE sources using PI and FLC

4. CONCLUSION

Comparative performance analysis of UPQC-BES system supplied by three RE sources i.e. PV, wind, and PV-wind hybrid respectively using PI controller and FLC have been discussed. In disturbance scenario 1 to 5, implementation of FLC on UPQC-BES system supplied by three RE sources is able to obtain average THD of load voltage slightly better than PI and both methods have already met the limit in IEEE 519. Under scenario 6, FLC applied on UPQC-BES system supplied by three RE sources gives significantly better result average THD of load voltage than PI. In six disturbance scenarios, both PI and FLC applied on UPQC-BES system supplied by three RE sources is able to obtain average. In interference scenario 1 to 5, FLC method on UPQC-BES system supplied by three RE sources is able to obtain average THD of source current slightly better than PI. Furthermore under scenario 6, FLC applied on UPQC-BES system supplied by three RE sources is able to obtain average THD of source current slightly better than PI. Furthermore under scenario 6, FLC applied on UPQC-BES system supplied by three RE sources is able to obtain average THD of source current slightly better than PI. Furthermore under scenario 6, FLC applied on UPQC-BES system supplied by three RE sources in six scenarios, PV is able to obtain the highest average THD of source current than PI. Both PI and FLC on UPQC-BES system supplied by three RE sources in six scenarios, PV is able to obtain the highest average THD of source current.

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APPENDIX

Three phase grid: RMS voltage 380 volt (L-L), 50 Hz, line impedance: $R_s=0.1$ Ohm $L_s=15$ mH; series and shunt active filter: series inductance $L_{se}=0.015$ mH; shunt inductance $L_{sh}=15$ mH; injection transformers: rating 10 kVA, 50 Hz, turn ratio (N₁/N₂)=1:1; non linear load: resistance $R_L=60$ ohm, inductance $L_L=0.15$ mH, load impedance $R_c=0.4$ ohm and $L_c=15$ mH; unbalance load: resistance $R_1=24$ ohm, $R_2=12$ ohm, and $R_3=6$ ohm, capacitance $C_1, C_2, C_3=2200 \ \mu\text{F}$; DC-link: voltage $V_{DC}=650$ volt and capacitance $C_{DC}=3000 \ \mu\text{F}$; battery energe storage: type=nickel metal hybrid, DC voltage=650 volt, rated capacity=200 Ah, initial SOC=100%, inductance $L_1=6$ mH, capacitance $C_1=200 \ \mu\text{F}$; photovoltaic: active power=0.6 kW temperature=25^o C, irradiance=1000 W/m²; PMSG wind turbine active power=0.6 kW, voltage=380 volt, 50 Hz, wind speed=5 m/s, picth angle=2; PI controller: $K_p=0.2$, $K_i=1.5$; fuzzy model: method=mamdani, composition=max-min; input membership function: error (V_{dc})=trapmf, trimf delta error (ΔV_{dc})= trapmf, trimf; output membership function: \bar{p}_{loss} =trapmf,trimf.



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