Implementation of Single-Phase DVR-BES Based on Unit Vector Template Generation (UVTG) to Mitigate Voltage Sag Using Arduino Uno and Monitored in Real-Time Through LabVIEW Simulation

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Implementation of Single-Phase DVR-BES Based on Unit Vector Template Generation (UVTG) to Mitigate Voltage Sag Using Arduino Uno and Monitored in Real-Time Through LabVIEW Simulation

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Abstract: This paper aims to design and implement a single-phase dynamic voltage restorer (DVR) supplied by battery energy storage (BES) using load voltage controlled by the unit vector template generation (UVTG) method. The UVTG method on the DVR system is implemented using the Arduino-Uno hardware. LabVIEW-based interface simulation is used for monitoring the parameter in real-time during 80% voltage sag period i.e. source voltage, injection voltage, load voltage, 40 ree current, load current, and DC-link voltage. The true power factor measurements are also carried out to obtain total harmonic distortion (THD) of the source current and load current. The single-phase DVR system is connected to load i.e. a 5-watt bulb lamp (linear-load), 5-watt fluorescent (FL) lamp (non-linear load), and 5-watt lightemitting diode (LED) lamp (non-linear load). During voltage sag, the single-phase DVR-BES system is able to maintain load voltage i.e. bulb lamp, FL lamp, and LED lamp of 216 volts, 256 volts, and 185 volts, respectively. The percentage of load sag voltage deviation for each load is 6.4%, 26.13%, and 8.87%, respectively. The measurement of source power-factor with voltage sag results in source true power factor of three loads of 0.985 pu leading, 0.985 pu leading, and 0.990 pu leading respectively. On the same system with voltage sag, single phase DVR-BES is able to result in source current THD for three loads of 1.523%, 1.523%, and 1.010% respectively. The proposed study is able to give the best performance because it is able to produce source current THD lower than the previous studies. By using the Arduino-Uno interface, this model can be run and monitored in real-time with LabVIEW better from the simulations conducted by previous researchers which were still carried out off-line using Matlab/Simulink.

Keywords: Single phase DVR, BES, Arduino uno, LabVIEW, Voltage sag.

1. Introduction

Dur 4g the last decade, there has been an increase in the number of sensitive and critical loads. On the other hand, the use of these tools also has an impact on deteriorating Power Quality (PQ). Among a number of PQ problems, problems related to voltage mitigation are also of increasing importance from a sensitive load and customer point of view. PQ problems related to voltage i.e. voltage sag, voltage swell, voltage harmonics, fluctuation 4 interruptions, and imbalance. In accordance with IEEE 1346 [1] and IEEE 1159 [2] standards, the sag voltage is defined as the RMS (root mean 35 are) AC voltage sag with a magnitude of 10% to 90% of the nominal

voltage, at power frequencies with a duration of 0.5 cycles to one minute. The voltage sag is caused by a single-phase short circuit to ground in the power system, starting in large-capacity induction motors, and sudden changes in the system connected to large loads [3]. Viewed from the system, the DVR is divided into two systems, namely one-phase DVR and three-phase DVR. Then three-phase DVR is connected to a 3 phase 3 wire (3P3W) or a 3 phase 4 wire (3P4W) system. Next, this paper will further focus on the design and implementation of single-phase DVRs to mitigate voltage sag at the source side and connect to a number of the lin 44 non-linear load. The simulation of low voltage single phase DVR based on the multilevel inverter to protect sensitive

loads has bee implemented in [4]. The proposed model is able to compensate for the valtage sag and increase the PQ on the load side. A DVR topology using a cascaded multilevel direct pulse with modulation (PWM) ac-ac converter has been proposed in [5]. In this scheme, the unit cell of the multilevel converter consists of a single-phase ac-ac converter PWM using a switching cell (SC) structure that is paired with ag inductor. The implementation of the phase shift PWM technique is capable of significantly reducing the size of the output filter inductor. One and three-phase DVR control schemes using 71 SCAD/EMTDC have been observed in [6]. The proposed system is able to compensate for a number of voltage sag variations and keep the 44 ad voltage constant. DVR control scheme with an ac-ac converter, based on voltage drop characterization has been investigated in [7] to reduce voltage drop with phase jumps. The superiority of the proposed control scheme is then validated on an ac-ac interphase converter topology. The vector-based one-phase DVR control using an improved synchronous reference frame (SR has been proposed in [8]. The vector analysis use 53 this control method during the voltage period was able to provide the magnitude and phase of the injection voltage.

The control methods to reduce sag voltages using a fuzzy logic controller (FLC) connected with sensitive loads [9] and distributed generation (DG) [10] have been proposed. The 63 LC control was used to generate pulses with the Sinusoidal Pulse Width Modulation (SPWM) technique at the output of an active filter circuit. Comparing to proportionalintegral (PI) control, FLC control was able to provide better performance during voltage sag because it has more advantages in terms of resistance to parameter variations and system execution. A DVR with DGconnected FLC control also able to enhance voltage profiles, power quality, and reliability. Sing 65 phase and three-phase DVRs use a single-phase ac to ac matrix converter to replace voltage source inverter (VSI), has been investigated by Matlab in [11, 12], and in PSCAD [13], at a number of variations in source voltage (sag, flicker, and unbalance). The single-phase DVR has been simulated in [14] and a special voltage detection method for single-phase DVRs has been introduced in [15]. The simulation results show 60t the DVR was able to maintain the nominal load voltage, despite interference and other abnormal conditions from the source side. The special detection method using double closed-loops of the proportional-resonant controller was also able to provide superior performance in voltage detection and compensation.

The DVR control scheme for ref 62 nce voltage generation based on a single-phase Second Order Generalized Integrator-Phase Lock Loop (SOGI-PLL) using a series of active compensator has been observed in [16]. The proposed scheme is capable of dynamically responding, detecting, and rapidly compensating for sag/swell voltages without and with phase jumps. A DVR that uses a multilevel Hbridge inverter with a capacitor as an energy source has been roduced in [17]. This configuration allows the DVR to connect directly to a mediumvoltage network, eliminating the need for a series injection transformer and batteries. The DVR model was the same but uses a single H-Bridge inverter and a battery on sag/swell voltage disturbances connected to the non-linear load which has also been observed in [18]. Interline DVR (IDVR) on two same [59] and different voltage distribution lines with voltage source inverter (VSI) and current source inverter (CSI) [20] to restore voltage sag and harmonics has been introduced. When voltage sag and voltage distortion occur on one channel, the DVR on the same channel is able to perform voltage compensation and harmonics e 46 nation, while the other DVR can recharge the ene 72 to the DC-link to maintain the DC-link voltage constant.

In order to efficiently the number of equipment in DVR circuit configuration, the implementation of a direct ac/ac converter on the DVR has been introduced in [21, 22]. The prof6sed configuration uses the minimum switches, did not require a dc-link energy storage element, and has a longer compensation tim 37 during sag/swell voltage disturbances. The compensation voltage for each phase is taken from each of the three-phase sources so that each courter was able to operate independently and is also able to compensate for single-phase blackouts and unbalance sag/swell voltages. The use of a single-phase transformer-less DVR (TDVR) to mitigate the sag/swell voltage has been observed in [23]. The proposed configuration was capable of reducing system size and losses compared to DVR which using a series transformer. The single-phase interactive channel DVR using the sag voltage detection algorithm has been developed in [24]. The detection algorithm has a hybrid structure consisting of a momentary detection section and a RMS variation detection segion. The DVR development could compensate for inp25voltage sag or interrupt in 2.0-ms delay and can be used effectively for sensitive loads.

The single-phase DVR with synchronous reference frame control under distorted source conditions has be 45 applied in [25]. The proposed control using a moving average filter (MAF) is

capable of extracting positive sequence fundamental 45 nponents as well as being able to mitigate voltages sag and distorted source voltages. The single-phase DVR using elliptical restoration-based voltage compensation to correct the power fact 19 on the source side has been proposed in [26]. The active and reactive voltage components and centrifugal angles are used to for ulate an elliptical compensation path. So that the voltage will be in-phase with the load current using precise control of the DVR injection voltage. The optimization of the voltage injection technique in DVR to protect sensitive loads has been observed in [27]. The recursive least square (RLS) method is used to estimate the magnitude and phase of the voltage in order to minimize the amplitude of the injection voltage. Meanwhile, repetitive control was proposed to track the compensation voltage. Both controls are suitable for sinusoidal reference and are reliable for mitigating harmonics, sags, and swell distortions.

Energy storage in single or three-phase DVR circuits related to the capacity and type of energy storage has become the attention of many researchers. The determination of the two 512 rameters relates to the ability and duration of the energy storage to supply real power to the inverter during a fault. Unbalanced voltage compensation in 3P3W system using DVR using a super capacitor has been investigated in [28]. The proposed DVR configuration uses a control based on the d-q-0 and Proportional Integral (PI) transformation technique and is further coded using a digital signal processor (DSP). DSP control and super capacitor implementation 43 mitigate unbalanced voltage disturbances. A compressed air energy storage powered dynamic voltage restorer (CAESPDVR) wit70 ANFIS control has been proposed in [29] to compensate for unbalanced sag/swell voltages and harmo 24 s. The single-phase DVR configuration using a hybrid energy storage system (HES) has been developed in 560].

The HES series consists of superconducting magnetic energy storage (SMES) in collaboration 24 h battery energy storage (BES) on a DC type DVR. The proposed HES concept integrated with fast response large power SMES unit and low-cost high capacity BES can further be implemented in large scale DVR development. The DVR uses VSI method with SPWM to compensate for sag voltage has been implemented in [31]. The voltage sag was able to be simulated and monitored by LabVIEW with the NI myRIO-1900 interface using LabVIEW in real-time. The mitigation of sag/swell voltage and harmonics in low voltage distribution networks using DVR-BES-PV using the UVTG control method has been observed in [32]. The proposed model was able to

compensate for sag voltage between 10% to 90% and swell voltage between 110% to 180% with a voltage THD within the IEEE 519 limit.

In this paper, BES is proposed as energy storage and implemented in single-phase DVR using load volta 78 control with the UVTG method and connected to linear/non-linear loads. The UVTG method on the DVR system is implemented using the Arduino-Uno microcontroller hardware. The LabVIEW based interface simulation is used to monitor electrical quantities in real-time during the voltage sag period i.e. source voltage, injection voltage, load voltage, source current, load current, and DC-link voltage. The true power factor measurements are also c 40 ed out to obtain the total harmonic value or Total Harmonic Distortion (THD) of the source current and load 52 litrent.

This paper is arranged as follows. Section 2 presents the proposed method, UVTG method, percentage of voltage sag, true power factor and harmonic, single-phase DVR-BES using LabVIEW, as well as hardware and software implementation, Section 3 presents results and discussion of the source

Table 1. Abbreviation

Symbol	Description
PQ	Power Quality
DVR	Dynamic Voltage Restorer
BES	Battery Energy Storage
PV	Photovoltaic
UVTG	Unit Vector Template Generation
THD	Total Harmonic Distortion
Pf_{true}	True Power Factor
FL	Fluorescent
LED	Light Emitting Diode
DG	73 tributed Generation
3P3W	Three Phase Three Wire
3P4W	Three Phas 48 our Wire
SPWM	Sinusoidal Pulse Width Modulation
VSI	Voltage Source Inverter
64]	Current Source Inverter
SOGI-PLL	Second Order Generalized Integrator-
	43 se Lock Loop
CAESPDVR	Compressed Air Energy Storage
	Powered Dynamic Voltage Restorer
ANFIS	Artificial Intelligent Fuzzy Inference
	System
IDVR	Interline Dynamic Voltage Restorer
CB	Circuit Breaker
49 IS	Root Mean Square
GUI	Graphic User Interface
PC	Personal Computer
USB	Universal Serial Bus
PU	Per Unit

voltage, injection voltage, load voltage, DC-link voltage, source current, load current, percentage of

voltage sag, true power-factor, and current THD which analyzed from data measured by Arduino-Uno and mozgored by LabVIEW. In this section, the system connected to the linear/non-linear load with and without voltage sag is selected to present the best single-phase DVR-BES system performance connected to three different types of load during voltage sa 32 Finally, this paper is concluded in Section 4. All manuscripts must be in English. These guidelines include complete descriptions of the fonts, spacing, and related information for producing your proceedings manuscripts. Table 1 shows the abbreviations used in this paper.

2. Research method

2.1 Proposed method

Fig. 1 shows a single-phase DVR supplied by BES using load voltage control with the UVTG method. The DVR is a tool [89] functions to compensate for the load voltage in the event of a voltage sag disturbance on the source bus at a level of 0.1 to 0.9 per unit. The UVTG method on the DVR system is implemented using the Arduino-Uno hardware. LabVIEW-based interface simulation is used to monitor electrical quantities in real-time during the voltage sag period.

The observed parameters are source voltage (V_S) , injection voltage (V_{inj}) , load voltage (V_L) , DC-link voltage $(V_{DC-Link})$, source current (I_S) , and load current (I_L) . The true power-factor (Pf_{true}) measurements are also carried out to obtain the THD value of the source current and load current. There are two cases in this study, the source without voltage sag, and with an 80% voltage sag. In each case, the single-phase DVR

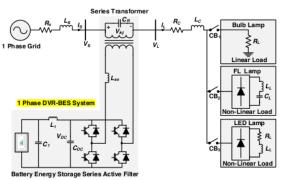


Figure. 1 Proposed single phase DVR-BES connected to linear/non-linear load

Table 2 Notation list and parameters

Table 2. Notation list and parameters		
Notation	Description	

V_S	Source Voltage
V_{inj}	Injection Voltage
V_L	291d Voltage
$V_{DC-Link}$	DC-Link Voltage
I_S	Source Current
I_L	Load Current
I_L^*	Reference Load Voltage
V_m	Peak Fundamental Input Voltage
	Magnitude
K	Gain
S_1, S_2, S_3, S_4	Gating Signal 1, 2, 3, and 4
Sag _{dev}	Voltage Sag Deviation
$V_{pre-sag}$	Pre-Sag Voltage
V_{sag}	Sag Voltage
Pf_{true}	True Power Factor
$P_{av,g}$	Average Power
S	Apparent Power
V_{rms}	RMS Voltage
I_{rms}	RMS Current
V_{1rms}	RMS Fundamental Voltage
I_{1rms}	RMS Fundamental Current
THD_V	Voltage THD
THD_I	Current THD
P_{1avg}	Fundamental Average Power
$Pf_{displacement}$	Displacement Power Factor
$Pf_{distorted}$	Distorted Power Factor
R_S	Line Resistance (0.1 ohm)
L_S	Line Inductance (0.15 mH)
R_C	Load Resistance (0.4 ohm)
L_C	Load Inductance (15 mH)
L _{Se} Series Inductance (0.015 mH)	
L_1 BES Inductance (6 mH)	
C_1 BES Capacitance (1000 μ F)	
C_{DC} DC-Link Capacitance (200 μ F)	
R_L Linier/Non-Linear Resistance (0.6 o	
L_L	Non-Linear Load Inductance (0.15 mH)
C_L	Non-Linear Load Capacitance (3.3 µF)
C_R	Ripple Capacitance (0.2 µF)

system is supplied by BES connected to a 5-watt bulb lamp (linear load), 5 watt FL lamp (non-linear load), and 5 watts LED lamp (non-linear load), so the total selected case is six. The CB1, CB2, and CB3 are used to connect and disconnect links to three linear/nonlinear loads. The DVR-BES system configuration is then run based on a predetermined case using Arduino-Uno microcontroller interfaced communication and the results are simulated and monitored in real-time by a LabVIEW. Table 2 shows the notation list and parameters of Fig. 1.

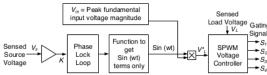


Figure. 2 UVTG control on single phase series active filter

2.2 Unit voltage template generation method

The series active filter protect sensitive loads against several voltage disturbances from the source bus. In [31], the control method of source and load voltage in a three-phase series active filter has been discussed. Using the same procedure, the authors propose the same method for single-phase series active filter control as shown in Fig. 2. This method extracts UVTG from the distorted input supply. Then, the template is expected to be an ideal sinusoidal signal with a unity amplitude. The source of the distorted voltage is measured and divided by the peak amplitude fundamental input voltage (V_m) .

A single-phase locked loop (PLL) is used in order to generate sinusoidal unit vector templates with a phase lagging by the use of the sine equation. The reference signal of the load voltage is calculated by multiplying the unit vector templates with the peak amplitude of the fundamental input voltage (V_m) . The reference load voltage (V_L) is then compared to the sensed load voltage (V_L) by a SPWM controller used to generate the desired four gating signal on a single-phase series active filter.

2.3 Percentage of voltage sag deviation

The recommended standard of practice on monitoring voltage sag/swell as part of electric power quality parameters is IEEE 1159 [2]. This standard presents the definition and table of voltage sag base on categories (instantaneous, momentary, temporary) typical duration, and typical magnitude. The percentage of load voltage sag deviation is formulated in Eq. (1) [31].

$$Sag_{dev}(\%) = \frac{|Vpre_sag-V_sag|}{Vpre_sag}$$
 (1)

2.4 True power factor and harmonics

The true power factor at the load is defined as the ratio of average power to apparent power. The true power factor for both sinusoidal and non-sinusoidal situations is presented in Eq. (2) [33].

$$pf_{true} = \frac{P_{avg}}{S} = \frac{P_{avg}}{V_{rms\,lrms}} \tag{2}$$

$$V_{rms} = V_{1rms} \sqrt{1 + (THD_V/100)^2}$$
 (3)

$$I_{rms} = I_{1rms} \sqrt{1 + (THD_I/100)^2}$$
 (4)

By substituting Eq. (3) and Eq. (4) into Eq. (2), the true power factor (Pf_{true}) results in Eq. (5) for both sinusoidal and non-sinusoidal cases [33].

$$pf_{true} = \frac{P_{avg}}{V_{1rms\,I_{1rms}}\sqrt{1 + (THD_V/100)^2}\sqrt{1 + (THD_I/100)^2}}$$
(5)

A useful simplification can be made by expressing Eq. (5) as a product of two components defined in Eq. (6).

$$pf_{true} = \frac{P_{avg}}{V_{1rms} I_{1rms}} \times \dots \qquad \dots \frac{1}{\sqrt{1 + (THD_V/100)^2} \sqrt{1 + (THD_I/100)^2}}$$
(6)

31 By making the following two assumptions: (1) In 31 st cases, the contributions of harmonics above the fundamental to average power are very small, so that is $P_{avg} \approx P_{1avg}$ and (2) Since THD_V is less than 10%, then from (12) we see that $V_{rms} \approx V_{1rms}$. Then, merging both assumptions into Eq. (6) results in the following approximate function for the true power factor (Pf_{true}) presented in Eq. (7) [33].

$$\begin{split} pf_{true} &= \frac{P_{1awg}}{V_{1rms}\,I_{1rms}} \times \frac{1}{\sqrt{1 + (THD_I/100)^2}} \\ &= Pf_{displacement} \times Pf_{distorted} \end{split} \tag{7}$$

Because displacement power factor (Pf_{disp}) could never be greater than unity, Eq. (7) shows that the true power factor (Pf_{true}) in non-sinusoidal cases has the upper limit so finally its function is defined in Eq. (8) [33].

$$pf_{true} \le Pf_{distorted} = \frac{1}{\sqrt{1 + (THD_I/100)^2}}$$
 (8)

2.5 Single phase DVR-BES using labVIEW

The implementation of the single-phase DVR-BES system consists of several stages. That stage i.e. create a single-phase series active filter, create a gate driver to trigger the MOSFET in the series active filter, create a SPWM program to drive the gate driver as an inverter trigger and create a monitoring program 41_abVIEW. Fig. 3 presents a schematic diagram of a single phase DVR-BES system.

Fig. 3 shows that the BES and series active filters play an important role in compensating for the

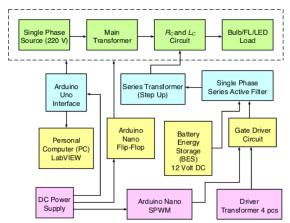


Figure. 3 A schematic diagram of single phase DVR-BES

voltage sag on a single-phase DVR. The step-up transformer that is installed in a series against the load functions to inject the voltage from the series active filter to the load. The main energy source for series active filters uses BES DC voltage 12 V with a capacity of 7.2 Ah. The process of changing the DC to AC voltage begins with the Arduino Nano SPWM microcontroller providing Sinusoidal SPWM pulses to the Gate Driver circuit which has the main component of the TLP 250 Optocoupler IC, then the Gate Driver circuit triggers the IRFP250 MOSFET gate on a series active filter circuit cross-like as an electric current cycle in the circuit bridge diode 134 tifier. So that it will produce an AC output from a series active filter circuit. The output voltage of the series active filter is an AC voltage of 7 V depending on the battery voltage conditions, which will then be increased to an AC voltage of 220 V using a step-up transformer. The step-up series transformer has a power of 600 VA with a primary AC input voltage of 7.2 V an 34 secondary AC output voltage of 220 V. The goal is that the series active filter is able to inject enough power to compensate for the sag voltage at a level of 10% to 90%.

The Arduino Nano flip-flop functions as a timer to run system simulations using a single-phase DVR-BES without and with sag voltage. The Arduino nano has been programmed with a flip-flop program with the 1-second case instructing the relay to turn "on" as a representation of the system experiencing sag voltage and 1 second ordering the relay to turn "off" as a representation of the system without experiencing sag voltage. This timer is expected to function when there is a sag voltage and 5 tomatically orders a single-phase active filter to inject a voltage compensation into the load so that the load voltage will remain stable.

The Arduino Uno interface functions as a medium for receiving data from voltage sensors and current sensors that are measuring the amount of electricity in the DVR circuit and sending the data to a personal computer (PC) with LabVIEW software. Curves and data displayed in LabVIEW i.e. source voltage, load voltage, injection voltage, DC-link voltage, source current, and load current respectively. The display form implemented in LabVIEW is in the form of graphs and number indicators. With a graphic display, the reader will find it easier to observe the wave condition both voltage and current during the system condition without and with voltage sag. All data displayed in LabVIEW is real-time and continuous data as long as the single-phase DVR-BES system is operated to the system. In addition to using the LabVIEW, data collection is 5750 carried out by the cos-phi meter to determine the value of the true power factor of source and load as a basis for determining the harmonic of source and load currents. The single-phase DVR-BES system connected to three linear/non-linear loads i.e. bulb lamp 5 W (linear), FL lamp 5 W (non-linear), LED lamp 5 W (non-linear) respectively.

2.5 Hardware and software implementation

The LabVIEW interface software diagram consists of the main program in the form of a Graphic User Interface (GUI) which functions to run all indicators a 67 controls on the front panel. Fig. 4 shows the model of the single-phase DVR-BES hardware circuit. The nominal parameters of Fig. 4 are presented in Table 3.

Table 3. Nominal of device parameters

Devices	Design Values
Single phase source voltage	220 V
Frequency	50 Hz
Series Transformer (step-up)	600 VA
	7,2/220 V
Main Transformer (CT)	3 A
Current Sensor ACS 712	5A
Relay	1 device
Arduino Uno (Interface)	1 device
Arduino Nano (Flip-Flop)	1 device
Arduino Nano (SPWM))	1 device
Load Resistance (R_C)	0.4 ohm
Load Inductance (L_C)	15 mH
Cos-phi-Meter	1 device
Battery Energy Storage (BES)	12 V/7.2 Ah
DC-link Capacitance (C_{DC})	1000 μF
Bulb Lamp Load	5 W
FL Lamp Load	5 W
LED Lamp Load	5 W

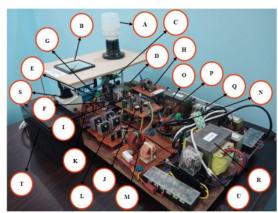


Figure. 4 Single-phase DVR-BES hardware

Where A: Load; B: Cos-phi-meter; C: Arduino Uno; D: Voltage Sensor Transformer; E: Current Sensor; F: Arduino Nano SPWM; G: Relay 1 (4 Channel); H: Arduino Nano Flip-Flop; I: Two Relays (220V-AC); J: Gate Driver Optocoupler; K: DC-link Capacitance and BES filter (C_{DC} , L_1 , C_1); L: Series Active Filter; M: Load Impedance (R_C , L_C); N: Series Inductance (L_{Se}); O: Main Transformer; P: Source Current Sensor; Q: Gate Driver Transformer; R: Series Transformer; S: Source Voltage; T: BES and U: Universal Serial Bus (USB) for data communication between hardware PC.

Fig. 5 shows the overall GUI program design and the component parts of the single-phase DVR-BES. In order for the LabVIEW software interface on the PC to communicate with the Arduino Uno, a program is needed to communicate the two devices. The communication program used by Lifa Base. Lifa Base is the driver for Arduino Uno in connecting data communication with PC. Lifa Base is the default program from Arduino when users install LabVIEW.

3. Results and discussion

Fig. 1 shows a series of DVR supplied by BES connected to a load of Bulb, FL, and LED respectively. The series transformer connected to the load functions to inject the voltage from the series active filter during voltage sag. The Arduino Nano Flip-Flop is used as a timer to run simulated data collection. The cycle timer applied to the DVR is 1 second on and 1 second off. The data collection period is carried out with a LabVIEW simulation for 3 seconds, with 80% depth of source voltage sag duration between 1 to 2 seconds. Data collection is carried out at 1.5 seconds from the curve of the source voltage (V_S) , injection voltage (V_{Inj}) , load voltage (V_L) , DC-link voltage $(V_{DC-Link})$, source current (I_S) , and load current (I_L) , curves. The true

power-factor (Pf_{true}) data in the source bus and load bus is measured from the cos-phi meter.

Using the same LabVIEW simulation procedure and period, data collection is also carried out without the voltage sag. The percentage of load voltage sag deviation is calculated using Eq. (1) with a pre-sag voltage of 203 V. Base on true power-factor, then harmonics current is measured using Eq. (8). Table 4 presents the performance of voltage, current, and percentage of sag deviation of load voltage (V_L) of the single-phase DVR supplied by BES without and with voltage sag disturbance. Table 5 presents the performance of true power factor (Pf_{true}) and harmonics value of the single-phase DVR supplied by BES without and with voltage sag disturbance. Fig. 6, Fig. 7, and Fig. 8 show the performance of voltage and current of the single-phase DVR supplied by BES connecting to bulb lamp, FL lamp, and LED lamp load respect 79 ly.

Fig. 6 shows the simulation curve of the sag voltage on a single-phase DVR system supplied by a BES connected to a bulb lamp load. The voltage sag disturbance lasts from t = 1 to t = 2 seconds with a total simulation time of 3 seconds. The measurements on all simulation parameters curves are carried out at t = 1.5 seconds. At t = 1 to t = 2 seconds, the source voltage (V_S) drops from 230 V to 44.7 V, and the se $\frac{1}{16}$ transformer injects a voltage (V_{Inj}) of 168 V so that the load voltage (V_L) remains constant at 216 V. In this disturbance condition the value of the source current (I_S) is 0.228 A and the load current (I_L) drops to 0.45 A. To keep the load voltage (V_L) maintain constant, BES releases its energy so that the DC link voltage $(V_{DC-Link})$ drops from 13.03 V to 8.20 V.

Fig. 7 shows the simulation curve of sag voltage on a single-phase DVR system supplied by the connected BES to the FL lamp load. At t = 1 to t = 2seconds, the source voltage (V_S) drops from 230 V to 50.3 V and the series transformer injects a voltage (V_{Inj}) of 200 V so that the load voltage (V_L) remains constant at 256 V. During the duration of the sag voltage, the capacitance effect of the capacitor component able to store charge on the FL lamp load, causing the load voltage value to exceed the source voltage. In the disturbance conditions, the value of the source current (I_S) is 0.166 A and the load current (I_L) drops to 0.208 A. To keep the load voltage (V_L) maintain constant, BES releases its energy so that the DC link voltage $(V_{DC-Link})$ drops from 13.03 V to 7.33 V.

Fig. 8 shows a simulation curve voltage sag on a single-phase DVR system supplied by BES connects to the LED lamp load. At t=1 to t=2 seconds, the

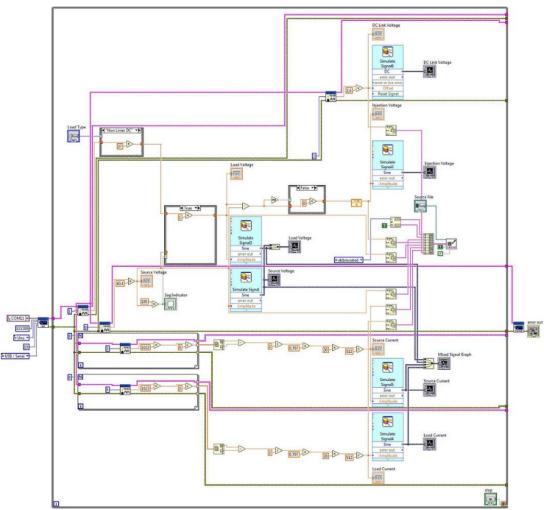


Figure. 5 Software design using LabVIEW interface for simulate signal i.e. (A) arduino-uno data communication, (B) source voltage (V_S) , (C) injected voltage (V_{Inf}) , (D) load voltage (V_L) , (E) source current (I_S) , (F) load current (I_L) , (G) DC-link voltage $(V_{DC-Link})$, and (H) mixed signal graph

Table 4. Performance of voltage, current, and sag deviation of load voltage of the single-phase DVR supplied by BES

No.	Load Type	$V_{S}(V)$	$V_{Inj}(V)$	$V_L(V)$	$I_{S}(A)$	$I_L(A)$	$V_{DC-Link}(V)$	Sag Dev of
								$V_L(\%)$
	Without Voltage Sag							
1.	Bulb Lamp	203	0	203	0.208	0.166	13.03	0
2.	FL Lamp	203	0	203	0.208	0.083	13.03	0
3.	LED Lamp	203	0	203	0.270	0.166	13.03	0
				With Sag	Voltage			
4.	Bulb Lamp	44.7	168	216	0.228	0.145	8.20	6.40
5.	FL Lamp	50.3	200	256	0.166	0.208	7.33	26.13
6.	LED Lamp	49.1	133	185	0.249	0.789	8.06	8.87

source voltage (V_S) drops from 230 V to 49.1 V and the series transformer injects a voltage (V_{Inj}) of 133 V so that the load voltage (V_L) remains constant at 185 V. During the disturbance conditions, the value

of the source current (I_S) is 0.249 A, and the load current (I_L) increases to 0.789 A. To keep the load voltage (V_L) maintain constant, BES then releases its energy so that the DC link voltage $(V_{DC-Link})$ drops

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Table 5. Performance of power factor and harmonics of the single-phase DVR supplied by BES

No.	Load Type	Source $Pf_{true}(pu)$	Load Pf _{true} (pu)	Source $THD_I(\%)$	Load THD _I (%)
		Wit	hout Voltage Sag		
1.	Bulb Lamp	0.850	0.999	17.647	0.1001
2.	FL Lamp	0.900	0.999	11.111	0.1001
3.	LED Lamp	0.990	0.999	1.010	0.1001
		W	ith Sag Voltage		
4.	Bulb Lamp	0.985	0.998	1.523	0.2040
5.	FL Lamp	0.985	0.998	1.523	0.6040
6.	LED Lamp	0.990	0.975	1.010	2.5640

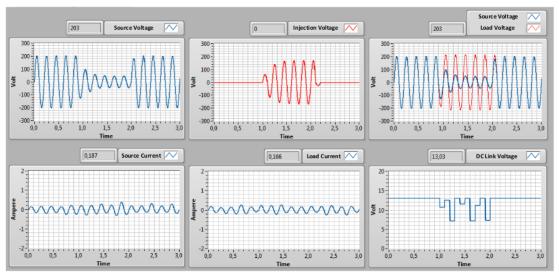


Figure. 6 Performance of V_S , V_{Inj} , V_L , I_S , I_L , and $V_{DC-Link}$ from the single-phase DVR-BES connected to bulb lamp load using LabVIEW

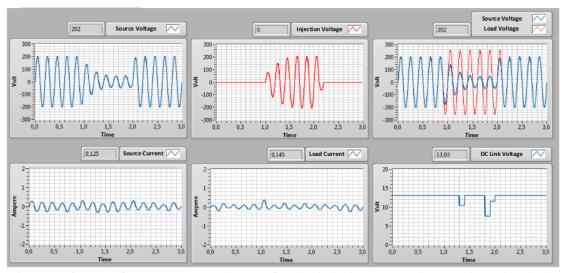


Figure. 7 Performance of V_S , V_{Inj} , V_L , I_S , I_L , and $V_{DC-Link}$ from the single-phase DVR- BES connected to FL lamp load using LabVIEW

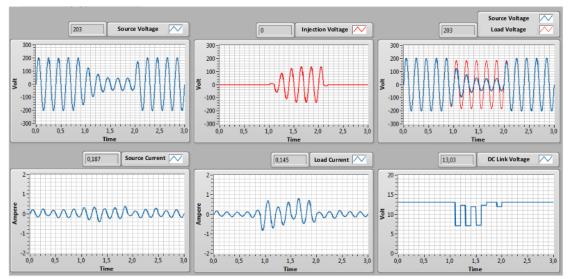


Figure. 8 Performance of V_S , V_{lnj} , V_L , I_S , I_L , and $V_{DC-Link}$ from the single-phase DVR- BES connected to LED lamp load using LabVIEW

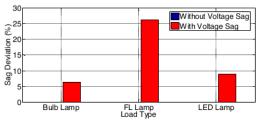


Figure. 9 Performance of sag deviation of V_L for single phase DVR-BES system on three load type

from 13.03 V to 8.06 V.

Fig. 9 shows that for the system without sag voltage, the series active filter circuit and series transformer on a single-phase DVR-BES system is not able to inject voltage into the load, so produces a percentage of sag deviation of load voltage (V_L) of 0%. Otherwise if the system with sag voltage, the single-phase DVR-BES system is able to maintain the load voltage (V_L) i.e. bulb lamp, FL lamp, and LED lamp of 216 V, 256 V, and 185 V, respectively.

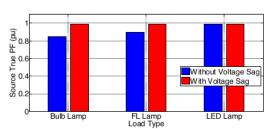


Figure. 10 Performance of source true power-factor for single phase DVR-BES system on three load type

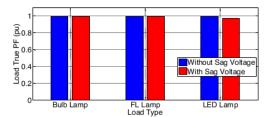


Figure. 11 Performance of load true power-factor for single phase DVR-BES system on three load type

The percentage of load voltage deviation for the system with sag deviation of V_L for the three loads type are 6.4%, 26.13%, and 8.87%, respectively.

Fig. 10 shows the measurement of source true power-factor without voltage sag of the bulb lamp has the worst true power-factor (Pf_{true}) of 0.850 perunit (pu) leading compared to an FL lamp of 0.900 pu leading and an LED lamp of 0.909 pu leading. Otherwise, for the system with voltage sag, the single-phase DVR-BES system produces source true power factor (Pf_{true}) for a bulb lamp, FL lamp, and LED lamp of 0.985 pu leading, 0.985 pu leading, and 0.990 pu leading respectively.

Fig. 11 shows the measurement of load true power-factor without voltage sag for all load categories results in the same true power factor (Pf_{true}) of 0.999 pu leading. Otherwise, for the system with voltage sag is able to result in load true power factor (Pf_{true}) i.e. bulb lamp, FL lamp, and LED lamp of 0.975 pu leading, 0.998 pu leading, and 0.994 pu leading respectively.

Fig. 12 shows that the system without sag voltage

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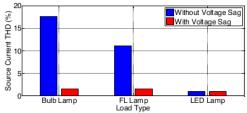


Figure. 12 Performance of source harmonics for single phase DVR-BES system on three load type

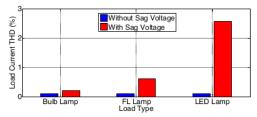


Figure. 13 Performance of load harmonics for single phase DVR-BES system on three load type

Table 6. Comparison of implementation UVTG-DVR-BES-Arduino-Uno-LabVIEW (proposed study) and previous studies

No.	Authors	Methods	Depth Sag of V _S (%)	Sag Dev of V _L (%)	Load THD _V (%)	Source THD _I (%)	Source pf _{true}	Real Time
1	D.N. Katole, et al [8]	Improved SRF	42	7.6	NA	NA	NA	Not
2	M.T. Hagh, et al. [10]	FLC	92 without and 95 with DG	8.9 without DG and 6.4 with DG	1.26 without DG and 3.54 with DG	NA	NA	Not
3	H.K. Yada, et. al [16]	SOGI-PLL	30	3.0	NA	NA	NA	Not
4	S. Galeshi, et al. [17]	Multilevel Cascade H-Bridge Inverter	20	0.0	4.0	NA	NA	Not
5	R. Nittala, et al [19]	IDVR with VSI and CSI	27.7 with VSI and CSI	0 with VSI and CSI	0.06 with VSI and 0.05 with CSI	NA	NA	Not
6	E. Babaei, et. al. [22]	Direct Converter	65	0	7.07 (Average)	NA	NA	Not
7	A. Benhail, et al. [23]	TDVR-PI	30	2.18	24	NA	NA	Not
8	J. Ye, et.al. [26]	Elliptical Restoration	60	NA	NA	NA	0.75	Not
9	R. Omar, et.al	DVR-Super- capacitor	30	0	NA	2.38	NA	Not
10	C.K. Sundara- balan, et. al. [29]	CAESPDVR- ANFIS	46.67 (Average)	0.4	2.35	NA	NA	Not
11	V.K. Awaar, et al. [31]	VSI-SPWM-NI- myRIO-1900- Labview	50	8.79	NA	NA	NA	Yes
12	A.Kiswantono et al. [32]	UVTG-DVR- BES-PV	80	2.89 (Average)	5.81 (Average)	NA	NA	Not
13	Proposed Study	UVTG-DVR- BES-Arduino- Uno-Labview	80	Bulb=6.4 FL =26.13 LED=8.87	NA	Bulb=1.523 FL=1.523 LED=1.010	Bulb=0.985 FL=0.985 LED=0.990	Yes

Note: NA = note available

is able to produce the source THD_I for bulb lamp, FL lamp, and LED lamp of 17.647%, 11.111%, and 1.010% respectively. Otherwise, for the same system with sag voltage is able to result source THD_I . for

bulb lamp, FL lamp, and LED lamp of 1.523%, 1.523%, and 68.010% respectively.

Fig. 13 shows that the system without voltage sag is able to produce the same load *THD*_I for bulb lamp, FL lamp, and LED lamp of 0.1001%. Otherwise, for

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the same system with voltage sag is able to result in load THD_I for bulb lamp, FL lamp, and LED 7a)p of 0.204%, 0.604%, and 2.564% respectively. Fig. 10 and Fig. 11 shows in the case of voltage sag and three types of loads, the LHE lamp is able to result in the best performance because it is able to produce the highest source true power factor (Pf_{true}) of 0.990 pu and the lowest source THD_I of 1.010%. The source THD_I and load THD_I value in voltage sag also had met the IEEE 519.

Table 6 shows the validation of the results for the proposed study compared to the 12 previous studies. The parameters observed are depth of sag of V_S , sag deviation of V_L , load THD_V , source THD_I , and realtime simulation. At [8], D.N. Katole, et.al proposed an improved SRF on the single-phase DVR series. With a depth of sag of V_S of 42%, this method produces a sag deviation of V_L of 7.6%. Furthermore, the FLC method for sag stress compensation was proposed by M.T. Hagh, et.al [10]. With a depth of sag of V_S of 92% without and 95% with DG, the FLC method yields a sag deviation of V_L of 8.9% without DG and 6.4% with DG, and a load THD_V of 1.26% without DG and 3.54 with DG. The SOGI-PLL method proposed by Yada et. Al [16], with a depth of sag of V_S of 30% was able to produce a sag deviation of V_L of 3.0%. S. Galeshi, et. al [17] already offer Multilevel Cascade H-Bridge Inverter topology. With a depth of sag of V_S of 20%, this topology produces a sag deviation of V_L of 0% and a load of THD_V of 4%. IDVR configuration with VSI and CSI has been proposed by R. Nittala, et.al [19]. With a depth of sag of V_S of 27.7% (with VSI and CSI), this configuration resulted in a sag deviation of V_L of 0%, load THD_V of 0.06% (with VSI) and 0.05% (with CSI). E. Babaei, et. al [22] have proposed a direct converter topology to mitigate voltage sag. With a depth of sag of V_S of 65%, this topology produces a sag deviation of V_L of 0% and a load THD_V of 7.07% (average).

The TDVR-PI configuration has been proposed by A. Benhail, et.al. [23]. With a depth sag of V_S , of 30%, this configuration results in a sag $\stackrel{\bullet}{0}$ viation of V_L of 2.18% and a load THD_V of 24%. J. Ye, et.al $\stackrel{\bullet}{39}$ have proposed an elliptical restoration method for voltage sag compensation and power factor correction. With a depth of sag of V_S , of 60%, this method is able to produce a source pf_{true} of 0.75 pu. The DVR-Super-capacitor configuration has been implemented by R. Omar, et.al [28]. With a depth of sag of V_S , of 30%, this topology is able to produce a sag deviation of V_L of 0% and source THD_I of 2.38%. The CAESPDVR-ANFIS topology has been investigated by C.K. Sundarabalan, et. al. [29]. With

a depth of sag of V_S , of 46.67% (average), this topology was able to produce a sag deviation of V_L of 0.4% and a load of THD_V of 2.35%. V.K. Awaar, et.al. [31] have implemented a VSI-SPWM-based single-phase DVR model with the NI-myRIO-1900 interface monitored in real-time by LabVIEW. With a depth of sag of V_S , of 50%, this model was able to produce a sag deviation of V_L of 8.79%. DVR control supplied by BES-PV using the UVTG method has been observed by A. Kiswantono [32]. With a depth of sag of V_S , of 80%, this configuration and method were able to produce a sag deviation of V_L of 2.89% (average) and a load THD_V of 5.81% (average). Based on the results of research [31] and [32], then this study has implemented the single-phase DVR model using the UVTG method with the Arduino-Uno interface monitored in real-time by LabVIEW. With a depth of sag of V_S of 80%, the proposed model is able to produce sag deviation of V_L of 6.4% (Bulb), 26.13% (FL), and 8.87% (LED). The model is also able to produce THD_I source of 1.523% (Bulb), 1.523% (FL), and 1.101% (LED) and pf_{true} respectively 0.985% (Bulb), 0.985% (FL), and 0.909% (LED). The proposed study is able to give the best performance because it is able to produce source THD_I lower than [28] and source pf_{true} is higher than [26]. Another contribution is that by using the Arduino-Uno interface, the proposed model can be run and monitored in real-time with LabVIEW. It is different from the simulations conducted by 12 previous researchers (except [31]) which were still carried out off-line using Matlab/Simulink environment.

4. Conclusion

The system using a single-phase DVR supplied by BES with load voltage controlled by a UVTG method has been implemented. The model is connected to three types of linear/non-linear load i.e. bulb lamp, FL lamp, and LED lamp. This configuration is proposed to mitigate 80% voltage sag using the Arduino-Uno hardware and monitored by LabVIEW simulation in real-time. The investigated parameter is source voltage, injection voltage, load voltage, source current, load current, and DC-link voltage. The true power-factor measureme 43 are also carried out to obtain the harmonics of the source current and load current. During voltage sag, the single-phase DVR-BES system is able to maintain load voltage for all types of loads. From the system with voltage sag and three different types of loads, the LHE lamp is able to result in the best performance because it is able to produce the highest source current power factor (pf_{true}) and

the lowest source THD_I . The source THD_I and load (THD_I) with voltage sag also had met the IEEE 519. The proposed study is able to give the best performance because it is able to produce source THD_I lower than the previous studies. By using the Arduino-Uno interface, this model can be run and monitored in real-time with LabVIEW better from the simulations conducted by previous researchers which were still carried out off-line using Matlab/Simulink.

In a system using a single-phase DVR-BES connected to the FL load, there is a significant increase in load voltage of 256 V compared to the source voltage. The percentage of sag voltage for FL lamps also increased by 26.13% and has far exceeded the value of 5%. The implementation of a single-phase bidirectional inverter circuit as the interface between the BES and series active filters can be proposed as future work to overcome this problem. The measurement of source THD_V at 69 and THD_V in the proposed model is also necessary to determine the harmonic mitigation performance of the voltage within the IEEE 519 limit.

Conflicts of Interest

The authors declare no conflict of interest.

Author Contributions

Conceptualization, Y.A. Setiawan and A. Amirullah; methodology, Y.A. Setiawan and A. Amirullah; software, Y.A. Setiawan; validation, Y.A. Setiawan; formal analysis, Y.A. Setiawan and A. Amirullah; investigation, Y.A. Setiawan and A. Amirullah; reso 55:s, Y.A. Setiawan; data curation, Y.A. Setiawan; writing—original draft preparation, Y.A. Setiawan; writing—review and editing, Y.A. Setiawan; visualization, Y.A. Setiawan; supervision, A. Amirullah; project administration Y.A. Setiawan; funding acquisition, A.Amirullah. All authors read and approved the final manuscript.

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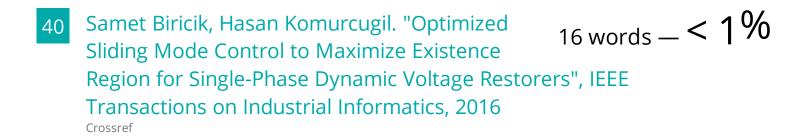
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